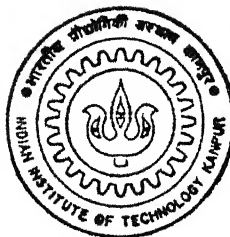


# TRACKING ERROR BASED SLIDING MODE CONTROLLER DESIGN WITH APPLICATION TO FLIGHT CONTROL

by  
GIRESH KUMAR SINGH



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DEPARTMENT OF ELECTRICAL ENGINEERING

**Indian Institute of Technology Kanpur**

FEBRUARY, 1998

# TRACKING ERROR BASED SLIDING MODE CONTROLLER DESIGN WITH APPLICATION TO FLIGHT CONTROL

*A Thesis Submitted*  
in Partial Fulfillment of the Requirements  
for the Degree of  
Doctor of Philosophy

*by*  
**GIRESH KUMAR SINGH**



*to the*  
**DEPARTMENT OF ELECTRICAL ENGINEERING  
INDIAN INSTITUTE OF TECHNOLOGY, KANPUR**  
**February, 1998**

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To  
Mini, Baby, Papa,  
&  
Sweet Memories of Mummy





## CERTIFICATE

It is certified that the work contained in this thesis entitled *Tracking Error Based Sliding Mode Controller Design with Application to Flight Control* by *Gireesh Kumar Singh* has been carried out under my supervision and that this work has not been submitted elsewhere for a degree.



---

Professor K. E. Holé  
Department of Electrical Engineering  
Indian Institute of Technology  
Kanpur

February, 1998

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# Synopsis

The Flight Control System (FCS) design for modern fighter aircrafts is one of the major problems encountered in its development phase. This design problem has assumed more importance with unstable airframes, ever expanding flight envelopes and involved technological developments. These developments are directed to enhance the combat agility and survivability. In fact, the development of new tactical maneuvers and strategies now hinges on the capability of the FCS. Conventionally, gain-scheduling has been the most widely used method to design the FCS. However, the method is rather ad hoc in nature and requires extensive simulation before it can be applied in flight. Recent developments in nonlinear control theory, namely the feedback linearization or the dynamic inversion, have also been applied to FCS design. However, guaranteeing stability and performance robustness in the presence of uncertainty and disturbances is not very straightforward and has been tackled using the approaches developed in the linear control theory.

The present work is a study of the feasibility and applicability of the Sliding Mode Control (SMC) method for the FCS design. The SMC method uses a nonlinear discontinuous control law and offers attractive robustness properties. The method originated in the Soviet literature. The method involves a) the selection of a sliding surface (SS), and b) the choice of a control law to make the SS attractive. The evolution of trajectories may be considered in two distinct phases, a reaching phase, in which a trajectory reaches the SS, and a sliding phase where it will evolve according to the dynamics specified by the selected SS. Invariance to unknown but bounded matched uncertainties and disturbances in the sliding phase has been established. This is made possible by using a high gain or switching type of control law. However, practical applications

of the method are limited by the facts that

1. It is directly applicable to input affine systems only.
2. Robustness in the presence of unmatched uncertainties is not guaranteed.
3. The inputs to any practical system are the outputs of a dynamic actuation system with a finite bandwidth, and thus instantaneous changes in the input cannot be achieved ruling out the use of a discontinuous term as in the conventional SMC method.

These issues are addressed in this work for the aircraft longitudinal FCS design problem.

The Chapter 2 considers the design of a constant plus proportional rate reaching law SMC for second order nonlinear systems. Conventionally, the controller parameters are selected so as to minimize the reaching time, i.e the time taken to arrive at the SS, and use the guaranteed invariance property offered by the SMC. However, a quick tracking performance in terms of the time taken to reach a small output tracking error (OTE) is of primary interest and should govern the parameter selection. For this, firstly it is established that this composite rate reaching law has a robust performance even before the onset of sliding. A new method of selection of the controller parameters based on the criterion of minimizing the time to reach a pre-specified OTE is proposed. It is established that controllers designed using the criterion of the time to OTE, while using similar peak levels of control effort, are expected to take substantially shorter times to the OTE as compared to designs based on the reaching time criterion. The method is applied to two second order mechanical systems, and the simulation results show that control laws designed based on the new criterion result in appreciably faster output tracking, verifying the parameter selection approach.

Although the SMC method has excellent robustness properties, its applications to the FCS design problem have been few. The forces and moments generated are known to be complicated nonlinear functions of the aerodynamics and control surface deflections. Most of the published works use linearized approximations of the nonlinear aerodynamics to develop input-affine models for the aircraft dynamics, as the SMC is

directly applicable to this class of systems. In this work, the forces and moments are directly treated as inputs to the aircraft instead of the conventional control surface deflections, with the assumption that appropriate methods of generation of the desired forces and moments exist. A bounded multiplicative uncertainty is assumed between the command force vector and the actually realized force vector to account for any errors that might be involved in generating the desired force-moment vector. An explicit model following (MF) structure is used to design a SMC (MF-SMC) based full-envelope control law, using full state feedback, for the nonlinear longitudinal dynamics of an aircraft for the case of matched uncertainties and disturbances in Chapter 3. Analytical control laws for two operational modes of the aircraft, namely i) the velocity tracking mode, and ii) the trimming mode are derived. Results of the numerical simulation using parameters of the F-16 aircraft confirm the robustness of the control law and establish the applicability of the design method.

The SMC method is next extended to include the presence of unmatched uncertainties and disturbances as it would be present in most practical systems. The SMC design for this case is developed based on a multi-loop (ML) strategy. With the velocities as primary outputs of the aircraft system, the uncertainties/disturbances present in the dynamics of the position state variables would be unmatched. It is assumed that model responses for the velocity and position state variables are available. The outer loop control law is designed so as to track the position state variables by treating the command signals for the velocity variables as the input. The ML strategy passes on the effect of the unmatched disturbances in the outer loop to the inner loop. A SMC based inner loop control law is then designed to track the command velocity variables. The difference between the model and the command velocity variables has been derived and is shown to depend on the magnitude of the unmatched uncertainties. The ultimate boundedness of the position and velocity errors is established and their time domain bounds are obtained as functions of the controller parameters. These bounds can thus serve as a guideline for their selection. The method is applied to the design of the velocity tracking mode controller for the aircraft longitudinal dynamics. Numeri-

cal results for various choices of the controller parameters are presented in Chapter 4. The ML approach is then applied to single input (SI) higher order nonlinear systems with unmatched uncertainties. Analysis for a third order system shows that, with the proposed method of selection of the switching term gain, the conventional SMC design can be applied to tackle unmatched uncertainty. The errors in the various loops are shown to be ultimately bounded. Numerical simulation on a nonlinear system confirms the developed bounds and verify the applicability of the ML strategy.

The chattering phenomenon, due to the use of a discontinuous control law, is one of the most serious limitations of the SMC approach which restricts its application to practical problems. Moreover, the control inputs to any system are generally applied through an actuation system with a finite bandwidth, ruling out the possibility of instantaneous switching capability. In this work, the input is considered to be the output of a specified first order system with disturbances and uncertainties. Available studies use higher order sliding modes and a differential algebraic approach to address this problem. However, both of these methods involve higher order derivatives of the states and thus the propagation of disturbances and uncertainties becomes complicated making robustness analysis very difficult. The ML strategy, developed in Chapter 4, is extended to the SMC design for such systems in Chapter 5. The propagation of disturbances in the ML strategy is better handled and obviates the need of derivatives of the uncertainties/disturbances leading to a simpler robustness analysis. The state and input errors are shown to be ultimately bounded. The method is first developed for a SI nonlinear system and applied to the nonlinear spring mass problem. Simulation results verify the approach. The method is then applied to the MI aircraft velocity tracking problem, considered earlier, with specified first order input dynamics, and the ultimate boundedness of the the velocity, position, and input errors is established. A parametric study of the choice of controller parameters is done. Results of the numerical simulation in the velocity tracking mode establish the applicability of the ML approach to this problem.

# Contents

Acknowledgments	iv
Synopsis	vi
Table of Contents	x
List of Tables	xii
List of Figures	xiii
<b>1 Introduction</b>	<b>1</b>
1.1 The Aircraft Flight Control Problem . . . . .	1
1.2 The Sliding Mode Control Method . . . . .	5
1.3 Application of SMC to Flight Control Design . . . . .	6
1.3.1 The Unmatched Uncertainty Case . . . . .	8
1.3.2 SMC with Input Dynamics . . . . .	9
1.4 Organization of the Thesis . . . . .	10
<b>2 Design of Proportional plus Constant Rate Reaching Law SMC for Second-order Systems</b>	<b>12</b>
2.1 Introduction . . . . .	12
2.2 The Reaching Law based SMC Design Method . . . . .	13
2.3 Selection of SMC Parameters . . . . .	17
2.3.1 The Relative Choice of $\alpha$ and $\epsilon$ . . . . .	21
2.4 Simulation Results . . . . .	24
2.4.1 Nonlinear Spring Mass Damper System . . . . .	25
2.4.2 Two-link Robotic Arm . . . . .	29
2.5 Conclusions . . . . .	32
<b>3 SMC for the Longitudinal Dynamics of a Fighter Aircraft</b>	<b>35</b>
3.1 Introduction . . . . .	35
3.2 Longitudinal Dynamics and Force Control Approach . . . . .	36
3.3 The Model-Following Control . . . . .	39



3.4	Tracking in Multi-Input Nonlinear Systems . . . . .	42
3.5	Numerical Example and Simulation . . . . .	46
3.5.1	Controller Design for Tracking Mode . . . . .	47
3.5.2	Controller Design for Trim Mode . . . . .	53
3.6	Conclusions . . . . .	60
4	Multi-Loop SMC Laws for The Unmatched Uncertainty Case	61
4.1	Introduction . . . . .	61
4.2	ML Strategy for Mechanical Systems . . . . .	62
4.3	SMC Design for Aircraft Velocity Tracking . . . . .	68
4.3.1	Simulation Results . . . . .	72
4.4	ML Analysis for Higher Order SISO Systems . . . . .	78
4.4.1	ML Analysis . . . . .	82
4.4.2	Numerical Example and Simulation . . . . .	89
4.5	Conclusions . . . . .	91
5	SMC for Systems with Input Dynamics	93
5.1	Introduction . . . . .	93
5.2	ML Analysis for a SI Mechanical System . . . . .	95
5.2.1	A Nonlinear Spring Mass Damper System . . . . .	98
5.3	Aircraft Longitudinal Control with First Order Input Dynamics . . . . .	102
5.3.1	Simulation Results . . . . .	108
5.4	Conclusions . . . . .	116
6	Conclusions & Scope for Further Work	117
	References	121
	Appendices	
A	The $S$ response	128
B	Proof of <i>Claim 1</i>	130
C	Proof of <i>Claim 2</i>	133
D	The Aircraft Parameters, Disturbances, and Uncertainties	138
E	Time Derivatives of Functions	142
F	The Uniform Ultimate Boundedness of Systems	145
G	The Error Bounds	147

# List of Tables

2.1	Comparison of time for OTE and Reaching: Example 1. . . . .	26
2.2	Comparison of time for OTE and Reaching: Example 2. (L1) and (L2) denote responses for the Links 1 and 2 respectively. . . . .	31

# List of Figures

2.1	Tracking responses for Case 1 ('C1') and Case 2 ('C2'). . . . .	27
2.2	The $s$ responses for Cases 1 and 2. . . . .	28
2.3	The error dynamics for Cases 1 and 2 and that given by the A-dynamics ( $e_A$ ). . . . .	28
2.4	The control effort $u$ required for Cases 1 and 2. . . . .	29
2.5	Error responses for the first link for Cases C3 ( $CQ$ ) and C4 ( $CP$ ). . . .	32
2.6	Error responses for the second link for Cases C3 ( $CQ$ ) and C4 ( $CP$ ). .	33
2.7	The input torque $\tau_1$ . . . . .	33
2.8	The input torque $\tau_2$ . . . . .	34
3.1	Schematic Model-Following Control Scheme. . . . .	40
3.2	Tracking error in $U$ (fps). . . . .	50
3.3	Tracking error in $W$ (fps). . . . .	51
3.4	Tracking error in $Q$ (rad/s). . . . .	51
3.5	The command $F_x$ ( $F_{com.}$ ) and the actually realized force ( $F_{act.}$ ). . . .	52
3.6	The command $F_z$ ( $F_{com.}$ ) and the actually realized force ( $F_{act.}$ ). . . .	52
3.7	The command $M$ ( $M_{com.}$ ) and the actually realized force ( $M_{act.}$ ). . . .	53
3.8	$V_t$ tracking error in the Trimming mode (fps). . . . .	58
3.9	Flight path angle ( $\gamma$ ) response in the Trimming mode (rad). . . . .	58
3.10	Angle of attack ( $\alpha$ ) response in the Trimming mode (rad). . . . .	59
3.11	Altitude ( $p_z$ (ft)) response in the Trimming mode. . . . .	59
4.1	Schematic Multi-Loop Control Scheme. . . . .	64
4.2	Variation in the $R_m$ and the $c_7$ parameters of the aircraft. . . . .	73
4.3	Tracking error $U - U_d$ (fps). . . . .	76
4.4	Tracking error $W - W_d$ (fps). Note that responses $R_1$ and $R_4$ overlap. .	77
4.5	Tracking error $Q - Q_d$ (rad/s). Note that responses $R_1$ and $R_4$ are overlapping. . . . .	77
4.6	The position tracking error $S_\theta = \theta - \theta_d$ (rad). Responses $R_1$ and $R_4$ are overlapping. . . . .	78
4.7	The position tracking error $S_x = p_x - p_{x_d}$ (ft). Responses $R_2$ and $R_4$ overlap. . . . .	79

4.8	The position tracking error $S_z = p_z - p_{z_d}$ (ft). Note that $R_2$ and $R_4$ are overlapping. . . . .	79
4.9	The command and achieved $F_x$ . . . . .	80
4.10	The command and achieved $F_z$ . . . . .	80
4.11	The command and achieved $M$ . . . . .	81
4.12	The $K_1 - K_2$ space. . . . .	89
4.13	Output tracking error $e_1 (= \bar{e}_1)$ . . . . .	91
4.14	Output tracking error $e_2$ . . . . .	92
5.1	The tracking responses for Cases $a_0$ and $a_1$ . . . . .	100
5.2	The $u$ dynamics for the $a_0$ case. . . . .	101
5.3	The $u$ dynamics for the $a_1$ case. . . . .	101
5.4	The $S_U = U - U_a$ response. Note that responses $R_1$ and $R_2$ overlap. . .	111
5.5	The $S_W = W - W_a$ response. The $R_2$ and $R_3$ are seen to be overlapping. .	111
5.6	The $S_Q = Q - Q_a$ response. The $R_2$ and $R_3$ are seen to be overlapping. .	112
5.7	The $p_x - p_{x_d}$ responses. . . . .	113
5.8	The $p_z - p_{z_d}$ responses. Note that the $R_2$ and $R_3$ responses overlap. . .	113
5.9	The $\theta - \theta_d$ responses. The $R_2$ and $R_3$ responses almost overlap. . . . .	114
5.10	The $F_x - F_{x_a}$ responses. . . . .	114
5.11	The $F_z - F_{z_a}$ responses. . . . .	115
5.12	The $M - M_a$ responses. . . . .	115
C.1	The $e-\dot{e}$ plane. . . . .	135
D.1	Variation in the $R_m$ and the $c_7$ parameters of the aircraft. . . . .	141

# Chapter 1

## Introduction

### 1.1 The Aircraft Flight Control Problem

The aircraft flight control system (FCS) design is amongst the most critical problems faced in an aircraft development project. This design problem has become more critical with unstable nominal aircraft designs, ever expanding flight envelopes, and ongoing technological developments. McRuer and Graham [1] chart out the historical developments in the controller design since the first flight in 1901 by the Wright Brothers. The onset of high speed digital computers revolutionized the conventional control schemes resulting in the fly-by-wire and the active control technology [2, 3]. Novel concepts such as the Control Configured Vehicles (CCVs) [2, 4, 5] have been tried out on many operational aircrafts with associated benefits. Another such emerging technology area is the thrust vectoring (TV) which will be equipping almost all the future generation fighter aircrafts [6–9]. This makes use of the fact that the engine thrust remains almost constant as compared to the flow dependent conventional flight control (CFC) surfaces, namely the elevator, aileron and the rudder, and hence can be used even after the CFC surfaces are ineffective. To increase combat effectiveness and survivability, fighters are being pushed not only to the limits of the conventional flight envelopes but also beyond to acquire a tactical edge over the contemporary fighters. So much so that the development of new combat tactics and strategies is now governed by the capability of the FCS. The 'Pougachev's Cobra maneuver' routinely displayed by the

Sukhoi fighters [9] is one of the so called super-maneuvers. Other examples include the 'Herbst Maneuver' in which the aircraft rotates its velocity vector through  $180^\circ$  in a minimum possible time. The governing theme guiding these developments is that maneuverability of manned flight should be bounded by the limitations of the human pilot and not the airframe.

The aircraft is conventionally modelled as a 6 degree of freedom (dof) rigid body [10] ( 3 for the translational and 3 for rotational). This results in a highly coupled and nonlinear set of dynamic equations. The dynamic modes of the aircraft may be broadly classified into two categories, i) Rotational modes, and ii) Flight path modes. The responsiveness of an aircraft to maneuvering commands, i.e its agility, is determined by the speed of the rotational modes. The natural frequencies of these modes are sufficiently high so as to make it impossible for the pilot to control the aircraft if these are lightly damped or unstable. Control systems are needed to augment the natural modes to have a suitable damping and frequency characteristics. These are popularly called the Stability Augmentation Systems. In addition to these, there are the Control Augmentation Systems, which help in achieving a desired response to the the pilot control inputs as in tracking etc. Autopilots are also used to perform pilot relief functions such as attitude hold or for navigational purposes. These control systems are intended to perform the functions designated to them over the entire flight envelope. The uncertainties and disturbances are an unavoidable feature of any practical dynamic system. These arise either because of the inexact knowledge of the parameters in the system (structured uncertainty) or because of unmodeled dynamics (unstructured uncertainty). A practical control system design besides performing stabilization should also provide

- robustness to uncertainty and disturbances, and
- some desired response characteristics- popularly known as Flying /Handling qualities (HQ).

This necessitates the design and use of a flight control system (FCS) to meet stability and performance specifications over an entire flight envelope.

Linearized aircraft dynamics has been conventionally used to design linear control laws [10]. One approach was to design a single linear controller for the entire flight envelope. Hence the variation in aircraft dynamics at different flight conditions was modeled as a nominal plant with an additional uncertainty term. Yedavalli [11] considers robust linear controller design under structured uncertainties. Houpis et.al. [12] using quantitative feedback techniques design a robust control law for the F-16 aircraft accounting for four different flight conditions and six failure modes, i.e. a total of 24 possible flight configurations. However, any scheme using a single linear control law for the entire flight envelope would achieve stability robustness only at the cost of sacrifice in performance. Moreover, the nature of changes involved in the aircraft dynamics with varying flight conditions is not completely unknown and may be incorporated in the design procedure.

Thus, a better control strategy was the gain-scheduled (GS) approach. In this method, linearized models of the aircraft, which would approximate the actual dynamics better in some local neighbourhood, at the specified operating points are obtained. Separate linear controllers, with desired stability and performance robustness in a local sense, are then designed for each linear model obtained earlier. These point designs are then 'stitched together' using a gain schedule to obtain the overall control law. Scheduling is heuristically done on parameters which i) vary slowly so that the actual plant may be considered quasi-steady, and ii) which capture the plant nonlinearities. Gangsaas et.al. [13] report practical applications of the LQG based gain-scheduled control law design. Adams et.al. [14] developed a a full envelope nonlinear control law for the longitudinal and lateral modes. Blight et.al. [15] design GS control law using LQG and structured singular value techniques to design for robust point designs. Shue et.al. [16] use a mixed  $H_2/H_\infty$  method for the point controller designs and schedule the controllers over the mach numbers. The main advantage of GS is that the wealth of linear control methods, performance measures, design intuition and computational tools may be used on the multi-variable nonlinear systems. However, the choice of the number of operating points and the point itself is not very well laid out, and therefore

the GS law has to be verified by extensive nonlinear simulation before it can be actually applied to an aircraft. Traditionally, this approach has been the most popular and widely used control law with both analog and digital versions of the method being used in various fighter aircrafts such as the Mirage 2000, and the F-16 among others. However, there have been notable failures also, for e.g. the JAS-39 and the YF-22 crashes [17, 18]. Shamma and Athans [19] discuss the application of this approach to non-linear plants. Shamma and Athans [20] point out some pitfalls of the method.

With the recent developments using differential geometric concepts in nonlinear control theory [21, 22], nonlinear inverse dynamics or feedback linearization based flight control design has been investigated by many researchers. The main advantage of the method was that it directly results in a global/ full-envelope control law. It also offers generality of application to different aircraft types. Smith and Meyer [23] used model inversion techniques to the aircraft control design problem treating the accelerations as pseudo-inputs. Lane and Stengel [24] used the method to decouple specific state variables that are of some particular interest to the pilots and used it to enhance stall prevention capabilities. They observed that 'Flight control systems based upon nonlinear inverse dynamics offer the potential of providing improved levels of safety and performance over conventional designs developed using linearizing assumptions'. Vukobratović and Stojić [25] discuss the centralized and decentralized control schemes using the inverse aircraft model. Singh [26] and Romano and Singh [27] design controllers for large nonlinear maneuvers of the aircraft. Durham et.al. [28] use a nonlinear model following approach to airplane control. Sun and Clarke [29] study auxiliary control devices, namely the flaps and spoilers for direct force control, for active control of the aircraft. Enns et.al. [17] apply the method to the F-18 HARV executing a Herbst maneuver.

However, this approach does not lead to an easy robustness analysis. This issue was addressed by using a multi-loop strategy with the inner loop performing the linearization of the unperturbed plant, and an outer loop was designed to take care of any uncertainties in the actual system. Adams and Banda [30] following the method



developed in [31] applied the structured singular value analysis to incorporate robustness in this approach. In another related work Sparks et.al. [32] use a gain-scheduled inner loop to obtain dynamic inversion. Enns et.al. [17] use loop shaping techniques to obtain robustness properties. An alternative method which uses a nonlinear discontinuous control law and offers attractive robustness properties, namely the sliding model control method, is next considered for this control design problem.

## 1.2 The Sliding Mode Control Method

The Sliding Mode Control (SMC) originated in the Soviet literature [33]. Some of the recent survey /review papers on this topic are Utkin [34], DeCarlo et.al. [35], and Hung et.al. [36]. They reflect the increasing interest of the control community in the method and report the developments and applications of the SMC to a myriad of control problems. The SMC design method involves two steps, i) the selection of a stable hyperplane in the state/error space on which motion should be restricted, called the sliding surface (SS), and ii) the synthesis of a control law which makes the selected surface attractive. In this method a trajectory, starting from a non-zero initial condition, evolves in two phases :

- A Reaching phase, in which it reaches the SS, and
- A Sliding phase, in which the trajectory on reaching the SS, remains there for all further times and thus evolves according to the dynamics specified by the SS.

The sliding surface specifies the dynamics in the second phase. Trajectories from any starting point can be shown to arrive at the SS in a finite time [37]. It has been shown that the trajectories on the SS exhibit invariance to unknown but bounded matched uncertainties and disturbances [21, 38]. This is achieved by using a switching/relay type of control law. However, the sliding motion commences only after the trajectory reaches the SS. Thus, to reap the benefits of the invariant response on the SS, it has been considered imperative to reduce the reaching time, i.e. the time spent in the first phase, and this has been traditionally used to select the controller parameters.

However, for a tracking task the quickness of response in terms of the time required to reach a small output tracking error (OTE) is of paramount interest and should be considered for the parameter selection. For the class of second order nonlinear systems, it is shown that a constant plus proportional rate reaching law as proposed in [37] offers a robust performance in the reaching phase also. Using this result, a new method of selection of controller parameters based on the time to OTE as the criterion is proposed. Simulations on two second-order mechanical systems show that the proposed parameter selection method takes substantially lower times to reach the OTE, while using similar levels of control effort, as compared with the selection method based on the traditional criterion of the reaching time.

The SMC method has been used to design controllers for various practical applications [36] including the aircraft FCS design. However, the method primarily applies to input affine systems, i.e. systems linear in the input, and has been applied to such systems. The SMC needs to be extended to tackle the presence of unmatched uncertainties and disturbances. Moreover, inputs to any practical system are generally generated by a dynamic actuation system and hence a discontinuous control law is not readily implementable. These issues need to be properly addressed for the method to gain more acceptance among the practising engineers and find more practical applications. The present work attempts to study these factors as related to an aircraft FCS design problem.

### 1.3 Application of SMC to Flight Control Design

The SMC, with its robustness properties, is an attractive alternate method for the aircraft flight control design problem. However, its application to the FCS design has been rather slow to pick up as is indicated by the method finding no application in the special issue of the *International Journal of Control* on aircraft flight control design [17, 39]. Calise and Kramer [40] were among the pioneers to adopt the SMC method for designing the FCS. They considered the linearized dynamics of the AV-8A Harrier in a hover mode under matched uncertainties. Singh [41] designed control laws for

large simultaneous longitudinal and lateral maneuvers of aircraft with linearized aerodynamics and matched uncertainty. Hedrick and Gopalswamy [42] reported the pitch axis control system design with nonlinear dynamics and linearized aerodynamics under matched uncertainty. They also considered various response criteria as developed by HQ engineers. Thukral and Innocenti [43] consider a linear model for the longitudinal problem. They consider the stabilization and tracking problems. Fossard [44] coupled the SMC with model following for the helicopter problem.

The above cited works model the nonlinear aircraft at best as an input affine system as the SMC technique is easily applied to such systems. However, the aircraft system of equations is known to be nonlinear in the states as well as the inputs [10]. Also, the number of independent inputs limit the number of outputs that may be exactly tracked. Thus the use of CFC surfaces, which is basically intended to control the three moments, imposes a fundamental limit on the number of tracked outputs. If, however, independent control of all the accelerations or equivalently the complete force-moment vector is possible, then these may be treated as pseudo-inputs, and the assumption of input affineness remains valid. It also increases the number of trackable outputs. Smith and Meyer [23] considered the accelerations as pseudo-inputs to the aircraft system. However, their design did not include robustness properties. Franklin [39] uses the forces as input for the low speed longitudinal landing control problem. Since, the generated forces depend on the bounded (with estimate of the bounds known) but uncertain time-varying inertia properties, the forces and moments have been treated as inputs to the aircraft system in this work, and is thus called the force control approach (FCA). To realize the forces as desired by the controller, appropriate control effectors are assumed to be present. With TV-FCS gaining popularity [6, 9, 45] independent control of the forces and moments affecting the motion is a feasible assumption. In fact flight tests on unmanned scaled fighter models have shown the practicality of a pure TV-FCS [46]. It is however observed that a proper mix of the CFC surfaces and TV leads to maximized safety agility and controllability levels. Presence of more alternatives, via the CFC surfaces, may be used to advantage by choosing control surface deflections that also

perform the CCV functions such as maneuver load control [2, 4]. This inverse problem of control allocation is being actively pursued in various development projects [7]. The constrained control allocation problem has been considered by Durham [47, 48]. The control surface deflections thus selected, on application to the airframe, are expected to generate the desired forces and moments. However, in practice the actually generated force vector would be different from its desired values, because of various reasons including the unsteady uncertain aerodynamics and the generally neglected aeroelastic effects. This discrepancy between the desired and the actually generated force vector has been modeled as a bounded multiplicative uncertainty in this study.

The explicit model following (MF) approach has been used to design the FCS. It offers many advantages. Firstly it facilitates the incorporation of various flight modes for different operational requirements. The HQs of an aircraft may be easily optimized by varying the models in-flight. One of its biggest advantages is that simulators can be widely used to train pilots with obvious advantages. In this work, a MF-SMC based full-envelope controller design for the nonlinear longitudinal dynamics of an aircraft has been done under matched uncertainties as is considered in almost all of the above cited works. A practical system however would not readily satisfy this assumption, and this is considered next.

### 1.3.1 The Unmatched Uncertainty Case

As seen earlier, there is a limit on the number of outputs that can be exactly tracked. The control of the remaining states is however still desirable. This was attempted by making use of the fact that there is a significant difference in time scales between the fast and slow states of an aircraft [49, 50]. In this multi-loop (ML) approach, a dynamic inversion based control law was synthesized for the slow states treating the fast states as the the input for the outer loop. Then an inner loop control law is designed so that the fast states actually track the command signals generated in the outer loop. Snell et.al. [49] report that better responses are obtained with this ML strategy as compared to the conventional gain-scheduled control law. The robustness of the control law was

however not dealt with. An integral error feedback in the outer loop was introduced by Azam and Singh [50] to obtain robustness while using a similar control structure.

As seen earlier, the SMC law guarantees invariance against the matched uncertainties and disturbances only, however, the presence of unmatched disturbances and uncertainties is not uncommon in practical systems. This would adversely affect the intended system performance. Design of control laws for the unmatched uncertainty case has been considered by many researchers [51–53] under various assumptions on the types of mismatch. In this work, the ML strategy is extended to include the effects of unknown but bounded unmatched uncertainties. The propagation of disturbances and uncertainties, from the outer to the inner loops, in this approach is worked out. Using the ML approach, a SMC law is developed for a general multi-input (MI) mechanical system under unmatched uncertainty and applied to the nonlinear longitudinal aircraft dynamics. The ultimate boundedness of the position and velocity tracking errors is established and the associated bounds are calculated as functions of the selected controller parameters. This can thus serve as a guideline for their selection. Application of the ML analysis, to a third order nonlinear system with unmatched uncertainties and disturbances, shows that conventional SMC design procedure, with a new method of selection of the gain of the switching term, may still be applied to tackle unmatched uncertainty. The ultimate boundedness of the errors in the various loops is established.

### 1.3.2 SMC with Input Dynamics

The switching control law as used by SMC is not practically feasible as it would require an infinite switching frequency to achieve the 'ideal' sliding. However, in practice any actuation system will have a finite bandwidth and delays resulting in 'real' sliding [54, 55]. Thus the invariance property is in effect lost and motion within some boundary of the SS can be guaranteed. This leads to the high frequency chattering effects which may excite the high frequency unmodeled dynamics in the system. To circumvent this difficulty, researchers have used two approaches i) use of continuous approximations of the discontinuous control law [21, 56], and ii) application of higher

order sliding methods [54, 55]. The control law then results in a continuous control law with discontinuities in the input rates. Ramirez and coworkers [57–59] using a differential algebraic approach construct input dependent sliding surfaces, and obtain similar results. The higher order sliding methods require higher order derivatives of the states and thus of the disturbances and uncertainties. This complicates the analysis of robustness properties, as the propagation of disturbances and uncertainties through the time derivatives is not very straight forward [60].

In this work, the input is considered to be the output of a first order actuator system. The ML strategy as discussed earlier is extended to address this problem. The propagation of disturbances and thus the robustness issues are more simply dealt with in the developed procedure. The method is first developed for a single input (SI) nonlinear system and ultimate boundedness of the state and the input errors are established. It is then applied to the MI aircraft velocity tracking problem with unmatched uncertainties. The position, velocity and input errors in the various loops are shown to be ultimately bounded. A parametric study of the involved feedback gains is required for their proper selection.

## 1.4 Organization of the Thesis

In this thesis, the aircraft control design problem using the SMC approach has been considered. Chapter 2 considers the design of a constant plus proportional rate reaching law based SMC design for second order mechanical systems. A method of selection of parameters for the SMC which results in lower times to an acceptable level of OTE is proposed. Simulation results obtained for a single input (SI) nonlinear spring-mass-damper and a two input two-link robot problems verify the method. Chapter 3 introduces the aircraft longitudinal dynamics and the force control approach. A MF-SMC based full-envelope controller design for the nonlinear longitudinal dynamics of a fighter aircraft has been done under the assumption of matched uncertainty. The desired model responses are obtained from a linear aircraft model given in Appendix D. The aircraft parameters, the assumed disturbances and uncertainties used in the

simulation are also given there. Analytical control laws for two operational modes, namely i) the Velocity Tracking Mode, and ii) the Trimming Mode, are derived for the case of matched uncertainty. A ML strategy is used to develop a SMC design procedure in the case of unmatched uncertainty in Chapter 4. Results of numerical simulation for the aircraft in the velocity tracking mode ascertain the robustness properties. This approach is then applied to SI higher order systems. Synthesis of a SMC law with first order input dynamics is discussed in Chapter 5. The method is first developed for the SI nonlinear spring-mass problem. Simulation results are presented to verify the feasibility of the approach. The design procedure is then applied to the MI aircraft problem. Simulation results for the velocity tracking mode with unmatched uncertainties are presented. Conclusions and scope of further research form Chapter 6.

# Chapter 2

## Design of Proportional plus Constant Rate Reaching Law SMC for Second-order Systems

### 2.1 Introduction

Many mechanical systems are modeled as second order systems e.g. as in the trajectory following robots, or the angular position control in aircrafts as nose pointing or pitch hold autopilots. Other examples include the classical inverted pendulum, or the antenna pointing of satellites among others. The SMC method has been used for many such applications as is evident from [36, 37]. Thus it is of particular interest to study the effect of the SMC parameters for this class of systems. As discussed earlier the sliding motion, and thus the invariant performance, occurs only after the trajectory reaches the SS, while the tracking behaviour in the reaching phase depends on the uncertainties. Thus, a smaller reaching time would imply that sliding begins earlier and this has been conventionally used to select the SMC parameters.

Gao and Hung [37] proposed a reaching law method which specifies the error dynamics in the reaching phase. They suggested three structures- the constant rate reaching, constant plus proportional rate, and the power rate reaching. The time taken to reach the SS is also evaluated. By appropriately selecting parameters the dynamic quality of the SMC system can be controlled. Choi et al. [61] suggest the use of a stepwise



time-varying SS, in which the SS is shifted and/or rotated as a function of time. They applied this method to a non-linear spring mass damper system and reported a handsome decrease in time to achieve zero tracking error. However, the resulting controller is cumbersome to implement because the parameters of the SS need to be calculated at different time instants. Bartoszewicz [62] proposed a continuously time-varying SS that gives still faster tracking. The choice of the time varying SS is extended in [63] so as to minimize the integral of the absolute error. However, the parameter selection is dependent on the initial error conditions.

In this chapter a study on the design of constant plus proportional rate reaching law for second order systems is done. Using Lyapunov theory, it is shown that the constant plus proportional rate reaching law imposes a second-order dynamics on the error variables, and thus guarantees a robust performance in the reaching phase also. The selection of controller parameters based on minimizing the reaching time is shown to be inadequate with regard to the time to reach a small output tracking error (OTE). A new method of the selection of the control law parameters based on the criterion of time to a specified OTE is proposed. To illustrate the method, it is applied to a nonlinear spring mass problem taken from Choi et al. [61] and a two-input two link robotic arm trajectory following problem [37]. Simulation results show that, for similar peak levels of control effort, considerably faster tracking performances are obtained for control laws designed using the proposed method.

## 2.2 The Reaching Law based SMC Design Method

Consider a single input, second order input-affine non-linear system of the form

$$\ddot{x} = f(x, \dot{x}) + g(x, \dot{x})u + d_f \quad (2.1)$$

where  $u$  is the control input, and  $d_f$  represents the bounded uncertainties and external disturbances, with  $|d_f| < D$ . Since the uncertainties and/or disturbances which are in the range space of the input are called matched, it is obvious that any uncertainty entering in the scalar system as given above is matched. The arguments of  $f$  and  $g$  are

dropped from now on for brevity. The uncertainty in the input distribution function  $g$  is expressed as  $g = \hat{g}(1 + \tilde{g})$ , where  $\hat{g}$  represents its nominal value, and  $\tilde{g}$  is bounded, i.e.,  $|\tilde{g}| < G < 1.0$ .

Defining the state variables as  $x_1 = x$  and  $x_2 = \dot{x}$ , (2.1) can be written in the state space form as

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} x_2 \\ f + gu + d_f \end{pmatrix}. \quad (2.2)$$

Let the trajectory to be followed (desired trajectory) be given as  $x_{1d}$  and  $x_{2d} = \dot{x}_{1d}$ . Then the error between the actual and the desired trajectories can be expressed as  $e = x_1 - x_{1d}$  and  $\dot{e} = x_2 - x_{2d}$ . In vector form,

$$\begin{pmatrix} e \\ \dot{e} \end{pmatrix} = \begin{pmatrix} x_1 - x_{1d} \\ x_2 - x_{2d} \end{pmatrix}. \quad (2.3)$$

Let  $y = (e, \dot{e})^T$ , where the superscript  $T$  denotes the transpose. Taking the time derivative of the above equation and using (2.2) results in the dynamics

$$\dot{y} = \begin{pmatrix} \dot{e} \\ f + gu + d_f - \ddot{x}_{1d} \end{pmatrix}. \quad (2.4)$$

The switching function  $s$  for second order systems is conventionally defined as a combination of the errors in (2.3) [21, 37] as

$$s = \dot{e} + \alpha e, \quad (2.5)$$

where,  $\alpha > 0$  sets the dynamics in the sliding mode. The SS selected above should be made attractive so that trajectories starting from a non-zero value of  $s$  approach the SS, and then stay on  $s = 0$  for all future time instants. For this, using  $\ddot{e}$  from (2.4), the time derivative  $\dot{s}$  is obtained from (2.5) as

$$\begin{aligned} \dot{s} &= \ddot{e} + \alpha \dot{e}, \text{ or} \\ &= f + gu + d_f - \ddot{x}_{1d} + \alpha \dot{e}, \\ &= f + \hat{g}(1 + \tilde{g})u + d_f - \ddot{x}_{1d} + \alpha \dot{e}. \end{aligned} \quad (2.6)$$

The input  $u$  remains to be chosen so as to make  $s$  go to zero for sliding. The normal procedure for its selection [21] is to express the input  $u$  as a sum of two terms. The first term is chosen, using the nominal plant parameters, so as to make  $\dot{s} = 0$ , when  $s = 0$ , and is called the equivalent control. The second term is then chosen to tackle the uncertainties in the system. Note that in (2.6)  $\hat{g}$  is the nominal  $g$ . Thus, the first term of  $u$  is chosen to cancel out the known terms in the right hand side of (2.6) and is seen to be  $\hat{g}^{-1}(\ddot{x}_{1d} - f - \alpha\dot{e})$ . The second term is selected as  $\hat{g}^{-1}(-\epsilon s - K\text{sgn}[s])$  to introduce stabilizing terms in the  $s$  dynamics (2.6). The complete  $u$  thus becomes

$$u = \hat{g}^{-1}(\ddot{x}_{1d} - f - \alpha\dot{e} - \epsilon s - K\text{sgn}[s]), \quad (2.7)$$

where,  $\epsilon, K > 0$  are positive real numbers to be selected, and  $\text{sgn}[\cdot]$  is the *signum* function. It is established later on in this section that the above control law actually imposes a constant plus proportional rate reaching law [37]. Note that the  $u$  in the above equation may be simplified by using the definition of  $s$  in (2.5) and defining  $a$  and  $b$  as

$$\begin{aligned} a &= \alpha\epsilon, \text{ and} \\ b &= \alpha + \epsilon, \end{aligned} \quad (2.8)$$

both of which are obviously positive real numbers. Thus  $u$  becomes

$$u = \hat{g}^{-1}(\ddot{x}_{1d} - f - ae - b\dot{e} - K \text{sgn}[s]). \quad (2.9)$$

Using this  $u$  in (2.6) and substituting  $g = \hat{g}(1 + \tilde{g})$  gives

$$\begin{aligned} \dot{s} &= f + g\hat{g}^{-1}(\ddot{x}_{1d} - f - ae - b\dot{e} - \epsilon s - K \text{sgn}[s]) + d_f - \ddot{x}_{1d} + \alpha\dot{e} \\ &= \tilde{g}(\ddot{x}_{1d} - f - ae - b\dot{e}) - (ae + b\dot{e}) - (1 + \tilde{g})K\text{sgn}[s] + d_f + \alpha\dot{e} \\ &= -ae - (b - \alpha)\dot{e} + \tilde{g}(\ddot{x}_{1d} - f - ae - b\dot{e}) - (1 + \tilde{g})K\text{sgn}[s] + d_f. \end{aligned} \quad (2.10)$$

Let

$$R = \ddot{x}_{1d} - f - ae - b\dot{e}. \quad (2.11)$$

Using  $R$  as above,  $a$  and  $b$  as defined in (2.8), and  $s$  from (2.5),  $\dot{s}$  in (2.6) may be simplified to get

$$\dot{s} = -\epsilon s + \tilde{g}R - (1 + \tilde{g})K \operatorname{sgn}[s] + d_f, \text{ or} \quad (2.12)$$

$$s\dot{s} = -\epsilon s^2 + s(\tilde{g}R + d_f) - (1 + \tilde{g})K|s|. \quad (2.13)$$

The scalar  $K$  should be chosen so that  $\dot{s}$  above satisfies a constant plus proportional rate reaching law [37] as

$$\dot{s} = -\epsilon s - \eta \operatorname{sgn}[s], \text{ or} \quad (2.14)$$

$$s\dot{s} = -\epsilon s^2 - \eta|s|, \quad (2.15)$$

where,  $\eta$  is a positive real number to be selected later. For  $s\dot{s}$  in (2.13) to satisfy the above equation,  $K$  should be chosen large enough so that  $-(1 + \tilde{g})K|s|$  in (2.13) always dominates the  $s(\tilde{g}R + d_f)$  and in the worst case,  $-(1 + \tilde{g})K|s| + s(\tilde{g}R + d_f)$  is at least  $-\eta|s|$ . Thus  $K$  may be selected [21] as

$$K = \frac{G|R| + D + \eta}{1 - G}. \quad (2.16)$$

For this choice of  $K$ , it may be easily seen that the  $-(1 + \tilde{g})K|s| + s(\tilde{g}R + d_f)$  term in (2.13) is always  $\leq -\eta|s|$ . The term may thus be equivalently written as  $-\eta'|s|$  where  $\eta' \geq \eta$ . The  $s\dot{s}$  in (2.13) thus becomes

$$s\dot{s} = -\epsilon s^2 - \eta'|s|, \text{ or} \quad (2.17)$$

$$\dot{s} = -\epsilon s - \eta' \operatorname{sgn}[s]. \quad (2.18)$$

It may be easily established for the  $s$  dynamics above that  $s = 0$  is the only stable equilibrium point. The control law (2.9) is thus seen to satisfy the above reaching condition, i.e. it makes the  $s = 0$  plane an attractive surface. It can be easily shown that the  $s$  dynamics as above will have better decay characteristics (See Appendix A) than the reaching law specified in (2.14). Furthermore, estimates of the reaching time i.e. the time to reach the SS ( $s = 0$ ) may be evaluated using (A.7). Note that  $\eta'$  as defined above can be shown to be bounded with a maximum possible value of  $\eta_M = \eta + 2K$ . The effect of the controller parameters, namely the positive scalars  $\alpha$ ,  $\epsilon$  and  $\eta$  are next studied.

## 2.3 Selection of SMC Parameters

In this section a method of selection of the parameters in  $u$  (2.9) is proposed. Using  $s$  from (2.5), and  $\dot{s} = \ddot{e} + \alpha\dot{e}$  from (2.6), (2.18) may be rewritten as

$$\ddot{e} = -\alpha\epsilon\dot{e} - (\alpha + \epsilon)\dot{e} - \eta'\text{sgn}[s], \text{ or} \quad (2.19)$$

$$\ddot{e} = -ae - b\dot{e} - \eta'\text{sgn}[\dot{e} + \alpha e], \quad (2.20)$$

with  $a$  and  $b$  as defined in (2.8).

With this, the  $y$  dynamics in (2.4) may be rewritten as

$$\dot{y} = Ay + \bar{q} \quad (2.21)$$

where,

$$A = \begin{bmatrix} 0 & 1 \\ -a & -b \end{bmatrix}, \quad (2.22)$$

and,

$$\bar{q} = \begin{pmatrix} 0 \\ -\eta'\text{sgn}[s] \end{pmatrix}. \quad (2.23)$$

With  $a$  and  $b$  defined as in (2.8), the  $A$  matrix above is seen to have its poles at  $-\alpha$  and  $-\epsilon$ . These poles govern the response of the linear homogeneous part (i.e. the  $A$ -dynamics). Conventionally, these are selected to achieve a desired error response and lower reaching times. Also, the choice of  $\alpha$  in (2.5) gives the rate of error decay in the SS. Note that  $K$  specifies the magnitude of the discontinuity in the control law in (2.9). The value of  $K$  in (2.16) is seen to increase with an increase in  $\eta$ . A higher value of  $\eta$  leads to smaller reaching times as discussed in Appendix A and has been shown to give rise to more chattering [37].

Next the effect of the  $\alpha$  and  $\epsilon$  parameters on the tracking performance is studied. This is done using the Lyapunov approach. A candidate Lyapunov function  $V$  for the  $y$  dynamics as specified in (2.21) is selected as

$$V(y) = y^T P y \quad (2.24)$$

where,  $P$  is a positive definite symmetric matrix and is taken as

$$P = \begin{bmatrix} \alpha^2 + \beta & \alpha \\ \alpha & 1 \end{bmatrix}, \quad (2.25)$$

and,  $\beta > 0$  guarantees the positive definiteness of the  $P$  matrix. The time derivative of  $V(y)$  may be obtained as

$$\dot{V} = \dot{y}^T P y + y^T P \dot{y}. \quad (2.26)$$

Using (2.21) in the above equation gives on simplification

$$\dot{V} = y^T [A^T P + P A] y + 2y^T P \bar{q}. \quad (2.27)$$

Since  $A$  in (2.22) is a Hurwitz matrix, it satisfies the Lyapunov equation

$$A^T P + P A = -Q \quad (2.28)$$

where, the  $Q$  can be derived from the above equation using  $A$  and  $P$  as given in (2.22) and (2.25) as

$$Q = \begin{bmatrix} 2\alpha^2\epsilon & 2\alpha\epsilon - \beta \\ 2\alpha\epsilon - \beta & 2\epsilon \end{bmatrix}. \quad (2.29)$$

Note that positive definiteness of  $Q$  is guaranteed if

$$\beta < 4\alpha\epsilon. \quad (2.30)$$

From  $\bar{q}$  and  $P$  as defined in (2.23) and (2.25) respectively, the  $y^T P \bar{q}$  is seen to be equal to  $-s\eta' \text{sgn}[s]$ . Using this and  $Q$  as obtained above in (2.29),  $\dot{V}$  in (2.27) may be simplified to

$$\begin{aligned} \dot{V} &= -y^T Q y - 2s\eta' \text{sgn}[s], \text{ or} \\ &= -y^T Q y - 2\eta' |s|, \end{aligned} \quad (2.31)$$

which is seen to be always negative definite. Thus, the stability of  $e$  dynamics in (2.21) or equivalently in (2.20) is guaranteed. To study the time decay performance of  $V$  in the above equation, the following result is required.

**Claim 1** *For the second order error dynamics as given in (2.19), a Lyapunov function may be selected as in (2.24). For the  $Q$  matrix in (2.29), as obtained from the Lyapunov equation (2.28), there exists a positive real number  $\delta > 0$  such that*

$$Q = \delta P + H, \quad (2.32)$$

where  $H$  is at least a positive semi-definite matrix.

**Proof:** It can be easily shown by a constructive proof that for the system under consideration, there is always a range of values that  $\delta$  can take. The detailed proof is presented in the Appendix B. In particular, it is established that permissible range of values of  $\delta$  lies in an open set and is given by  $\delta \in (0, \min[2\alpha, 2\epsilon])$ , where  $\min[\cdot, \cdot]$  gives the minimum of its arguments. ■

Using the decomposition of  $Q$  as in (2.32), the  $\dot{V}$  in (2.31) may be rewritten as

$$\begin{aligned} \dot{V} &= -y^T[\delta P + H]y - 2s\eta' \text{sgn}[s], \text{ or} \\ &= -\delta V - y^T H y - 2\eta'|s|. \end{aligned} \quad (2.33)$$

From the developments in Appendix A, it follows that the  $V$  decay response of the above system will be better than the response of the system described by

$$\dot{V} = -\delta V. \quad (2.34)$$

It is interesting to find out the  $A_b$  matrix with the dynamics specified as

$$\dot{y} = A_b y, \quad (2.35)$$

that satisfies (2.34). The  $A_b$  should thus satisfy the Lyapunov equation (2.28) with the  $P$  as selected in (2.25), i.e.  $A_b^T P + P A_b = -\delta P$ , for some feasible choice of  $\delta > 0$  as in (2.34). For this, the general form of the  $A_b$  matrix is taken as

$$A_b = \begin{bmatrix} 0 & c' \\ -a' & -b' \end{bmatrix}, \quad (2.36)$$

where,  $a', b', c'$  are to be determined. The Lyapunov equation for  $A_b$  matrix as given above is solved for these unknowns for a general value of  $\delta$ . These may be easily obtained by the solution of a set of simultaneous linear equations in  $a', b', c'$  as

$$\begin{aligned} a' &= \frac{\delta(\alpha^2 + \beta)}{2\alpha} \\ b' &= \delta \\ c' &= \frac{\delta}{2\alpha}. \end{aligned} \quad (2.37)$$

It is known that (see Appendix B)  $\delta$  can take values as large as  $2\epsilon$  or  $2\alpha$ , in the limit as  $\beta \rightarrow 0$ , depending on whichever is smaller. Using (2.37), the  $A_b$  matrix for  $\delta = 2\alpha$  may be obtained as

$$A_b = \begin{bmatrix} 0 & 1 \\ -(\alpha^2 + \beta) & -2\alpha \end{bmatrix}, \quad (2.38)$$

and is seen to have both of its poles at  $-\alpha$ , for  $\beta = 0$ . Similarly, for  $\delta = 2\epsilon$ , the  $A_b$  matrix becomes

$$A_b = \begin{bmatrix} 0 & \epsilon/\alpha \\ -(\epsilon\alpha + \epsilon\beta/\alpha) & -2\epsilon \end{bmatrix}, \quad (2.39)$$

and for  $\beta = 0$ , both the poles of the above  $A_b$  matrix are easily seen to lie at  $-\epsilon$ . It follows from Appendix A that the decay of the Lyapunov function (2.24) as obtained in (2.33), i.e. for the dynamics in (2.21) with the  $A$  matrix in (2.22) having its poles as  $-\alpha$  and  $-\epsilon$ , is guaranteed to be better than the decay response in (2.34), which is achievable by a  $A_b$  matrix as selected in (2.38) or (2.39) which has both of its poles at  $-\min[\alpha, \epsilon]$ . This implies that the error dynamics in (2.21) in the reaching phase is bounded by the response of the second order  $A_b$  dynamics in (2.35) and a robust performance in the presence of the matched uncertainties and disturbances is achievable even before the onset of sliding. Estimates of the guaranteed times to reach the OTE may be obtained using the  $A_b$  dynamics. It is obvious that shorter times to the OTE are expected as both  $\alpha$  and  $\epsilon$  are increased. However, the control law in (2.9) will also require larger control magnitudes as  $a$  and  $b$  will also increase as can be seen from (2.8). Next the effect of the relative values of these parameters is considered.



### 2.3.1 The Relative Choice of $\alpha$ and $\epsilon$

Let the poles of the  $A$  matrix in (2.22) be selected as  $-p$  and  $-q$ , where  $p$  and  $q$  are positive real numbers satisfying  $p > q$ . This could be achieved in the following two ways:

- **Case  $CP$ :**  $\alpha = p$  and  $\epsilon = q$ . This would result in the SS being  $\dot{e} + pe$ , say  $S_p$ .
- **Case  $CQ$ :**  $\alpha = q$  and  $\epsilon = p$ , with which the SS becomes  $\dot{e} + qe$ , say  $S_q$ .

It follows from (2.8) that  $a = pq$  and  $b = p + q$  remain the same in both the cases resulting in the same  $A$  matrix in (2.22). With  $a$  and  $b$  being the same,  $R$  in (2.11) and thus  $K$  (2.16) are expected to have comparable magnitudes for both the cases. Thus the peak values of the control effort  $u$  in (2.9) should also be nearly equal. The performance obtained in the two cases is compared next. For this, a common Lyapunov function is first constructed as follows.

**Claim 2** *Let  $P$  and  $Q$  be symmetric positive definite matrices as specified in (2.25) and (2.29) respectively, for the Case  $CP$ , i.e.  $\alpha = p$  and  $\epsilon = q$ . Then, there exists a sufficiently large positive scalar  $M$  such that*

$$V(y) = y^T P y + M|S_p| + M|S_q| \quad (2.40)$$

where,  $y = (e, \dot{e})^T$ , is a valid common Lyapunov function for Cases  $CP$  and  $CQ$ .

**Proof:** For  $V$  to be a Lyapunov function, at least negative semi-definiteness (n.s.d.) of its time derivative must be established for the two cases. Detailed derivations are given in the Appendix C. Let  $\dot{V}_i$ ,  $i = p, q$  represent the time derivative  $\dot{V}$  of the Lyapunov function in (2.40) for the cases denoted by the subscript 'i'. The  $\dot{V}_p$  has been derived in (C.6) - (C.9) for the Case  $CP$  and  $\dot{V}_q$  in (C.12) - (C.17) for the Case  $CQ$  respectively. The negative definiteness of the time derivatives in the two cases is shown for a choice of  $M$  as in (C.19). ■

The discussion in the Appendix C shows that (C.6) - (C.9) giving  $\dot{V}_p$  for the Case  $CP$  may be combined to give the time derivative as in (C.10). Similarly (C.20) gives

$\dot{V}_q$  for the Case  $CQ$ . Further, for the Case  $CQ$ , it is shown in the Appendix C that there exists a  $0 < \delta_q < q$  ( $< p$  by selection), using which  $\dot{V}_q$  in (C.20) may be rewritten as

$$\dot{V}_q \leq -y^T Q y - \delta_q M[|S_q| + |S_p|] - (p - \delta_q) M |S_q|. \quad (2.41)$$

From Claim 1, it is known that the  $Q$  matrix may be decomposed as given in (2.32) as  $Q = \delta_q P + H_q$ , where  $H_q$  is a positive definite matrix, since  $\delta_q < q < \min[2q, 2p]$ . Using this decomposition, the  $\dot{V}_q$  above may be expressed as

$$\begin{aligned} \dot{V}_q &\leq -\delta_q y^T P y - y^T H_q y - \delta_q M[|S_q| + |S_p|] - (p - \delta_q) M |S_q|, \text{ or} \\ &\leq -\delta_q V_q - (p - \delta_q) M |S_q|, \end{aligned} \quad (2.42)$$

using the definition of  $V$  in (2.40) where the subscript ' $q$ ' represents the Case  $CQ$ . As  $p > q > \delta_q$ , the  $(p - \delta_q) M |S_q|$  term in the above equation is always non-negative, and thus the results of Appendix A imply that the  $V_q$  decay response of this system will be better than the exponential decay response offered by

$$\dot{V}_q = -\delta_q V_q, \text{ where } \delta_q \in (0, q). \quad (2.43)$$

Note that  $\delta_q$  can assume a maximum value of  $\bar{\delta}_q = q$  in the limit.

For the Case  $CP$ , the  $\dot{V}_p$  is seen from (C.10) to be given as

$$\dot{V}_p \leq -y^T Q y - M[q|S_p| + p|S_q|] - 2\eta'|S_p|. \quad (2.44)$$

The  $Q$  matrix in this case is decomposed as  $\delta_p P + H_p$ , where  $0 < \delta_p < 2q = \min[2q, 2p]$  has to be found out. Following the steps as for the Case  $CQ$ , the  $\dot{V}_p$  above may be rewritten as

$$\begin{aligned} \dot{V}_p &\leq -\delta_p V_p - y^T H_p y - (p - \delta_p) M |S_q| - (q - \delta_p) M |S_p| - 2\eta'|S_p|, \text{ or} \\ &\leq -\delta_p V_p - y^T H_p y - (p - \delta_p) M |S_q| - (q - \delta_p + \frac{2\eta'}{M}) M |S_p|. \end{aligned} \quad (2.45)$$

Thus, it is seen that if  $\delta_p < \min[p, q + \frac{2\eta'}{M}]$ , then the  $(p - \delta_p) M |S_q| + (q - \delta_p + \frac{2\eta'}{M}) M |S_p|$  term in the above equation is always guaranteed to be non-negative. As discussed in

the Appendix C, the condition on  $M$  for  $V_p$  to be a Lyapunov function is  $M \geq 0$ . For  $M \rightarrow 0$ , the  $2\eta'/M$  term will increase, However, since the decomposition in (2.32) is possible only for  $\delta_p < 2q = \min[2q, 2p]$ , the  $\delta_p$  may be selected to be smaller than  $\min[p, 2q]$ . It thus follows that the  $V_p$  decay response of the above system will be better than the response of the system given by

$$\dot{V}_p = -\delta_p V_p, \text{ where } \delta_p \in (0, \min[p, 2q]). \quad (2.46)$$

Thus the upper limiting value of  $\delta_p$  is seen to be given by  $\bar{\delta}_p = \min[p, 2q]$ . Thus it is obvious that  $\bar{\delta}_p > \bar{\delta}_q$ .

With the guaranteed decay responses of  $V_q$  and  $V_p$  being given as in (2.43) and (2.46) respectively, it is clear that Case  $CP$  guarantees a faster exponential decay of the Lyapunov function (2.40) as compared to the Case  $CQ$ . These guaranteed decay performances may be used to develop an estimate of the time to reach a specified level of OTE in terms of the Lyapunov function. Thus, given an initial value  $V(0)$  at  $t = 0$ , the time  $t_f$  required for  $V_i$ ,  $i = q, p$  dynamics, in (2.43) and (2.46) respectively, to decay to a final value of  $V_f$  may be evaluated as

$$t_f = \frac{1}{\bar{\delta}_i} \ln \left[ \frac{V(0)}{V_f} \right], \quad (2.47)$$

where,  $i = q, p$ , and  $\bar{\delta}_i$  are as defined earlier and represent the maximum limiting value of  $\delta_i$  for the  $\delta_q$  and  $\delta_p$  as given in (2.43) and (2.46) respectively. For the same  $V(0)/V_f$ , it is obvious that  $t_f$  in the Case  $CP$  will be smaller than in the Case  $CQ$ , as the right hand side of the above equation will be smaller because of the fact that  $\bar{\delta}_p > \bar{\delta}_q$ . The  $t_f$  in (2.47) gives conservative estimates for the decay of the Lyapunov function. The actual times  $t_{OTE}$  required, for the  $V$  decay responses in (2.42) and (2.45) for the Cases  $CQ$  and  $CP$  respectively, to reach the  $V_f$  are expected (see Appendix A) to be smaller than the  $t_f$ , i.e.  $t_{OTE} \leq t_f$ . Thus the  $\alpha$  and  $\epsilon$  parameters should be selected as in the Case  $CP$  to have a smaller value of  $t_f$ , i.e. for a given choice of the poles of the  $A$  matrix in (2.22),  $\epsilon$  should be selected as the magnitude of the dominant pole, and  $\alpha$  as the magnitude of the other, or simply  $\alpha > \epsilon$ . This is summarized as follows.

**Lemma 1** *The choice of  $\alpha$  and  $\epsilon$  parameters, for the constant plus proportional rate reaching SMC law as in (2.9), with  $a$  and  $b$  selected as in (2.8) and the sliding surface as in (2.5), such that*

$$\alpha > \epsilon. \quad (2.48)$$

*guarantees a faster decay of the Lyapunov function (2.40).*

Note that the above lemma indicates that the choice of  $\alpha$  and  $\epsilon$  as in (2.48) only ensures that  $t_f$  will be smaller. It however does not guarantee that the  $t_{OTE}$  for the Case  $CP$  will be smaller than the Case  $CQ$ , although it is so expected and can actually be seen from the simulation results presented in the next section. There may however be parameter combinations where this would not hold.

A smaller value of  $V$  implies a smaller tracking error in the sense of the norm (as defined by the Lyapunov function). Thus, since the Case  $CP$  has a faster guaranteed decay performance, it is expected to take lesser times as compared to the Case  $CQ$  to reach an acceptably small OTE. As discussed earlier, the control effort is expected to be almost the same for both the  $CP$  and  $CQ$  cases. Note that, lower reaching times correspond to the case of  $\epsilon > \alpha$  (Case  $CQ$ ) as can be seen from the results in the next section. However, the above theoretical developments show that shorter times to a desired OTE are expected for the cases where  $\alpha > \epsilon$  (Case  $CP$ ). The estimates of the time to the OTE using (2.47) showing the effect of the relative choices of  $\alpha$  and  $\epsilon$  as suggested in Lemma 1 are verified by applying the design method to two mechanical systems. The systems and the obtained simulation results are presented next.

## 2.4 Simulation Results

For the illustration of the proposed SMC design method, the results presented in the previous section have been used to design controllers for two practical problems. The numerical results of these examples ascertain the validity of Lemma 1.

### 2.4.1 Nonlinear Spring Mass Damper System

The first example concerns a non-linear mass-spring-damper system from Choi et. al. [61]. The governing differential equation is

$$m\ddot{x} + \nu(\dot{x}, t) + \mu(x, t) = u(t) + d(t), \quad (2.49)$$

where,  $x, \dot{x}$  represent the position and the velocity of the mass  $m$ ,  $u(.)$  represents the applied input force, and  $d(.)$  the disturbance signal.  $\nu(.,.)$  and  $\mu(.,.)$  represent the damping and spring force term respectively. The system parameters and functions are given to be  $m = 1$ ,  $f = f_1 + f_2 + f_3 + f_4$ , which are given as  $f_1 = \mu_0 x$ ,  $f_2 = -\mu_1 x^3$ ,  $f_3 = -\nu_0 \dot{x}$ , and  $f_4 = -\nu_1 \dot{x}|\dot{x}|$  with  $\mu_0 = 0.5$ ,  $\mu_1 = 0.5$ ,  $\nu_0 = 0.3$ , and  $\nu_1 = 0.3$ . The system also has uncertainties expressed as  $a_1 f_1 + a_2 f_2 + a_3 f_3 + a_4 f_4$  with  $a_1 = -.05 + 0.25 \sin(5\pi t)$ ,  $a_2 = -.05 + 0.25 \sin(5\pi t)$ ,  $a_3 = -.05 + 0.15 \sin(7\pi t)$ , and  $a_4 = -.05 + 0.15 \sin(7\pi t)$  and disturbance  $d = 0.05 + 0.25 \cos(3\pi t)$ . The signal to be tracked is given by  $x_{1d} = -0.5 \cos(\pi t/5)$ . The above system in (2.49) may be expressed in standard form as in (2.1). The initial conditions are taken as 0.5 and 0 for the two states respectively.

Simulation was done using the fourth order Runge-Kutta method with a time step of 2.5ms. The remaining parameters were selected as  $\beta = 1$  and  $\eta = 1$ . Several combinations of  $\alpha$  and  $\epsilon$  were used.

- Case 1:  $\alpha = 2$  and  $\epsilon = 6$
- Case 2:  $\alpha = 6$  and  $\epsilon = 2$
- Case 3:  $\alpha = 3$  and  $\epsilon = 4$
- Case 4:  $\alpha = 4$  and  $\epsilon = 3$
- Case 5:  $\alpha = 4$  and  $\epsilon = 5$
- Case 6:  $\alpha = 5$  and  $\epsilon = 4$

**Table 2.1:** Comparison of time for OTE and Reaching: Example 1.

Case no.	$\alpha$	$\epsilon$	Time to OTE ( $< 1 \times 10^{-3}$ ) in (s)		Reaching time (s) (A.7)	$t_f$ (s) (2.47) for $\frac{V_0}{V_f} = 10^4$
			Bound obtained from $A_b$ dynamics (2.35)	Actual		
1	2	6	4.24	3.30	0.183	4.605
2	6	2	4.24	2.00	1.472	2.302
3	3	4	2.83	2.35	0.426	3.070
4	4	3	2.83	2.00	0.732	2.302
5	4	5	2.13	1.80	0.439	2.302
6	5	4	2.13	1.65	0.650	1.842

The time to OTE (defined as the time after which the error is less than  $1.0 \times 10^{-3}$ ) obtained for the bounding  $A_b$  dynamics in (2.35), the actual tracking times, the reaching times calculated from (A.7) and the  $t_f$  for  $V_0/V_f = 1.0 \times 10^4$  as evaluated from (2.47) for all the cases are presented in Table 2.1. It can be seen from the table that the actual time to achieve the OTE is appreciably smaller for Case 2 as compared with Case 1. The Table 2.1 also shows that similar results are obtained for Cases 4 and 6. In all these cases  $\alpha > \epsilon$ , thus verifying Lemma 1. It is noticed from Table 2.1 that, for all of these cases, the reaching time is greater than the corresponding Cases 1, 3 and 5. Although Cases 1,3 and 5 have smaller reaching times, they require about 65%, 17.5%, and 9.1% more time to the OTE than the time required by the Cases 2,4, and 6 respectively. Thus, from the table it is clearly evident that parameter selections giving lower reaching times actually take longer times to reach the specified OTE. Moreover, the time bounds  $t_f$  calculated from (2.47) are seen to be better than those obtained from the  $A_b$  dynamics (2.35) in the sense of being able to bring out the effect of the relative values of  $\alpha$  and  $\epsilon$ .

Choi et al. [61] reported a time of 2.58 seconds to achieve a zero tracking error (OTE). It can be observed from Table 2.1 that in almost all the cases under consid-

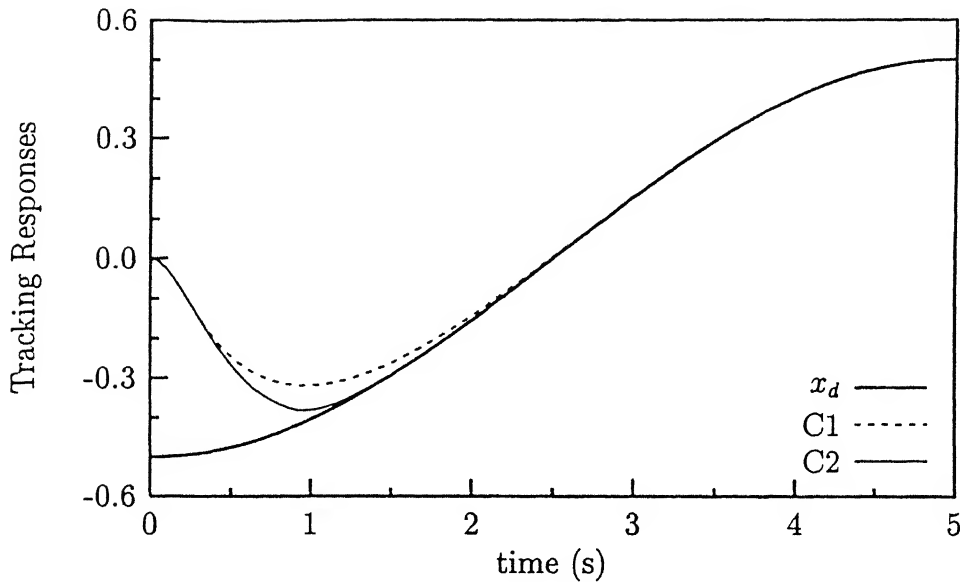


Fig. 2.1: Tracking responses for Case 1 ('C1') and Case 2 ('C2').

eration, a lesser tracking time is achieved by this approach. In fact the best tracking time achieved is 1.65 seconds for Case 6. In all of the cases the actual time to reach OTE is smaller than the bound given by the  $A_b$  dynamics and the  $t_f$ . As qualitatively similar responses were obtained, the responses obtained for the parameter combination in Cases 1 and 2 are presented in Figs. 2.1, 2.2, and 2.3 respectively. The responses are indexed by the case numbers in these figures. Note that Case 1 corresponds to Case  $CQ$ , and Case 2 to Case  $CP$ . Fig. 2.1 shows the tracking response obtained in the two cases. It is evident from the figure that the 'C2' (satisfying the Lemma 1) trajectory approaches the OTE in appreciably lower time as compared to the 'C1' trajectory. Fig. 2.2 shows the  $s$  response in the two cases. The 'C1' response has a lower reaching time (see also Table 2.1) as compared to 'C2'. Fig. 2.3 shows the error decay with time for both the cases and also for the solution of the  $A_b$  dynamics in (2.35), labeled as  $e_A$ . Although, only a better decay of the Lyapunov function in (2.24) is guaranteed for the control law in (2.9), the figure shows that the decay of  $e$  obtained in the two cases are better than the solution of the  $A_b$  dynamics in (2.35).

The required control effort in the two cases are shown in Fig. 2.4. As discussed in

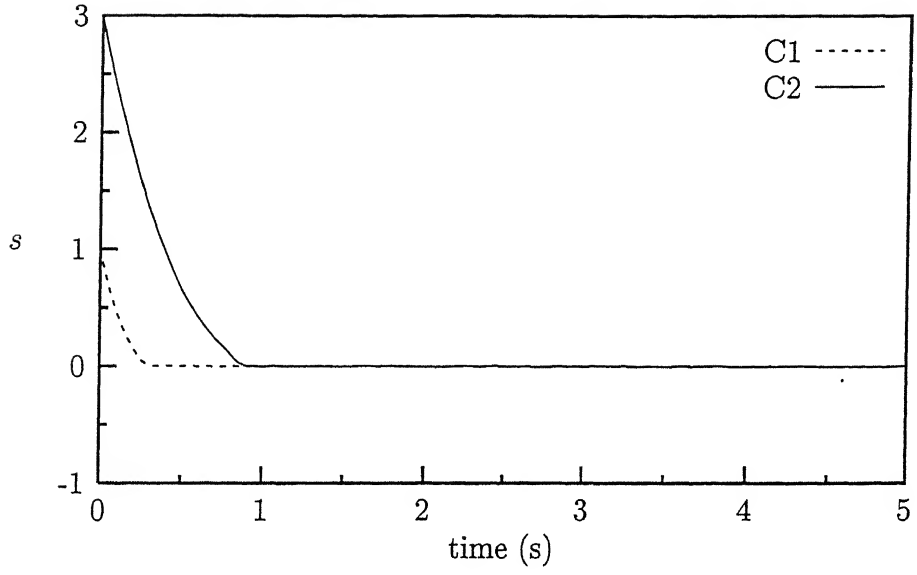


Fig. 2.2: The  $s$  responses for Cases 1 and 2.

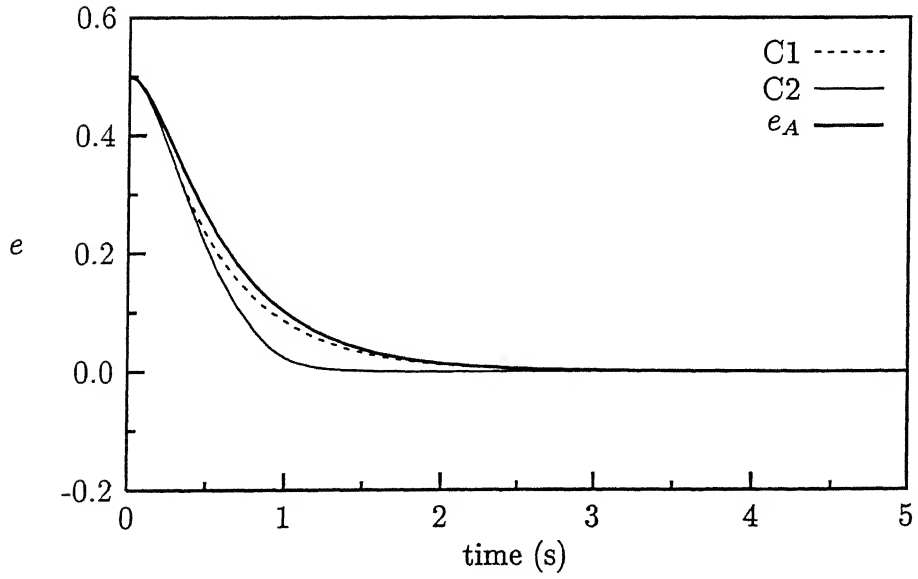


Fig. 2.3: The error dynamics for Cases 1 and 2 and that given by the A-dynamics ( $e_A$ ).



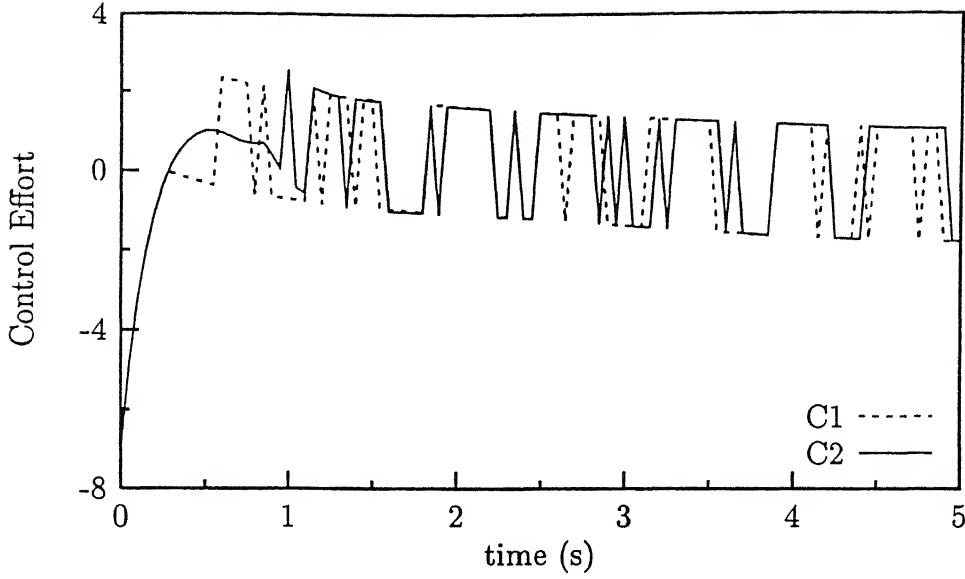


Fig. 2.4: The control effort  $u$  required for Cases 1 and 2.

the previous section, since  $a = 12$  and  $b = 8$  from (2.8) are same for the cases 'C1' and 'C2', thus the control efforts in these cases should be of about the same magnitudes. This can indeed be seen from Fig. 2.4, thus it verifies that the proposed method uses about the same control effort to achieve the same tracking accuracy much faster. However as the reaching time in 'C1' is smaller, the input in Case 'C1' begins chattering earlier as can be seen from the figure. Thus the selection of the parameters can be easily done drawing on the experience of the initial condition responses of linear second order systems. If the  $\alpha$  and  $\epsilon$  are chosen so as to satisfy Lemma 1, better results are expected.

### 2.4.2 Two-link Robotic Arm

The design method given in Section 2.3 is extended to multi-input case consisting of the two-link robot arm problem [37]. The equations governing the dynamics are given as

$$H(q)\ddot{q} + C(q, \dot{q})\dot{q} = \tau + d \quad (2.50)$$

where,  $q = (\theta_1, \theta_2)^T$  gives the angles of the two links in radians.  $H(q)$  is the positive definite inertia matrix. The vector  $\tau = (\tau_1, \tau_2)^T$  is the control torque vector, and

$d = (d_1, d_2)^T$  represents the disturbance vector with bounds on their magnitude given as  $|d_1| < D_1$ , and  $|d_2| < D_2$ . The expressions for all the functions in the above equation are taken from [21]. The above equation can be rewritten as

$$\ddot{q} = H^{-1}(q)[\tau + d - C(q, \dot{q})\dot{q}]. \quad (2.51)$$

The trajectory to be followed is given as  $q_d = (\theta_{1d}, \theta_{2d})$ , and its time derivatives. The error vector is defined as before.

$$\begin{pmatrix} e_1 \\ \dot{e}_1 \\ e_2 \\ \dot{e}_2 \end{pmatrix} = \begin{pmatrix} \theta_1 - \theta_{1d} \\ \dot{\theta}_1 - \dot{\theta}_{1d} \\ \theta_2 - \theta_{2d} \\ \dot{\theta}_2 - \dot{\theta}_{2d} \end{pmatrix}. \quad (2.52)$$

Following the developments in Section 2.2, the input torques are selected as

$$\begin{pmatrix} \tau_1 \\ \tau_2 \end{pmatrix} = H(q) \begin{pmatrix} \ddot{\theta}_{1d} - a_1 e_1 - b_1 \dot{e}_1 - \bar{D}_1 \text{sgn}[s_1] \\ \ddot{\theta}_{2d} - a_2 e_2 - b_2 \dot{e}_2 - \bar{D}_2 \text{sgn}[s_2] \end{pmatrix} + C(q, \dot{q})\dot{q}. \quad (2.53)$$

where, the quantities  $a_1, b_1, a_2, b_2 > 0$  are selected by appropriate choices of  $\alpha_1, \alpha_2$  and  $\epsilon_1, \epsilon_2$ . Also  $\bar{D}_1 = D_1 + \eta_1$ , and  $\bar{D}_2 = D_2 + \eta_2$ . Under the application of the control law the system decouples into two single input systems. It is easily seen that the above control law satisfies the following constant plus proportional rate reaching law

$$\begin{aligned} \dot{s}_1 &\leq -\epsilon_1 s_1 - \eta_1 \text{sgn}[s_1], \text{ and} \\ \dot{s}_2 &\leq -\epsilon_2 s_2 - \eta_2 \text{sgn}[s_2]. \end{aligned} \quad (2.54)$$

Then the choice of the parameters can be done based on the discussion in Section 2.3.

Simulation was done as in the previous example, but with a time step of  $500\mu s$ . The parameters of the robot, the disturbance signals, and the controller parameters are taken from [37] in which the SMC parameters were taken as  $\alpha = 1$ , and  $\epsilon = 15$  (Case  $CQ$  of Section 2.3). The Lemma 1 indicates that the choice of the two parameters should be the other way round.  $\beta$  and  $\eta$  were selected as in the earlier example. The Table 2.2 presents the various time bounds and the actual tracking times for four parameter combinations.

**Table 2.2:** Comparison of time for OTE and Reaching: Example 2. (L1) and (L2) denote responses for the Links 1 and 2 respectively.

Case no.	$\alpha$	$\epsilon$	Time to OTE ( $< 1 \times 10^{-3}$ ) in (s)		Reaching time (s) (A.7)	$t_f$ (s) (2.47) for $\frac{V_0}{V_f} = 10^4$
			Bound obtained from $A_b$ dynamics (2.35)	Actual		
1	2	6	4.24	3.128 (L1) 2.890 (L2)	0.183	4.605
2	6	2	4.24	1.095 (L1) 0.910 (L2)	1.472	2.302
3	1	15	2.83	5.683 (L1) 5.475 (L2)	0.027	9.210
4	15	1	2.83	0.563 (L1) 0.423 (L2)	4.732	4.605

It is seen from the table that the Cases 1 and 3, corresponding to the Case  $CQ$ , have very small reaching times as compared to the Cases 2 and 4 which correspond to the Case  $CP$ . Although the Case  $CP$  exhibits a much larger reaching time, it is expected from Lemma 1 and the results in the previous section that it should exhibit a faster tracking performance as compared to the Case  $CQ$ . The times to OTE for the Case  $CP$  is indeed seen to be substantially smaller than the corresponding Case  $CQ$ .

Since the qualitative nature of the responses in the Cases 2 and 4 are similar, as was also observed for the the other two cases, the error responses obtained only for the Cases 3 (labeled as  $C3$ ) and 4 (labeled  $C4$ ) for the first link is presented in Fig. 2.5, and that for the second link in Fig. 2.6. As is indicated by the very small reaching time for the Case  $CQ$ , it was observed from the numerical simulation results that in Case  $CQ$ , sliding begins almost instantaneously as compared to the Case  $CP$ . However, from the  $CQ$  response in the figures, the time to OTE is seen to be about 5.5s as compared to about 0.5s for the Case  $CP$ . This again shows that substantially better performances are achievable by satisfying Lemma 1. It also substantiates the view that

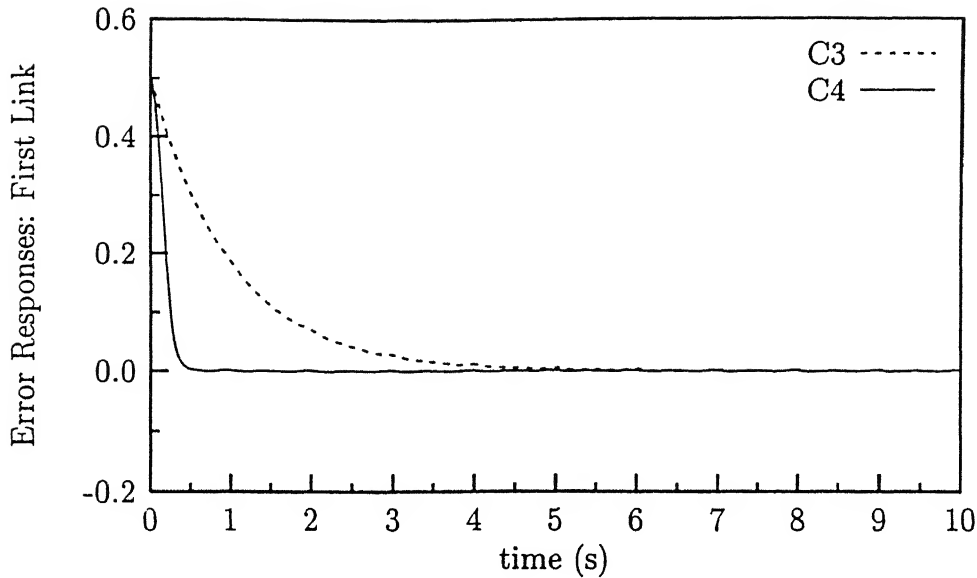


Fig. 2.5: Error responses for the first link for Cases C3 (*CQ*) and C4 (*CP*).

a lower reaching time does not imply faster tracking. Thus, it may be concluded that the time to OTE should be used as the criterion to select the controller parameters rather than the reaching time.

The required control efforts  $\tau_1$  and  $\tau_2$  (2.53) for parameter combinations in Cases 3 and 4 are presented in Figs. 2.7 and 2.8 respectively. It is observed that required torque levels for both cases are similar.

## 2.5 Conclusions

In this chapter the design of the constant plus proportional rate reaching SMC for second order nonlinear systems has been studied. An investigation of the effect of the choice of the controller parameters has been done. Using a Lyapunov approach it has been shown that the design method imposes a bounding second order dynamics on the error variables, and thus a robust performance in the reaching phase is guaranteed. A new method of selection of the SMC parameters which results in smaller times to reach a given level of OTE, while using almost similar levels of maximum control effort, is proposed. It is seen that for the class of systems under study, a small reaching time does

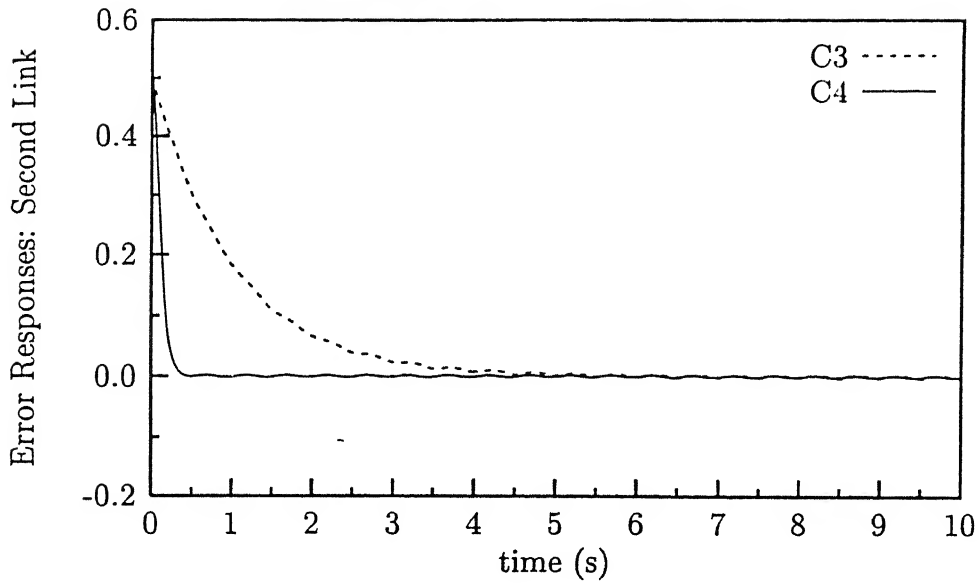


Fig. 2.6: Error responses for the second link for Cases C3 (*CQ*) and C4 (*CP*).

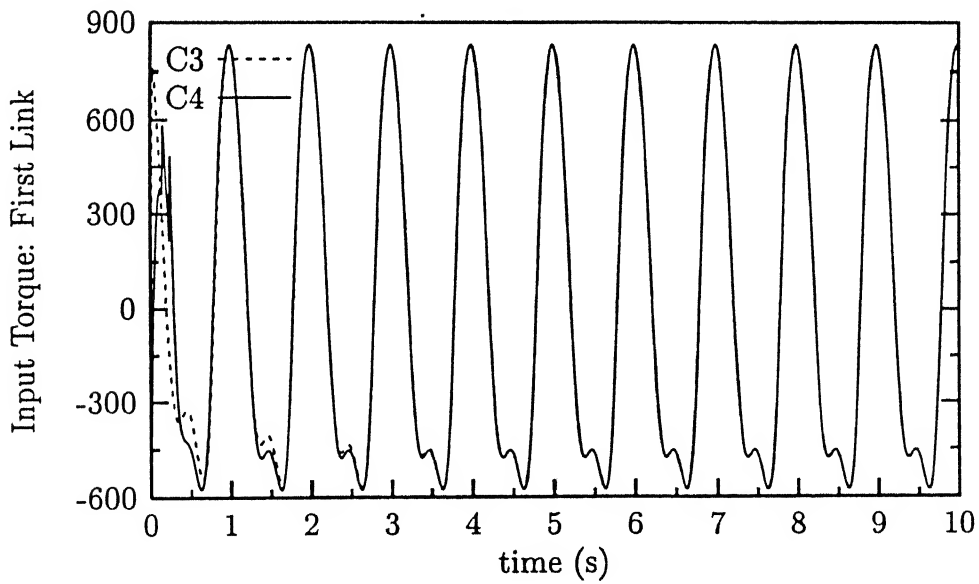


Fig. 2.7: The input torque  $\tau_1$ .

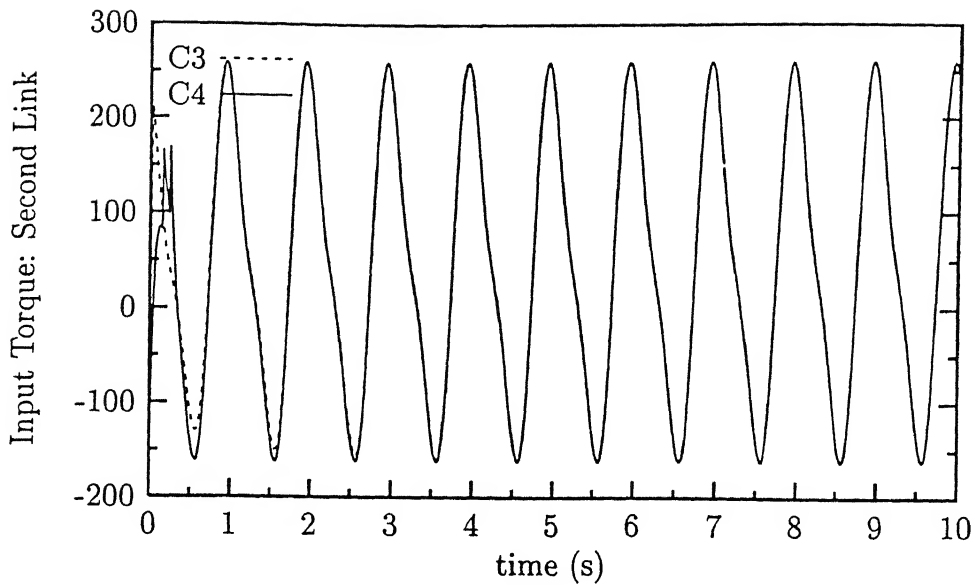


Fig. 2.8: The input torque  $\tau_2$ .

not guarantee a fast tracking response. The method of parameter selection should thus be based on the time to OTE, rather than on the criterion of the reaching time. The design technique has been applied to a nonlinear spring-mass-damper system under matched uncertainties and exogenous disturbances. From the simulations done it is seen that the control laws based on the lower reaching times require approximately 10 – 60% more time as compared to the proposed control laws to reach the same level of OTE, while using the same levels of control magnitudes. The method developed for a single input system has been extended to a two input two link robotic arm problem. Results of numerical simulation for the parameters used show that significantly faster tracking is obtained with the proposed control law, thus establishing the utility of the method. However, more work is required to develop better estimates of the time to OTE.

# Chapter 3

## SMC for the Longitudinal Dynamics of a Fighter Aircraft

### 3.1 Introduction

The aircraft flight control system (FCS) forms the backbone of the current generation fighter aircrafts. This chapter discusses the application of the SMC method for the design of FCS for fighter aircrafts. The aircraft is conventionally modelled as a 6 degree of freedom (dof) rigid body [10]. As discussed in Chapter 1, the nonlinear inverse dynamics based flight control design has been applied in many works [17, 23, 24, 27–29, 39] to various aircrafts for varying purposes. However, the issue of robustness of the feedback linearization techniques to disturbances and uncertainties still needs to be addressed. The SMC, with its robustness properties, offers an alternative method for this problem. However, it has not been readily used for the FCS design problem as is evident from the lack of a single application paper in the the special issue of the *International Journal of Control* (Vol. 59 no.1, 1994) on aircraft flight control design [17, 39].

The SMC method has earlier been used for FCS design problem by some researchers. Calise and Kramer [40] applied the SMC design method to the linearized dynamics of the AV-8A Harrier in a hover mode under matched uncertainties and compared the obtained responses with those obtained using a LQ based design. They observed that the SMC method outperformed the linear controller in the presence of disturbances

and uncertainties. Mudge and Patton [64] designed SMC laws with eigenstructure assignment for a remotely piloted vehicle and provide frameworks for assessment of robustness. Singh [41] defined a switching function which included the integral of the tracking error also and led to improved closed loop performance. Control laws for large rapid rotational maneuvers of aircraft under the perturbational model for aerodynamics and matched uncertainty are developed. Hedrick and Gopalswamy [42] show that the undesirable zero-dynamics could be tackled by output redefinition. They designed control laws for the nonlinear pitch axis system dynamics with linearized aerodynamics under matched uncertainty. The HQ criteria were incorporated into the design procedure. They also developed a method of selection of sliding gains for a MIMO system. Thukral and Innocenti [43] designed SMC laws for a linearized model of the longitudinal dynamics for the stabilization and tracking problems. They also presented a review of related work.

In this chapter, the longitudinal or the pitch axis control problem for the nonlinear aircraft dynamics has been studied. The aircraft longitudinal dynamics and the force control approach (FCA) are explained briefly in the next section. In addition to the uncertainties and disturbances generally considered, an error between the command force vector and the actually obtained force vector is taken into consideration. A model following (MF) structure is next described and is used to design a full envelope SMC law taking these uncertainties into account. Analytic control laws for the tracking and the trimming modes of the aircraft are developed and simulations are done using the inertia parameters of the F-16 aircraft to show the effectiveness of the MF-SMC (model following-SMC) approach.

## 3.2 Longitudinal Dynamics and Force Control Approach

The aircraft longitudinal dynamics in the body fixed frame is defined by the set of ordinary nonlinear differential equations [10] as given in (3.1).



$$\begin{pmatrix} \dot{U} \\ \dot{W} \\ \dot{Q} \\ \dot{\theta} \\ \dot{p}_x \\ \dot{p}_z \end{pmatrix} = \begin{pmatrix} -QW - g_0 \sin(\theta) \\ QU + g_0 \cos(\theta) \\ 0 \\ Q \\ U \cos(\theta) + W \sin(\theta) \\ U \sin(\theta) - W \cos(\theta) \end{pmatrix} + \begin{pmatrix} R_m F_x \\ R_m F_z \\ c_7 M \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad (3.1)$$

The system states are  $U, W$ , the velocities along the body X and Z axes respectively, the pitch rate  $Q$ , the pitch angle  $\theta$ , and  $p_x, p_z$  the positions along X and Z axes respectively from an earth frame of reference.  $F_x, F_z$  represent the forces along the X and Z directions respectively; and  $M$  is the pitching moment. Also  $g_0$  denotes earth's gravity,  $R_m$  denotes the inverse of the mass of the aircraft, and  $c_7$  is the inverse of inertia of the aircraft about its pitching axis.

The forces and the moments in (3.1) are in general nonlinear functions of the state and the deflections of the CFC (conventional flight control) surfaces i.e., the elevator and the throttle [10]. However, the SMC design technique has mainly been developed for systems that are input affine. Most of the FCS applications cited earlier are based on input affine or linearized models of the aircraft. Bartolini and Zolezzi [65] extended the SMC method to include the case of systems nonlinear in the input by redefining the equivalent control, based on the existence of a particular map. This approach has been used in this work through the FCA, which is discussed next.

If the forces  $F_x, F_z$ , and the pitching moment  $M$  can be independently varied, these may be treated as the pseudo input vector, and would render the governing system of equations in (3.1) input affine. Independent control of the 3-component force vector with the two CFC inputs is however not possible, and therefore, it becomes necessary to use additional control effectors. Smith and Meyer [23] treated the desired accelerations as pseudo-inputs. Hauser et al. [66] assumed that there exists a *one-to-one* mapping from the input space to the force vector. Snell et.al. [49] used TV (thrust vectoring) to augment the standard control surfaces. Franklin [39] used the forces as input for the translational longitudinal control problem. The TV concept is gaining increasing

popularity and in fact is going to be present in almost all of the next generation fighters [6, 8]. It has the advantage that its effectiveness does not vary much with the aircraft speed as opposed to the conventional aerodynamic surfaces. Hence, it may be used to advantage when the CFC surfaces are ineffective or are damaged in combat [46]. The TV-FCS has been flight tested on scaled aircraft models and is already equipping the front line USAF F-15, F-16, and YF-22 fighters [7], the X-31 experimental aircraft [45], and the Russian Sukhoi family of fighters [9]. With TV capability, the forces  $F_x$ ,  $F_z$  and the pitching moment  $M$ , with the assumption that the thrust acts through the center of gravity, are given [46] as

$$\begin{aligned} F_x &= \bar{q}S \left[ C_x(\alpha, \delta_{el}) + \frac{\bar{c}Q}{2V_t} C_{x_Q}(\alpha) \right] + T_x, \\ F_z &= \bar{q}S \left[ C_z(\alpha, \delta_{el}) + \frac{\bar{c}Q}{2V_t} C_{z_Q}(\alpha) \right] + T_z, \text{ and} \\ M &= \bar{q}S\bar{c} \left[ C_m(\alpha, \delta_{el}) + \frac{\bar{c}Q}{2V_t} C_{m_Q}(\alpha) + C_{m_{TV}}\delta_v \right], \end{aligned} \quad (3.2)$$

where,  $\bar{q}$ ,  $S$ ,  $\alpha$ ,  $\delta_{el}$ ,  $\bar{c}$ ,  $V_t$  represent the dynamic pressure, the wing surface area, the angle of attack, the elevator deflection, the mean aerodynamic chord, and the total velocity. Also the  $\delta_v$  represents the effective pitch thrust-vectoring angle. The various  $C_i(\cdot, \cdot)$  give the functional relations of the  $i^{th}$  component of the non-dimensional force with its arguments (Refer [10] for further details). Also  $T_x$  and  $T_z$  are the components of the thrust vector in the directions specified by their subscripts, and are given as  $T_x = \eta T_a \cos(\delta_v)$  and  $T_z = \eta T_a \sin(\delta_v)$ , where  $\eta$  is a dimensionless nozzle thrust coefficient, and  $T_a$  is the actual thrust of the engine [46]. Thus the force vector is seen to be a function of three variables  $\delta_{el}$ , the  $T_a$  and the vectoring angle  $\delta_v$ . Other more conventional alternatives, such as the air brakes, spoilers, flaps etc. may also be used. Thus using a suitable combination of the available effectors, it should be possible to control the 3-component force vector. Durham [48] considers the control allocation problem to generate a set of desired accelerations. In case, many solutions exist, a suitable combination of these alternatives may be used to perform other control configured vehicle (CCV) functions. For this work, it is assumed that the aircraft has sufficient number of control effectors so that the 3-component force vector may be used as pseudo-input.

With this, the governing equation (3.1) becomes input affine and can be seen to depend on parameters such as  $R_m$  and  $c_7$ . Depending on the mission objectives of the aircraft project, a fair estimate of these parameters can be made using data from other aircrafts of a similar category. It is better to define these parameters as a range of values they are likely to take. This would have to be taken as such even if the aircraft parameters were known, because fuel and armaments carried on-board vary with time and also from mission to mission. These have been incorporated as time varying but bounded multiplicative uncertainties as

$$\begin{aligned} R_m &= (1 + \delta_{b1})\hat{R}_m, \text{ and} \\ c_7 &= (1 + \delta_{b2})\hat{c}_7 \end{aligned} \quad (3.3)$$

where  $\hat{R}_m$  and  $\hat{c}_7$  represent the nominal values of  $R_m$  and  $c_7$  respectively. The time varying multiplicative uncertainties represented by  $\delta_{b1}$  and  $\delta_{b2}$  are bounded as  $|\delta_{b1}| \leq D_{b1}$ , and  $|\delta_{b2}| \leq D_{b2}$ . In this section the aircraft longitudinal dynamics system, as considered in this work, has been explained. As discussed in Chapter 1, a model-following approach has been used for this problem and is presented next.

### 3.3 The Model-Following Control

A MF structure as shown in Fig 3.1 is used to achieve robust tracking performances. The nonlinear aircraft state equations (3.1) have already been presented in the previous section. The method also requires a model response trajectory. This can be generated by the pilot with the inputs available to him namely the elevator, the throttle gear and the mode selector. The mode selector specifies the outputs to be tracked. Different models may be selected, for the various modes and with varying operating regimes, as specified by the HQ engineers and/or the pilots. It suffices to assume, that one is provided with the state trajectory to be tracked and its time derivative. The model used in the present study is given in the Appendix D.

As can be seen from the figure, the controller gives as output the desired force vector  $F_{com}$  which should be applied to the aircraft. An aerodynamic inversion is required

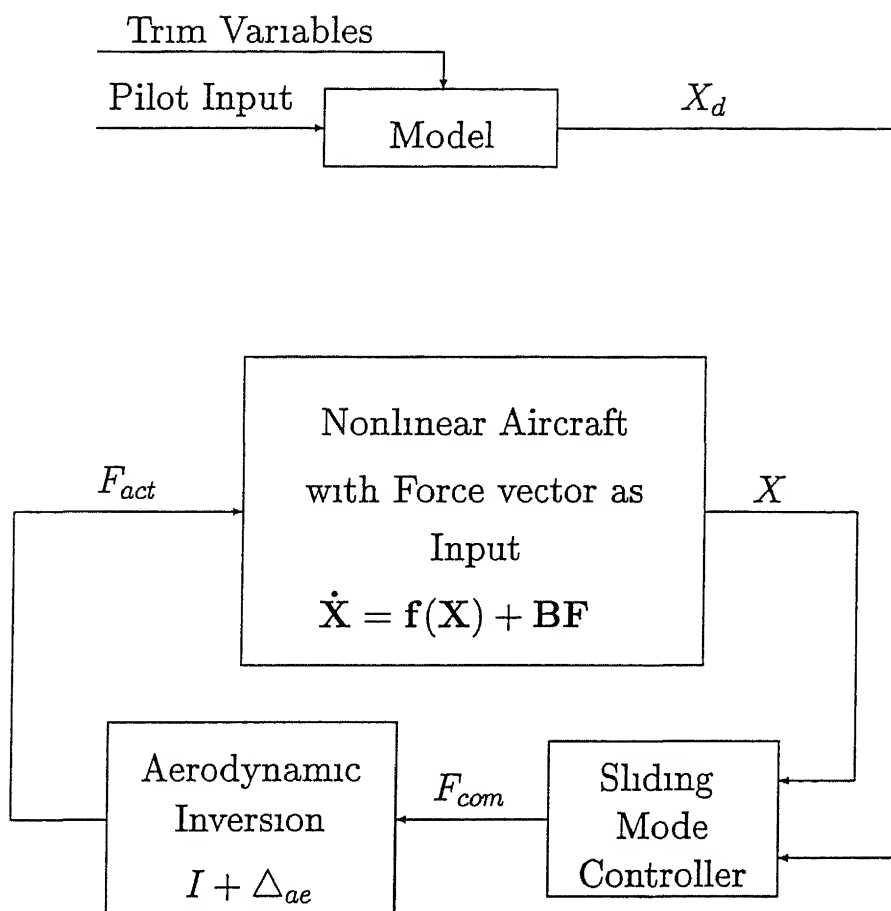


Fig. 3 1 Schematic Model-Following Control Scheme

to get the actual control surface deflections. On applying these to the actual aircraft, the generated force vector  $F_{\text{act}}$  is likely to be different from the  $F_{\text{com}}$  as shown in Fig 3.1. Most of the works cited earlier [23, 39] assume that these signals are identical. However, in practice this assumption is likely to lead to errors for the following reasons

- 1 **Uncertainties in the aerodynamic modeling and data:** The data used for control design is normally based on some models and/or observations from wind-tunnel experiments on the scaled models of the aircraft. Also the aeroelastic effects are generally not considered.
- 2 **Uncertainties in the aerodynamic inversion block:** The nonlinear inversion process itself may not be exact.
- 3 **Unmodeled actuator dynamics:** The actuator dynamics are generally neglected in a first level control design.
- 4 **Uncertain position of the center of gravity (CG):** The moment  $M$  depends, besides other factors, on the actual position of the CG.
- 5 **Uncertainty in the air velocity relative to the aircraft:** The forces and the moments vary proportionally with the square of the relative air velocity. Errors in measurement and the presence of wind gusts can lead to this uncertainty.

It is assumed that errors from the above sources are bounded and can be represented by time varying multiplicative uncertainties as

$$F_{\text{act}} = (I + \Delta_{ae})F_{\text{com}} \quad (3.4)$$

where  $\Delta_{ae}$  is a  $3 \times 3$  diagonal matrix with the diagonal entries being  $\delta_{ae}(i)$ ,  $i = 1, 2, 3$  all of which are bounded with  $|\delta_{ae}(i)| \leq D_{ae}(i)$ , a known quantity.

The Section 3.2 and this section completely define the FCS design problem with the system equations in (3.1), the uncertainties involved in the aircraft inertia parameters and the inputs in (3.3) and (3.4), the desired model response (as in Appendix D), and the MF control structure used (as shown in Fig. 3.1). The SMC design method for the MF problem of a MI nonlinear system as presented above is next discussed.

### 3.4 Tracking in Multi-Input Nonlinear Systems

The aircraft system of equations in (3.1) with external disturbances can be expressed in a general form as

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{f}(\mathbf{x}) + \mathbf{G}(\mathbf{x})\mathbf{u} + \mathbf{d}, \text{ and} \\ \mathbf{y} &= \mathbf{y}(\mathbf{x}),\end{aligned}\tag{3.5}$$

where  $\mathbf{x} \in \mathcal{R}^n$ ,  $\mathbf{u}, \mathbf{y} \in \mathcal{R}^m$  represent the state, input and output vectors respectively, and  $\mathbf{d}$  represents the external disturbance vector given bounded as  $|d_i| \leq D_i$ ,  $i = 1, \dots, n$ . Since the number of trackable outputs equals the number of independent inputs, the number of outputs and inputs are assumed to be equal. Also  $\mathbf{G}(\mathbf{x})$  is assumed to be of rank  $m$  over the entire state space. The number of differentiations of  $\mathbf{y}(\mathbf{x})$  required for the input  $\mathbf{u}$  to appear in its expression is called the relative degree of the system. It is assumed without any loss of generality that all components of  $\mathbf{y}$  have a relative degree '1'.

Under a suitable coordinate transformation from  $\mathbf{x}$  to  $\mathbf{z} = [\mathbf{y}^T \xi^T]^T$ , where the superscript T denotes the transpose, and  $\xi \in \mathcal{R}^{n-m}$ , the above nonlinear system may be expressed in a reduced form [37, 52] as

$$\dot{\mathbf{y}} = \mathbf{f}_1(\mathbf{z}) + \mathbf{B}_1(\mathbf{z})\mathbf{u} + \mathbf{d}_1, \text{ and}\tag{3.6}$$

$$\dot{\xi} = \mathbf{f}_2(\mathbf{z}) + \mathbf{d}_2\tag{3.7}$$

The (3.6) represents the matched dynamics and the disturbances and/or uncertainties,  $\mathbf{d}_1$ , entering this equation are called matched. The (3.7) gives the unmatched portion of the dynamics and the disturbances and/or uncertainties,  $\mathbf{d}_2$ , entering this equation are said to be unmatched. In this chapter, only matched disturbances/uncertainties are assumed since the SMC guarantees invariant performance in the presence of this class of uncertainties. The case of unmatched uncertainties is considered in the next chapter. The matched disturbance vector  $\mathbf{d}_1$  is given to be bounded with  $|d_{1,i}| \leq D_{1,i}$ ,  $i = 1, \dots, m$ . Under the assumptions made above the matched dynamics represents a square system of  $m$  equations. Also  $\mathbf{B}_1(\mathbf{z})$  is an  $m \times m$  matrix having full rank over

the state space  $\mathbf{z}$  thus implying a strong relative degree '1'. The arguments of the various functions defined above are dropped if no confusion is likely to arise. Let  $\hat{\mathbf{B}}_1$  represent the nominal  $\mathbf{B}_1$  matrix. It is assumed that the  $\mathbf{B}_1$  may be expressed as  $\mathbf{B}_1 = (\mathbf{I} + \Delta_b)\hat{\mathbf{B}}_1$ , in which all the matrices are appropriately dimensioned with  $\mathbf{I}$  representing the identity matrix. Also the matrix  $\Delta_b$  is bounded by a known matrix  $D_b$  as  $|\Delta_b(i, j)| \leq D_b(i, j)$ .

As explained earlier,  $\mathbf{u}$  in (3.6) is the actually applied control signal, i.e.  $\mathbf{u}_{act}$ . With the uncertainty as modeled in (3.4),  $\mathbf{u}_{act} = (\mathbf{I} + \Delta_{ae})\mathbf{u}_{com}$ , the system equations in (3.6) and (3.7) can be rewritten as

$$\mathbf{y} = \mathbf{f}_1 + (\mathbf{I} + \Delta_b)\hat{\mathbf{B}}_1(\mathbf{I} + \Delta_{ae})\mathbf{u}_{com} + \mathbf{d}_1, \text{ and} \quad (3.8)$$

$$\xi = \mathbf{f}_2 \quad (3.9)$$

The MF-SMC design for the case when  $\Delta_{ae} = 0$  is reported in Slotine and Li [21] and Hedrick and Gopalswamy [42]. In this chapter the method has been extended to a more general case with  $\Delta_{ae} \neq 0$ .

Let the trajectory to be followed be specified as  $\mathbf{y}_d$  and  $\dot{\mathbf{y}}_d$ . Define  $\mathbf{S}$  as a vector consisting of the error function for the output vector as

$$\mathbf{S} = \mathbf{y} - \mathbf{y}_d \quad (3.10)$$

It is desired that  $\mathbf{S} = 0$ . To this end, taking time derivative of the above equation, and using (3.8) gives

$$\begin{aligned} \mathbf{S} &= \mathbf{y} - \mathbf{y}_d \\ &= \mathbf{f}_1 + (\mathbf{I} + \Delta_b)\hat{\mathbf{B}}_1(\mathbf{I} + \Delta_{ae})\mathbf{u}_{com} + \mathbf{d}_1 - \mathbf{y}_d \end{aligned} \quad (3.11)$$

The equivalent control [21] is defined as the input  $\hat{\mathbf{u}}_{com}$ , which makes  $\mathbf{S} = 0$ , when  $\mathbf{S} = 0$  for the nominal plant, i.e.  $\Delta_b = 0$ ,  $\Delta_{ae} = 0$ , and  $\mathbf{d}_1 = 0$ . Thus the equivalent control becomes

$$\hat{\mathbf{u}}_{com} = \hat{\mathbf{B}}_1^{-1}(\mathbf{y}_d - \mathbf{f}_1) \quad (3.12)$$

The applied input function should make the SS attractive in the presence of disturbances and uncertainties also. This is achieved by selecting the applied control signal

as the sum of the equivalent control and a discontinuous function as

$$\mathbf{u}_{\text{com}} = \hat{\mathbf{B}}_1^{-1}(\mathbf{y}_d - \mathbf{f}_1 - \mathbf{k} \operatorname{sgn}[\mathbf{S}]) \quad (3.13)$$

where,  $\mathbf{k} \operatorname{sgn}[\mathbf{S}]$  is an  $m \times 1$  column vector with all  $k_i > 0$ ,  $i = 1, \dots, m$ . Let  $(\mathbf{k} \operatorname{sgn}[\mathbf{S}])_i = k_i \operatorname{sgn}[S_i]$  represent the  $i^{\text{th}}$  component of the vector. The real vector  $\mathbf{k}$  has to be selected so that trajectories starting from nonzero values of  $\mathbf{S}$  approach the SS. Putting  $\mathbf{u}_{\text{com}}$  from (3.13) in (3.11) gives

$$\mathbf{S} = \mathbf{f}_1 + (I + \Delta_b)\hat{\mathbf{B}}_1(I + \Delta_{ae})\hat{\mathbf{B}}_1^{-1}(\mathbf{y}_d - \mathbf{f}_1 - \mathbf{k} \operatorname{sgn}[\mathbf{S}]) + \mathbf{d}_1 - \mathbf{y}_d \quad (3.14)$$

The above equation may be simplified by defining an  $m \times m$  matrix  $\Delta_t$ , such that

$$(I + \Delta_t) = (I + \Delta_b)\hat{\mathbf{B}}_1(I + \Delta_{ae})\hat{\mathbf{B}}_1^{-1} \quad (3.15)$$

The bounds on the matrix  $\Delta_t$  can be evaluated from the known bounds on  $\Delta_b$  and  $\Delta_{ae}$  as will be shown in the next section. Let these be given as  $|\Delta_t(i, j)| \leq D_t(i, j)$ . With this, (3.14) can be rewritten as

$$\mathbf{S} = \mathbf{f}_1 + (I + \Delta_t)(\mathbf{y}_d - \mathbf{f}_1 - \mathbf{k} \operatorname{sgn}[\mathbf{S}]) + \mathbf{d}_1 - \mathbf{y}_d, \quad (3.16)$$

which may further be simplified to

$$\mathbf{S} = \Delta_t(\mathbf{y}_d - \mathbf{f}_1) - (I + \Delta_t)\mathbf{k} \operatorname{sgn}[\mathbf{S}] + \mathbf{d}_1 \quad (3.17)$$

The SS is made attractive by selecting  $\mathbf{k}$  such that

$$S_i S_i < -\eta_i |S_i|, \quad (3.18)$$

where  $\eta_i, i = 1, \dots, m$  is a positive scalar quantity to be selected, thus satisfying the reaching condition [21]. The above equation guarantees (see Appendix A) that the  $S_i$  response will be better than the response of

$$S_i = -\eta_i \operatorname{sgn}[S_i] \quad (3.19)$$

Following the algebraic manipulations along the lines of [21, 42],  $\mathbf{k}$  can be obtained as the solution of the following system of linear algebraic equations

$$(I - D_t)\mathbf{k} = \Psi, \quad (3.20)$$



where,  $D_t$  is the matrix with  $D_t(i, j)$  as its components, and  $\Psi$  is an  $m \times 1$  vector with

$$\Psi_i = \Psi(i) = D_{1,i} + \eta_i + \sum_{j=1}^m D_t(i, j) |y_d(j) - f_1(j)|, \quad i = 1, \dots, m \quad (3.21)$$

It is obvious that  $\Psi(i) > 0$ ,  $i = 1, \dots, m$  from the above equation. The existence of a unique solution  $\mathbf{k}$  with all  $k_i \geq 0$  is easily established using the Forbenius-Perron Theorem [21] (See Theorem 1 in Appendix G) and requires that the largest positive eigenvalue of  $D_t$  be less than 1.0

The use of a  $\text{sgn}[\cdot]$  function in (3.13) gives rise to the chattering problem. Various methods have been suggested in the literature for its alleviation [21, 56]. In this study, the concept of a boundary layer as proposed by Slotine [21] has been used to approximate the discontinuity by a continuous control law. Accordingly, for implementation purposes, the vector  $\mathbf{k} \text{sgn}[\mathbf{S}]$  in (3.13) is replaced by  $\mathbf{k} \text{sat}[\mathbf{S}/\Phi]$ , whose  $i^{\text{th}}$  element is given as  $k_i \text{sat}[S_i/\phi_i]$ , where  $\Phi$  is a  $m \times 1$  column vector of appropriately selected boundary layer thickness, given as  $[\phi_i]^T$ ,  $i = 1, \dots, m$ . The control law in (3.13), then becomes

$$\mathbf{u}_{\text{com}} = \hat{\mathbf{B}}_1^{-1}(\mathbf{y}_d - \hat{\mathbf{f}} - \mathbf{k} \text{sat}[\mathbf{S}/\Phi]) \quad (3.22)$$

The  $S_i$  dynamics then becomes

$$\dot{S}_i = -\eta_i \text{sat}[S_i/\phi_i] \quad (3.23)$$

With the  $\mathbf{u}_{\text{com}}$  as selected above, the motion in the sliding mode is guaranteed to be inside of thickness  $\Phi$  of the SS [21]. Thus,

$$|S_i| \leq \phi_i \quad (3.24)$$

Moreover, starting from a non-zero initial condition  $\mathbf{S}_0$ , the dynamics in (3.23) guarantees that its  $i^{\text{th}}$  component  $S_i$  reaches the boundary layer within a finite time  $(t_{0,i})$  given by

$$t_{0,i} \leq \frac{S_{0,i} - \phi_i}{\eta_i} \quad (3.25)$$

Thus, a larger value of  $\eta$  leads to a smaller reaching time and larger control efforts

Thus, the above selection of  $\mathbf{u}_{\text{com}}$  in (3.22) guarantees that the outputs are tracked with a desired accuracy, however, the stability properties of the unmatched dynamics in (3.9) need to be investigated. It has been shown [21] that this can be determined by studying the stability of the zero dynamics (ZD), which is defined as the dynamics of the system when the outputs and all its time derivatives are kept at 0 (zero) by appropriate choice of the input. The ZD for the system (3.5), with all outputs having a relative degree '1' is thus seen to be a special case of the unmatched dynamics in (3.9) as

$$\xi = \mathbf{f}_2([0^T \xi^T]^T) \quad (3.26)$$

The stability of the unmatched dynamics is proved if the ZD is at least bounded [21]

The SMC method as outlined here is applied to the design of control laws for the longitudinal dynamics of an aircraft using the MF structure as discussed in Section 3.3. Therefore, the method is termed as the MF-SMC. The results of numerical simulation are presented next.

### 3.5 Numerical Example and Simulation

MF-SMC laws are synthesized, following the steps outlined in the previous section, for the FCS design problem as presented in Sections 3.2 and 3.3. The numerical values of the time varying multiplicative parametric uncertainties and disturbances and their bounds as defined in the previous sections as also the mass and inertia parameters of the aircraft as used for simulation purposes are given in the Appendix D. To show the applicability of the proposed method, controllers are designed for the following two cases

- 1 **C1:** In this case, the controller design is done assuming that the  $F_{\text{com}}$  and  $F_{\text{act}}$  are identical, i.e.  $\Delta_{ae} = 0$
- 2 **C2:** Here, the controller design takes into account that  $\Delta_{ae} \neq 0$

The controllers corresponding to the cases **C1** and **C2** will be called as the **M1** and **M2** respectively.

As stated earlier, it is possible to track only three states or outputs using the 3-component force vector. Thus various operational modes for the aircraft can be specified, depending on the variables which are of concern during a given flight phase. However, any trajectory of interest can be tracked using a suitably generated velocity signal denoted by  $U_d$ ,  $W_d$ , and  $Q_d$  where the subscript 'd' stands for desired trajectory. Trimming of an aircraft at a level flight condition is of vital importance to the pilot. The trim variables are also required to evaluate the desired trajectories as can be seen in the Appendix D. The responses obtained by the two controllers (M1 and M2) are then compared for the Tracking and Trimming modes. The velocity tracking is considered first.

### 3.5.1 Controller Design for Tracking Mode

In this case, the state equation (3.1) including the disturbances can be seen to be

$$\begin{pmatrix} \dot{U} \\ \dot{W} \\ \dot{Q} \\ \dot{\theta} \\ \dot{p}_x \\ \dot{p}_z \end{pmatrix} = \begin{pmatrix} -QW - g_0 \sin(\theta) \\ QU + g_0 \cos(\theta) \\ 0 \\ Q \\ U \cos(\theta) + W \sin(\theta) \\ U \sin(\theta) - W \cos(\theta) \end{pmatrix} + \begin{pmatrix} R_m F_x \\ R_m F_z \\ c_7 M \\ 0 \\ 0 \\ 0 \end{pmatrix} + \begin{pmatrix} d_U \\ d_W \\ d_Q \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad (3.27)$$

where,  $d_i$ ,  $i = U, W, Q$  represent the external disturbances and uncertainties entering in the channels denoted by the subscript  $i$  and their magnitudes are bounded by  $|d_i| < D_i$ . It is seen that, with  $\mathbf{y}^T = [U \ W \ Q]$  as the output vector, the above equation is already in the reduced form, with the first three components forming the matched dynamics (3.6) and the remaining three the unmatched dynamics (3.7). The ZD (3.26) in this case is thus given by

$$\begin{pmatrix} \dot{\theta} \\ \dot{p}_x \\ \dot{p}_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \quad (3.28)$$

Thus, the states of the ZD are in a neutral equilibrium, implying that the unmatched dynamics are bounded-input bounded-state (BIBS)

For both cases (C1 and C2), the  $\hat{B}_1$  matrix is seen from (3 27) to be

$$\hat{B}_1 = \text{diag}[\hat{R}_m, \hat{R}_m, \hat{c}_7], \quad (3 29)$$

where  $\text{diag}[\ ]$  denotes a diagonal matrix. Also, the  $\Delta_b$  matrix is seen to be  $\text{diag}[\delta_{b1}, \delta_{b1}, \delta_{b2}]$ . The vector  $\mathbf{S} = [S_U, S_W, S_Q]^T$  is as defined in (3 10). Following the steps as outlined in the previous section,  $I + \Delta_t$  in (3 15) can be simplified as

$$(I + \Delta_t) = \text{diag}[q_1, q_2, q_3], \quad (3 30)$$

where,  $q_1 = (1 + \delta_{b1})(1 + \delta_{ae}(1))$ ,  $q_2 = (1 + \delta_{b1})(1 + \delta_{ae}(2))$ , and  $q_3 = (1 + \delta_{b2})(1 + \delta_{ae}(3))$ . The  $\Delta_t$  matrix for the case C1 can be obtained by putting  $\delta_{ae}(i) = 0$  for  $i = 1, 2, 3$ . In this case the  $D_t$  matrix, which bounds the  $\Delta_t$  matrix in (3 30), is seen to be given by the bounds on  $\delta_{b1}$  and  $\delta_{b2}$  (given in the Appendix D) as

$$D_t = \text{diag}[1/3, 1/3, 3/7] \quad (3 31)$$

For the case C2, the  $I + \Delta_t$  matrix in (3 30) would attain its maximum (minimum) values when both the terms in the product individually take their maximum (minimum) values. Using the bounds as given in Appendix D, the elements of the diagonal matrix  $I + \Delta_t$  can be seen to vary within the following bounds

$$\begin{aligned} \frac{8}{15} &\leq 1 + \Delta_t(1, 1) \leq \frac{8}{5} \\ \frac{8}{15} &\leq 1 + \Delta_t(2, 2) \leq \frac{8}{5} \\ \frac{16}{35} &\leq 1 + \Delta_t(3, 3) \leq \frac{12}{7} \end{aligned} \quad (3 32)$$

from which, the  $D_t$  matrix bounding  $\Delta_t$  in (3 30) becomes

$$D_t = \text{diag}[3/5, 3/5, 5/7] \quad (3 33)$$

It is obvious that in both cases, all the eigenvalues of  $D_t$  are less than 1.0, thus guaranteeing the existence of  $k$  in (3 20). The positive scalar  $\eta_i$  in (3 18) has been taken to

be 1 0,  $i = 1, 2, 3$  With these choices, the  $3 \times 1$  vector  $\Psi$  in (3 21) can be seen to be

$$\begin{aligned}\Psi_1 &= \Psi(1) = 1 0 + D_U + D_t(1, 1)|U_d - QW + g_0 \sin(\theta)|, \\ \Psi_2 &= \Psi(2) = 1 0 + D_W + D_t(2, 2)|W_d - QU - g_0 \cos(\theta)|, \text{ and} \\ \Psi_3 &= \Psi(3) = 1 0 + D_Q + D_t(3, 3)|Q_d|\end{aligned}\quad (3 34)$$

Note that for the two cases **C1** and **C2**, different  $D_t$  as in (3 31) and (3 33) respectively have to be used

The  $3 \times 1$  vector  $\mathbf{k}$  in (3 20) can then be evaluated for the two cases as

$$1 \quad \mathbf{C1}: \mathbf{k}^T = [1.5\Psi_1, 1.5\Psi_2, 1.75\Psi_3], \text{ and}$$

$$2 \quad \mathbf{C2}: \mathbf{k}^T = [2.5\Psi_1, 2.5\Psi_2, 3.5\Psi_3]$$

The calculated values of  $\mathbf{k}$  are then used in (3 22) to obtain the control law as

$$\begin{aligned}F_{x_{com}} &= \frac{1}{\hat{R}_m} \left( U_d + QW + g_0 \sin(\theta) - k_1 \text{sat}\left[\frac{S_U}{\phi_U}\right] \right), \\ F_{z_{com}} &= \frac{1}{\hat{R}_m} \left( W_d - QU - g_0 \cos(\theta) - k_2 \text{sat}\left[\frac{S_W}{\phi_W}\right] \right), \text{ and} \\ M_{com} &= \frac{1}{\hat{c}_7} \left( Q_d - k_3 \text{sat}\left[\frac{S_Q}{\phi_Q}\right] \right)\end{aligned}\quad (3 35)$$

The boundary layer thicknesses ( $\phi_U, \phi_W$  and  $\phi_Q$ ) for the three outputs as used in the simulation are specified in the Appendix D. It can be seen that the state variables  $p_x$  and  $p_z$  are not used in the control law, however they constitute the ZD, and hence they have been included in the above development. Simulation has been done using a fourth order Runge-Kutta algorithm with the time step of 0.25ms. The aircraft is initially assumed to be in a trimmed level flight with a total velocity of 502 feet per second (fps). Till 0.5s, the elevator and throttle gear commands are maintained at their equilibrium values, and at this time instant the pilot increments the elevator by  $15^\circ$  and the throttle gear by 20 units and maintains them at a constant value till 2.0s.

The responses were obtained for two sets of uncertainties (UC1 and UC2, as specified in the Appendix D) for the two cases (**C1** and **C2**). The tracking error of the

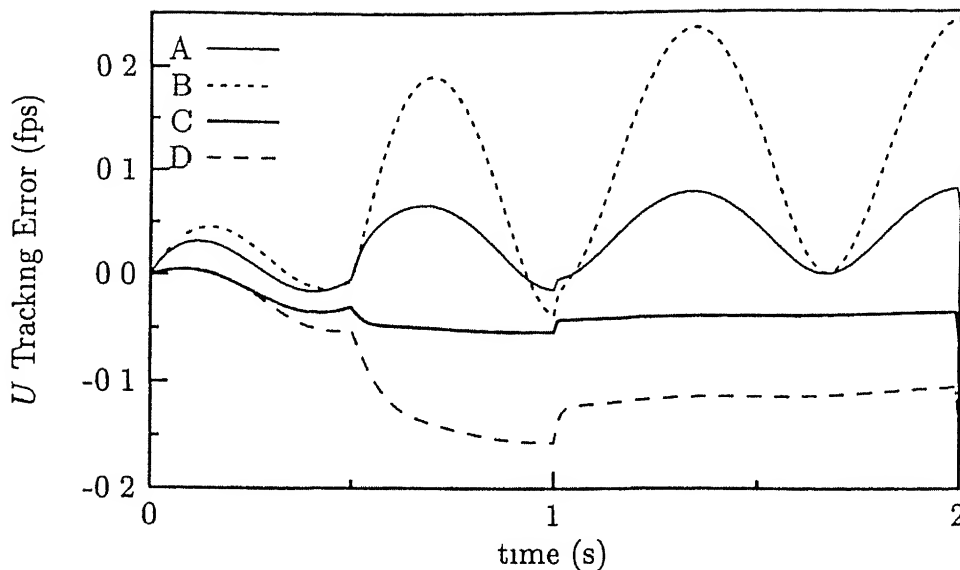


Fig. 3.2 Tracking error in  $U$  (fps)

outputs ( $U$ ,  $W$  and  $Q$ ) are shown in Figs 3.2, 3.3 and 3.4 respectively. In these figures, the solid lines labeled 'A' and 'C' correspond to the responses using the M2 controller for the uncertainties UC1 and UC2 respectively. Similarly the dashed lines 'B' and 'D' show the results using the controller M1 for UC1 and UC2 respectively. It is observed from the figures, that the output tracking error stays well within the specified boundary layer thickness and good tracking of the desired trajectory is achieved. From the figures, it is clear that the tracking errors in the case C2 are smaller than those of the case C1 for all the outputs. Although,  $\theta$  is not a tracked output, in the absence of unmatched uncertainties, it was found to be well tracked with a similar trend. Thus, the controller M2 clearly gives better performance as compared to the controller M1. Thus it is seen that ignoring the uncertainties involved in the force generation can lead to a degraded system performance.

The desired force command and the actually applied force vector, with the assumed uncertainty in aerodynamic inversion / modeling is shown in Figs 3.5, 3.6, and 3.7 for the UC1 uncertainty and case C2.

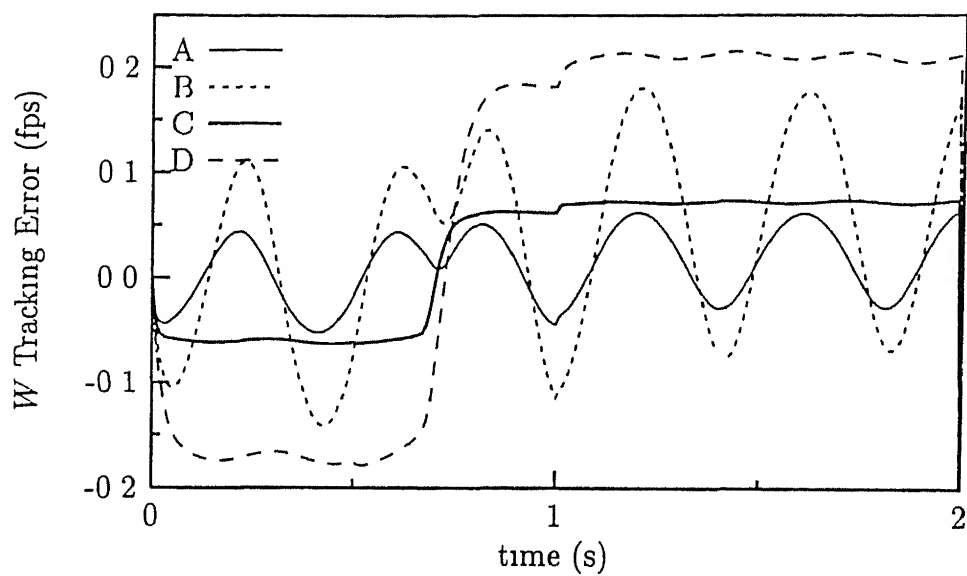


Fig 3.3 Tracking error in  $W$  (fps)

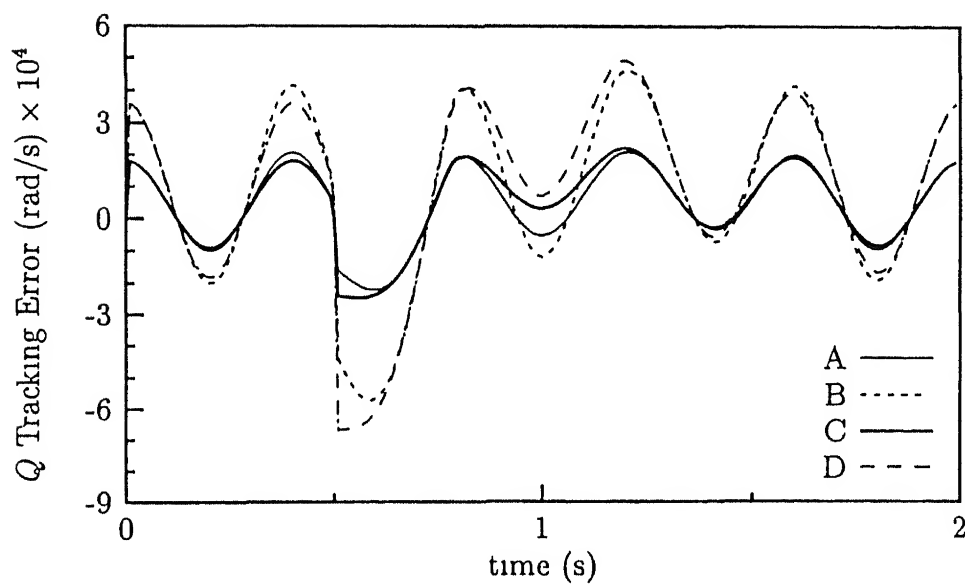


Fig. 3.4 Tracking error in  $Q$  (rad/s)

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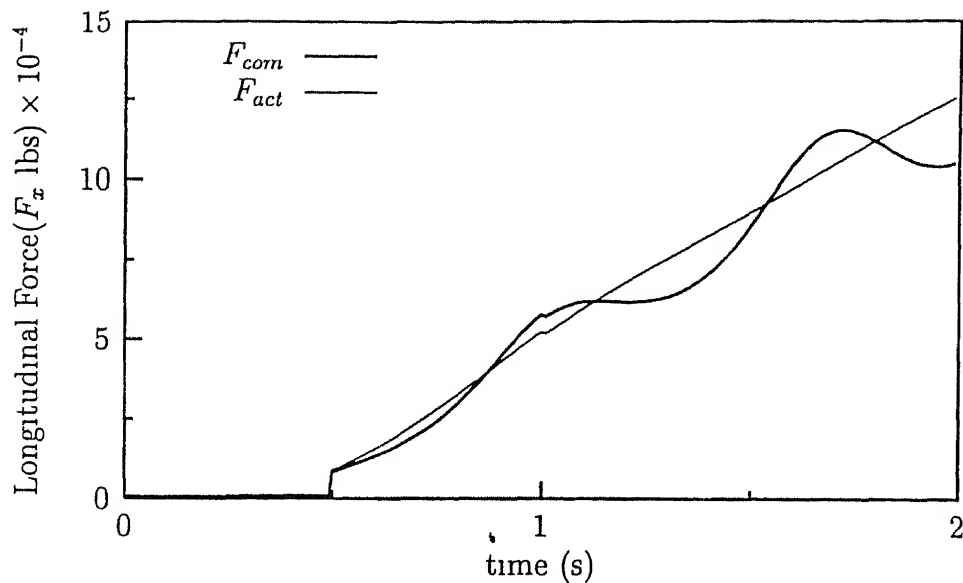


Fig 3.5 The command  $F_x$  ( $F_{com}$ ) and the actually realized force ( $F_{act}$ )

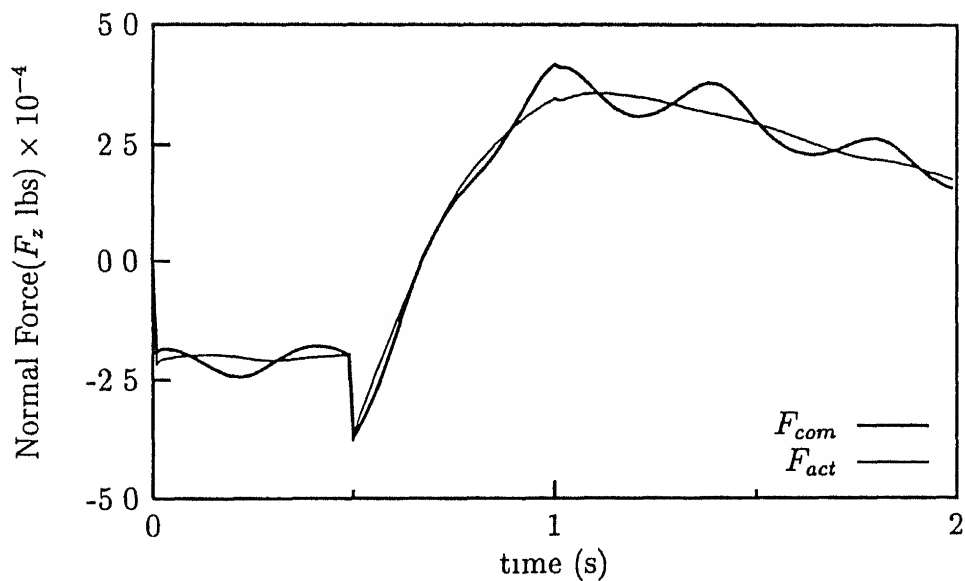


Fig. 3.6 The command  $F_z$  ( $F_{com}$ ) and the actually realized force ( $F_{act}$ )



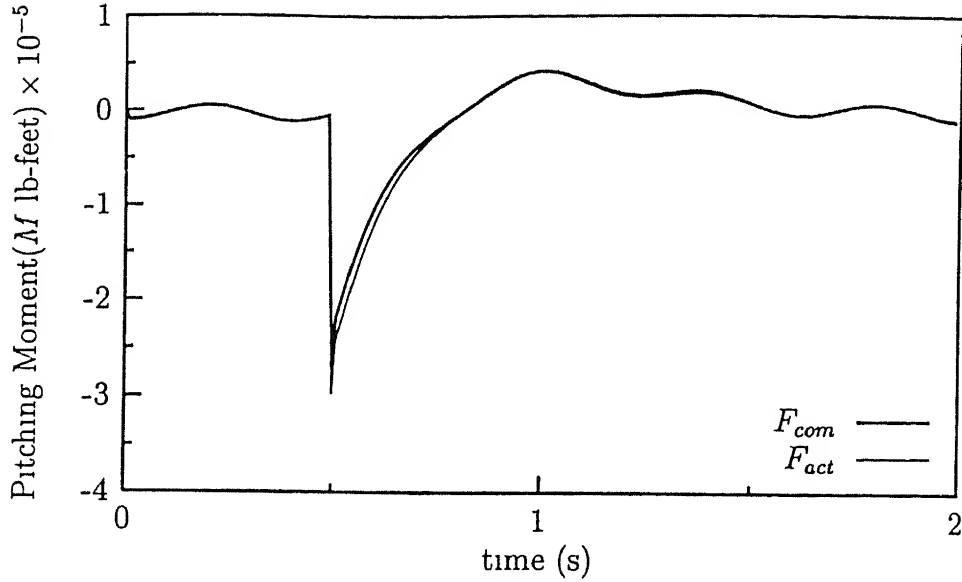


Fig. 3.7 The command  $M$  ( $M_{com}$ ) and the actually realized force ( $M_{act}$ )

### 3.5.2 Controller Design for Trim Mode

The trimming of an aircraft at a level flight condition requires that an equilibrium condition is reached at any given velocity. Most earlier works require a trim map or some algorithm [23] to generate the trimming variables. With the proposed design method this is not required. Given the velocity at which the aircraft is to be trimmed, the control law leads the aircraft states to the desired trim variables. The pilot is provided with a trim switch to trim the aircraft at the current value of the total forward velocity. Continuing with the simulation results in the previous section, the pilot activates the trim switch at  $t = 2.0$  s. The trimmed or the equilibrium state is defined as

$$\begin{pmatrix} V_t \\ \gamma \\ Q \end{pmatrix} = \begin{pmatrix} V_0 \\ 0 \\ 0 \end{pmatrix} \quad (3.36)$$

where,  $V_0$  is the desired trim velocity. In the above equation  $V_t = (U^2 + W^2)^{1/2}$  represents the total velocity,  $\alpha = \tan^{-1}(W/U)$  is called the angle of attack, and  $\gamma =$

$\theta - \alpha$  is the flight path angle. It is assumed that there are appropriate sensors to measure these quantities. Also define  $\mathbf{S} = [S_{V_t}, S_\gamma, S_Q]^T$  as the error function for the outputs as in (3.10). To track the outputs as defined in (3.36) the dynamic equations governing them need to be defined. These are given in standard textbooks [10] or can be directly obtained from the definitions of the outputs as above, and using (3.27). The state equation in the new set of coordinates,  $\mathbf{z}^T = [V_t \ \gamma \ Q \ \theta \ p_x \ p_z]$ , may be written as

$$\begin{pmatrix} \dot{V}_t \\ \dot{\gamma} \\ \dot{Q} \\ \dot{\theta} \\ \dot{p}_x \\ \dot{p}_z \end{pmatrix} = \begin{pmatrix} -g_0 \sin(\gamma) \\ -g_0 \cos(\gamma) \\ 0 \\ Q \\ V_t \cos(\gamma) \\ V_t \sin(\gamma) \end{pmatrix} + \begin{bmatrix} R_m \cos(\alpha) & R_m \sin(\alpha) & 0 \\ R_m \sin(\alpha) & -R_m \cos(\alpha) & 0 \\ 0 & 0 & c_\gamma \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{pmatrix} F_x \\ F_z \\ M \end{pmatrix} + \begin{pmatrix} d_{V_t} \\ d_\gamma \\ d_Q \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad (3.37)$$

where,  $d_{V_t}$ ,  $d_\gamma$ , and  $d_Q$  represent the matched external disturbances and can be evaluated as

$$\begin{aligned} d_{V_t} &= d_U \cos(\alpha) + d_W \sin(\alpha), \\ d_\gamma &= d_U \sin(\alpha) - d_W \cos(\alpha), \text{ and} \\ d_Q &= d_Q \end{aligned} \quad (3.38)$$

Their bounds change to

$$\begin{aligned} D_{V_t} &= D_U + D_W, \\ D_\gamma &= D_U + D_W, \text{ and} \\ D_Q &= D_Q \end{aligned} \quad (3.39)$$

It is seen that, with  $\mathbf{y}^T = [V_t \ \gamma \ Q]$  as the output vector, (3.37) is already in the reduced form as before with the first three equations defining the matched dynamics and the remaining unmatched dynamics. Also the ZD in this case are the same as in (3.28). Thus the unmatched dynamics is BIBS.

For the system (3 37) the input distribution matrix (denoted by  $\mathbf{B}'_1$ ), corresponding to the  $\mathbf{B}_1$  in (3 6), is defined in the first three equations in (3 37), and the nominal  $\hat{\mathbf{B}}'_1$  matrix is seen to be given as

$$\hat{\mathbf{B}}'_1 = \begin{bmatrix} \hat{R}_m \cos(\alpha) & \hat{R}_m \sin(\alpha) & 0 \\ \hat{R}_m \sin(\alpha) & -\hat{R}_m \cos(\alpha) & 0 \\ 0 & 0 & \hat{c}_7 \end{bmatrix} \quad (3 40)$$

for both the cases. It is easily verified that  $\hat{\mathbf{B}}'_1$  matrix above is invertible over the entire state space and the chosen parameter range. The  $\Delta_b$  matrix is the same as in the tracking mode. Following the steps as in the previous section,  $I + \Delta_t$  in (3 15), can be obtained as

$$(I + \Delta_t) = \begin{bmatrix} (1 + \delta_{b1})q_1 & \frac{1}{2}(1 + \delta_{b1})q_2 & 0 \\ \frac{1}{2}(1 + \delta_{b1})q_2 & (1 + \delta_{b1})q_3 & 0 \\ 0 & 0 & (1 + \delta_{b2})(1 + \delta_{ae}(3)) \end{bmatrix} \quad (3 41)$$

where,  $q_1 = (1 + \delta_{ae}(1) \cos^2(\alpha) + \delta_{ae}(2) \sin^2(\alpha))$ ,  $q_2 = (\delta_{ae}(1) - \delta_{ae}(2)) \sin(2\alpha)$ , and  $q_3 = (1 + \delta_{ae}(1) \sin^2(\alpha) + \delta_{ae}(2) \cos^2(\alpha))$

Note that for the case **C1** with  $\Delta_{ae} = 0$ ,  $q_1 = q_3 = 1$  and  $q_2 = 0$ . With this, the matrix  $D_t$  for this case is seen to be the same as in the tracking mode and is given in (3 31)

For the case **C2**, with  $\Delta_{ae}(i) \neq 0$  using the bounds as given in the Appendix D, it is seen that the  $q_1, q_2$  and  $q_3$  as defined above are bounded as

$$\begin{aligned} \frac{4}{5} &\leq q_1 \leq \frac{6}{5} \\ \frac{-2}{5} &\leq q_2 \leq \frac{2}{5} \\ \frac{4}{5} &\leq q_3 \leq \frac{6}{5} \end{aligned} \quad (3 42)$$

Proceeding as in the previous section, the components of the symmetric  $I + \Delta_t$  matrix in (3 41) are seen to assume values as given by

$$\frac{8}{15} \leq [I + \Delta_t](1, 1) \leq \frac{8}{5}$$

$$\begin{aligned}
\frac{-2}{15} &\leq [I + \Delta_t](1, 2) \leq \frac{4}{15} \\
\frac{8}{15} &\leq [I + \Delta_t](2, 2) \leq \frac{8}{5} \\
\frac{16}{35} &\leq [I + \Delta_t](3, 3) \leq \frac{12}{7}
\end{aligned} \tag{3 43}$$

From the above equation, a  $3 \times 3$  bounding matrix  $D_t$  can be selected as

$$D_t = \begin{bmatrix} 3/5 & 4/15 & 0 \\ 4/15 & 3/5 & 0 \\ 0 & 0 & 5/7 \end{bmatrix} \tag{3 44}$$

It can be easily verified that for both the cases, all the eigenvalues of  $D_t$  are less than 1.0. The  $\Psi$  vector (3 21) in this mode becomes

$$\begin{aligned}
\Psi_1 &= 1.0 + D_{V_t} + g_0 D_t(1, 1) |\sin(\gamma)| + g_0 D_t(1, 2) |\cos(\gamma)|, \\
\Psi_2 &= 1.0 + D_\gamma + g_0 D_t(2, 1) |\sin(\gamma)| + g_0 D_t(2, 2) |\cos(\gamma)|, \text{ and} \\
\Psi_3 &= 1.0 + D_Q + D_t(3, 3)
\end{aligned} \tag{3 45}$$

with the time derivatives of the outputs (i.e.  $V_{td}$ ,  $\gamma_d$ , and  $Q_d$ ) taken to be zero. Using the  $D_t$  in (3 31) and (3 44) for the cases C1 and C2 respectively, the  $\mathbf{k}$  in (3 20) can be evaluated in the two cases as

1. C1:  $\mathbf{k}^T = [1.5\Psi_1, 1.5\Psi_2, 1.75\Psi_3]$ , and
2. C2:  $\mathbf{k}^T = [4.5\Psi_1 + 3.0\Psi_2, 3.0\Psi_1 + 4.5\Psi_2, 3.5\Psi_3]$

Using the  $\mathbf{k}$  as above and the inverse of the  $\hat{\mathbf{B}}'_1$  matrix in (3 40) in (3 22) gives the control law as

$$\begin{aligned}
F_{x_{com}} &= \frac{g_0}{\hat{R}_m} \sin(\theta) - \frac{1}{\hat{R}_m} \left[ k_1 \text{sat}\left[\frac{S_{V_t}}{\phi_{V_t}}\right] \cos(\alpha) + k_2 \text{sat}\left[\frac{S_\gamma}{\phi_\gamma}\right] \sin(\alpha) \right], \\
F_{z_{com}} &= -\frac{g_0}{\hat{R}_m} \cos(\theta) - \frac{1}{\hat{R}_m} \left[ k_1 \text{sat}\left[\frac{S_{V_t}}{\phi_{V_t}}\right] \sin(\alpha) - k_2 \text{sat}\left[\frac{S_\gamma}{\phi_\gamma}\right] \cos(\alpha) \right], \\
M_{com} &= -\frac{1}{\hat{c}_7} k_3 \text{sat}\left[\frac{S_Q}{\phi_Q}\right],
\end{aligned} \tag{3 46}$$

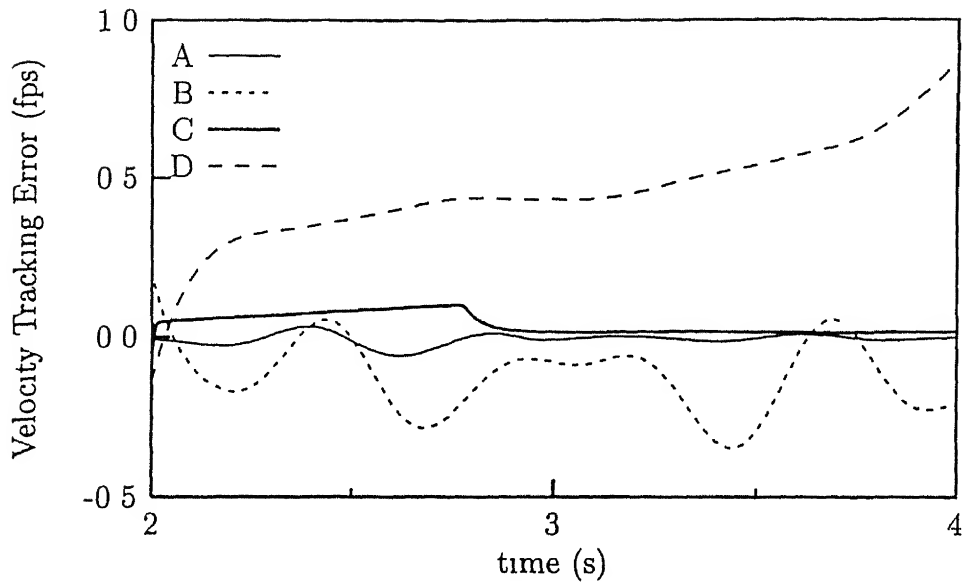


Fig. 3.8  $V_t$  tracking error in the Trimming mode (fps)

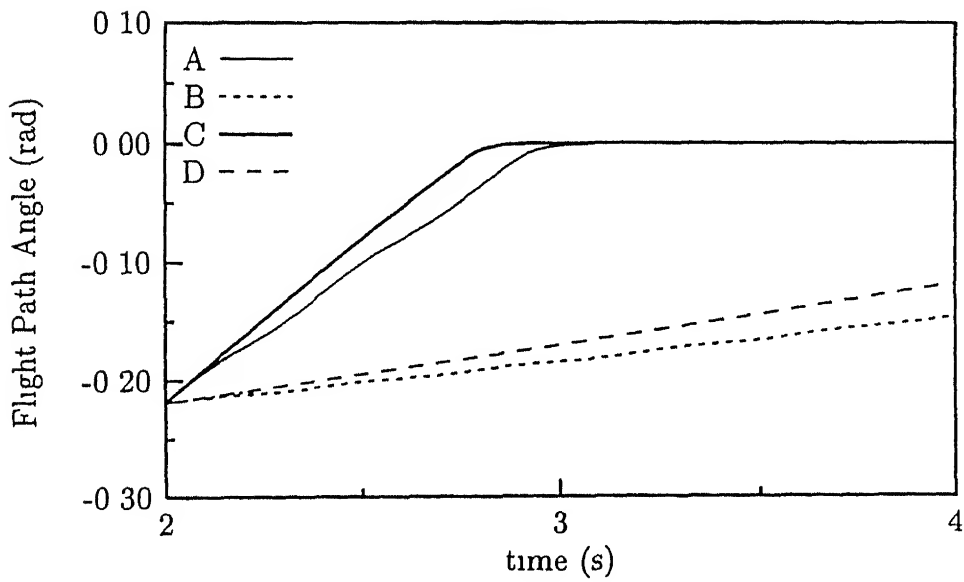


Fig. 3.9 Flight path angle ( $\gamma$ ) response in the Trimming mode (rad)

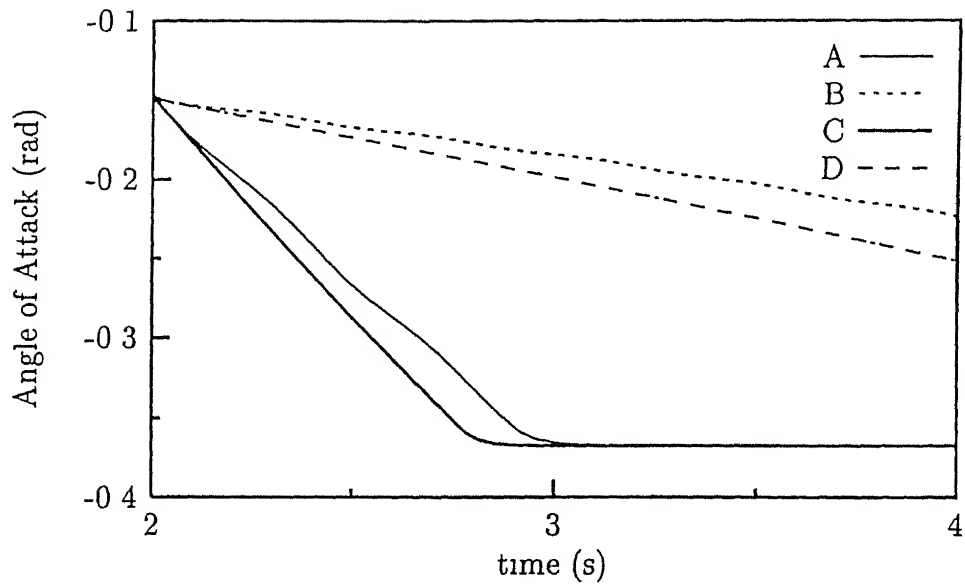


Fig. 3.10 Angle of attack ( $\alpha$ ) response in the Trimming mode (rad)

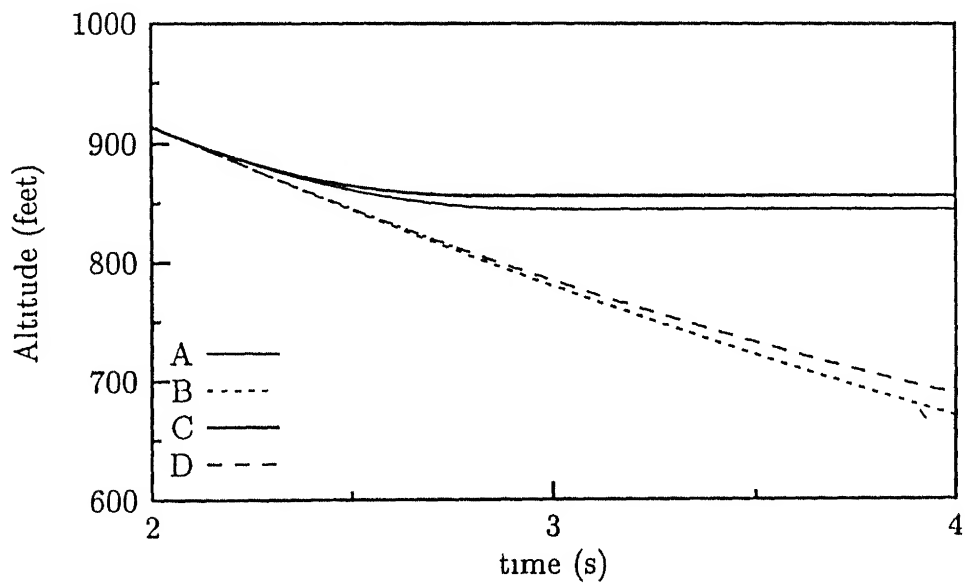


Fig. 3.11 Altitude ( $p_z$  (ft)) response in the Trimming mode

## 3.6 Conclusions

In this chapter, the robust nonlinear control law design for the nonlinear longitudinal dynamics of a fighter aircraft, based on a model following sliding mode approach and using a full state feedback, is presented. The components of the force vector are considered as inputs to the aircraft, with the assumption that a desired force vector can be generated using appropriate control surface deflections. An error between the commanded force vector and the actually obtained force vector is considered, which is in contrast to the assumptions made in the literature. The MF-SMC method is extended to include this uncertainty. Simulation results show that ignoring this uncertainty in the controller design may lead to substantial loss in performance. All other uncertainties and disturbances are assumed to satisfy the matching conditions. Analytical expressions for the control laws for two operational modes, namely the velocity tracking and the trimming are derived. It can be seen from the developed control laws for the two modes in (3.35) and (3.46) that they depend on the estimated mass and inertia parameters and their expected range of variation only. In a preliminary aircraft design project, these control laws can thus be used to generate the required forces and moments for some critical flight maneuvers which can be placed as targets to the aerodynamics and the propulsion groups. This would enable the control group to have a more active role in such an exercise, and help in achieving the best possible performance from the airframe. Numerical simulations on a fighter aircraft show the robustness of the control law. An interesting feature of the trimming control law is that it does not require an algorithm or a trim map to specify the trim variables.

# Chapter 4

## Multi-Loop SMC Laws for The Unmatched Uncertainty Case

### 4.1 Introduction

In the previous chapter, controller design for output tracking with matched uncertainty and disturbances was considered. As seen there, the number of trackable outputs are limited by the number of independent inputs available. This leaves out a portion of the dynamics, also called the internal dynamics, and is seen from (3.7) to be a function of the tracked outputs and the internal states. An approach to control these internal states was to formulate the aircraft dynamics as a two time scale problem and use a multi-loop (ML) strategy. The state vector was thus separated into fast and slow variables [49, 50] and a dynamic inversion based inner loop control law was then designed for the fast variables. With the command signals for the fast variables as the input, an outer loop control law is designed to track the slow states, which gives the command signals to be tracked in the inner loop. The inversion based control law was reported to give better responses as compared to a gain-scheduled linear law [49]. Analysis for robustness was, however, not performed. Azam and Singh [50] used an integral error feedback in the outer loop for robustness against parameter variations. Both of the works cited above use conventional control surfaces as inputs and hence were limited to track the angular velocities in the inner loop and corresponding angular states in the outer loop. However, with the force control approach (Section 3.2), control



of the entire state vector is possible, as is shown in this chapter

The presence of unmatched disturbances and uncertainties,  $\mathbf{d}_2$  in (3.7) in the internal states, which was neglected in the works cited above, is a practical problem and leads to a degraded system performance. This chapter deals with the design of SMC laws in the presence of unmatched uncertainties using the ML strategy. A basic assumption used in this work is that the nominal unmatched dynamics are assumed to be acceptable. Accordingly, tracking of the position state variables is accomplished in the outer loop considering the command velocity signals as the inputs. A SMC law is designed in the inner loop so that the velocity states track these augmented velocity commands generated in the outer loops. The ML strategy is shown to lead to a simpler propagation of disturbances in the outer loop to the inner loop using which robustness properties are evaluated in terms of the bounds on the tracking errors in the inner and the outer loops. Simulation results for the nonlinear longitudinal dynamics of an aircraft are then presented. The ML strategy is next applied to a higher order SISO system with unmatched disturbances and uncertainties. The developments herein can be seen to be giving results similar to those of [67, 68] which uses the singular perturbation methods (SPMs). The SMC design method presented here requires the knowledge of the bounds as in the previous works [67, 68]. It is shown that the conventional SMC design, with the modified way of selecting the switching gains, may be used to handle this problem.

## 4.2 ML Strategy for Mechanical Systems

Many mechanical systems may be represented in the reduced form as in (3.6) and (3.7) as

$$\mathbf{V} = \mathbf{f}_1(\mathbf{X}, \mathbf{V}) + \mathbf{B}_1(\mathbf{X}, \mathbf{V})\mathbf{u} + \mathbf{d}_1, \quad (4.1)$$

$$\mathbf{X} = \mathbf{f}_2(\mathbf{X}, \mathbf{V}) + \mathbf{d}_2 \quad (4.2)$$

where  $\mathbf{X}, \mathbf{V}$  and  $\mathbf{u} \in \mathcal{R}^n$  represent the position and velocity state variables and the input vectors respectively, and  $\mathbf{d}_1$  and  $\mathbf{d}_2$  represent the combined influence of the exter-

nal disturbance and uncertainty vector and are given to be bounded  $d_i$ , representing the  $j^{th}$  component of the disturbance vector  $\mathbf{d}_i$  is bounded as  $|d_{i,j}| \leq D_{i,j}$ ,  $i = 1, 2$ ,  $j = 1, \dots, n$ . Let  $\mathbf{Z} = [\mathbf{X}^T \mathbf{V}^T]^T$ . Also  $\mathbf{B}_1(\mathbf{Z})$  is assumed to be of full rank over the entire state space. The other assumptions in Section 3.4 for matrix  $\mathbf{B}_1$  hold in this chapter. It is clear from the above system equation that with the velocity variables as the output, it has a strong relative degree of 1. Also, the above nonlinear system is seen to be in the reduced form [37, 52]. The arguments of the various functions defined above are dropped if no confusion is likely to arise.

As in the Section 3.4, (4.1) represents the matched dynamics and (4.2) gives the unmatched portion of the dynamics. The ZD, for the class of systems defined above, were seen to be a special case of the unmatched dynamics (3.26). These equations in such systems generally are integrators of the velocity variables and as seen in the aircraft examples in Sections 3.5.1 and 3.5.2 are BIBS. It is also seen from the system equation in (3.27) in Section 3.5.1 that the term  $\mathbf{f}_2(\mathbf{X}, \mathbf{V})$  is actually separable in  $\mathbf{X}$  and  $\mathbf{V}$ , i.e. it may be represented as  $\mathbf{B}_2(\mathbf{X})\mathbf{V}$ . Thus (4.2) may be rewritten as

$$\dot{\mathbf{X}} = \mathbf{B}_2(\mathbf{X})\mathbf{V} + \mathbf{d}_2 \quad (4.3)$$

The earlier control laws (in Section 3.4) were designed neglecting the presence of  $\mathbf{d}_2$ . In this section, a ML strategy for the SMC is presented. It is assumed that the desired trajectories for the velocity variables are specified  $(\mathbf{V}_d, \dot{\mathbf{V}}_d)$  and the associated desired position trajectories given by the nominal  $\mathbf{X}$  dynamics (4.2) as

$$\dot{\mathbf{X}}_d = \mathbf{B}_2(\mathbf{X}_d)\mathbf{V}_d \quad (4.4)$$

are acceptable. For notational simplicity,  $\mathbf{B}_{2d}$  will be taken to represent  $\mathbf{B}_2(\mathbf{X}_d)$ , and similarly  $\mathbf{B}_2 = \mathbf{B}_2(\mathbf{X})$  from now on. It is further required that  $\mathbf{B}_2$  be nonsingular everywhere.

The ML control scheme is shown in Fig. 4.1. As can be seen from the figure an inner loop is used to synthesize  $\mathbf{u}_{com}$  such that the velocity variables track an augmented signal  $\mathbf{V}_a$  instead of the conventional  $\mathbf{V}_d$ . The outer loop is used to create the augmented signal for the inner loop such that the position tracking is within acceptable

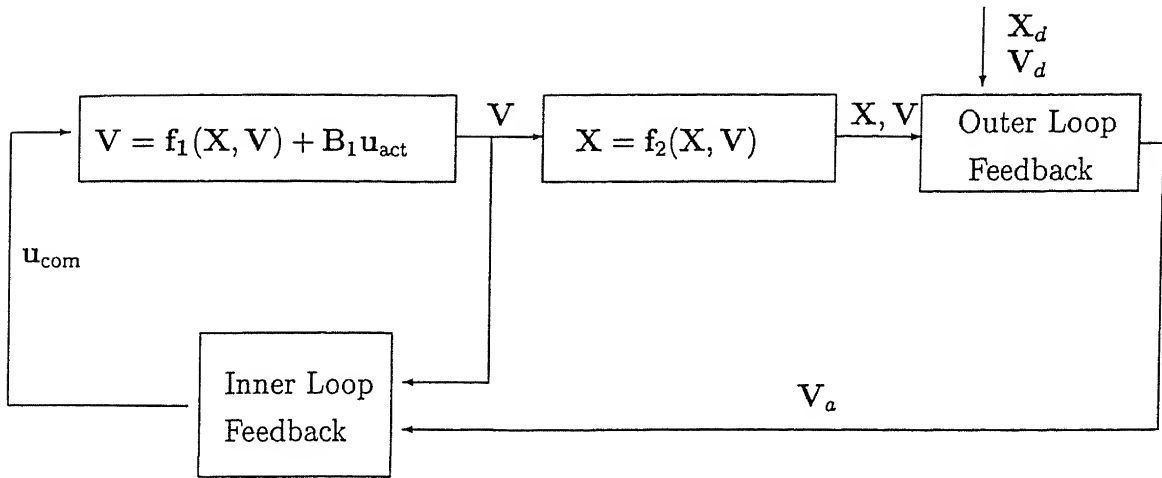


Fig. 4 1 Schematic Multi-Loop Control Scheme

bounds. Accordingly bounds on the tracking errors in the inner and outer loops are developed as follows

Define  $S_x$  and  $S_v$  as vectors consisting of the error function for the position and velocity variables as

$$S_x = X - X_d, \text{ and} \quad (4.5)$$

$$S_v = V - V_a, \quad (4.6)$$

where,  $V_a$  is yet to be defined. Taking the time derivative of  $S_x$  and using (4.3),  $S_x$  becomes

$$S_x = B_2 V + d_2 - B_{2d} V_d \quad (4.7)$$

Using  $V = V_a + S_v$  from (4.6) in the above equation gives

$$S_x = B_2 V_a + B_2 S_v + d_2 - B_{2d} V_d \quad (4.8)$$

Note that the time derivative of  $V_a$  would be required for  $V$  to track  $V_a$  in the inner loop, therefore  $V_a$  should not have discontinuities and should be selected so as to make  $S_x$  as small as possible. With the invertibility condition on  $B_2$ , the command signal  $V_a$  for the inner loop is selected from (4.8) to cancel out the known terms and by

introducing a stabilizing feedback as

$$\mathbf{V}_a = \mathbf{B}_2^{-1}(\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x), \quad (4.9)$$

where,  $\mathbf{K}_x\mathbf{S}_x \in \mathcal{R}^n$  with its  $i^{th}$  component as  $[\mathbf{K}_x\mathbf{S}_x]_i = K_{x_i}S_{x_i}$  and  $K_{x_i} > 0$ ,  $i = 1, \dots, n$ .  $\mathbf{K}_x$  is taken as a  $n \times n$  real matrix as  $\text{diag}[K_{x_1}, \dots, K_{x_n}]$

Using the  $\mathbf{V}_a$  selected above in (4.8) gives  $\mathbf{S}_x$  as

$$\mathbf{S}_x = -\mathbf{K}_x\mathbf{S}_x + \mathbf{B}_2\mathbf{S}_v + \mathbf{d}_2, \quad (4.10)$$

which is rewritten as

$$\mathbf{S}_x = \mathbf{T}_x + \mathbf{d}_2 \quad (4.11)$$

for simplicity, and  $\mathbf{T}_x$  is obviously defined. The  $S_{x_i}$  is thus seen to have the dynamics given by

$$S_{x_i} = -K_{x_i}S_{x_i} + [\mathbf{B}_2\mathbf{S}_v]_i + d_{2_i} \quad (4.12)$$

The assumption of  $\mathbf{f}_2 = \mathbf{B}_2\mathbf{V}$  has been used in the selection of  $\mathbf{V}_a$  in (4.9). However, only the existence of the following map guarantees that there would exist a unique  $\mathbf{V}_a$ , such that

$$\mathbf{f}_2(\mathbf{X}, \mathbf{V}_a) = \mathbf{f}_2(\mathbf{X}_d, \mathbf{V}_d) - \mathbf{K}_x\mathbf{S}_x \quad (4.13)$$

From (4.12), it is seen that any bounds on the position error  $\mathbf{S}_x$  depend on the velocity error  $\mathbf{S}_v$ . Hence, it is first necessary to check the  $\mathbf{S}_v$  dynamics before any estimates of the  $\mathbf{S}_x$  bounds can be made. The time derivative of the  $\mathbf{V}_a$  in (4.9) would be required for  $\mathbf{V}$  to track  $\mathbf{V}_a$  in the inner loop. Snell et al [49] used a band limited filter to generate this time derivative. Azam and Singh [50] used the nominal system equations (4.1) and (4.3) to evaluate the derivative. However, the effect of disturbances and uncertainties was not directly considered in their study. The time derivative of  $\mathbf{V}_a$  is obtained from (4.9) as

$$\dot{\mathbf{V}}_a = \frac{d}{dt}[\mathbf{B}_2^{-1}](\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x) + \mathbf{B}_2^{-1}\frac{d}{dt}[\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x] \quad (4.14)$$

The definitions and notations used in the present work to calculate the time derivatives of scalar, vector, and matrix functions of vectors are given in Appendix E. A well

known result in matrix theory [69] gives that for a nonsingular matrix  $\mathbf{B}_2$

$$\frac{d}{dt}[\mathbf{B}_2^{-1}] = -\mathbf{B}_2^{-1}\left[\frac{d}{dt}\mathbf{B}_2\right]\mathbf{B}_2^{-1} \quad (4.15)$$

Using the notation in (E 8) from Appendix E, the time derivative of  $\mathbf{B}_2$  in the above equation is seen to be

$$\frac{d}{dt}[\mathbf{B}_2] = J_{B_2}[\mathbf{I}_n \otimes \mathbf{X}], \quad (4.16)$$

where  $\otimes$  represents the Kronecker product. From (4.2), it is observed that  $\mathbf{X} = \mathbf{f}_2 + \mathbf{d}_2$ .

Substituting this in the above equation gives

$$\frac{d}{dt}[\mathbf{B}_2] = J_{B_2}[\mathbf{I}_n \otimes \mathbf{f}_2] + J_{B_2}[\mathbf{I}_n \otimes \mathbf{d}_2] \quad (4.17)$$

Using (4.15) and (4.17) and  $\mathbf{S}_x = \mathbf{T}_x + \mathbf{d}_2$  from (4.11),  $\mathbf{V}_a$  in (4.14) becomes

$$\begin{aligned} \mathbf{V}_a &= -\mathbf{B}_2^{-1}\frac{d}{dt}[\mathbf{B}_2]\mathbf{B}_2^{-1}(\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x) + \mathbf{B}_2^{-1}\left(\frac{d}{dt}[\mathbf{B}_{2d}\mathbf{V}_d] - \mathbf{K}_x\mathbf{S}_x\right) \\ &= \mathbf{B}_2^{-1}\left[\left(\frac{d}{dt}[\mathbf{B}_{2d}\mathbf{V}_d] - \mathbf{K}_x\mathbf{T}_x - \mathbf{K}_x\mathbf{d}_2\right) \right. \\ &\quad \left. - (J_{B_2}[\mathbf{I}_n \otimes \mathbf{f}_2] + J_{B_2}[\mathbf{I}_n \otimes \mathbf{d}_2])\mathbf{B}_2^{-1}(\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x)\right], \end{aligned} \quad (4.18)$$

which may be rewritten as

$$\begin{aligned} \mathbf{V}_a &= \mathbf{B}_2^{-1}\left(\frac{d}{dt}[\mathbf{B}_{2d}\mathbf{V}_d] - \mathbf{K}_x\mathbf{T}_x - J_{B_2}[\mathbf{I}_n \otimes \mathbf{f}_2]\mathbf{B}_2^{-1}(\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x)\right) \\ &\quad - \mathbf{B}_2^{-1}\left(\mathbf{K}_x\mathbf{d}_2 + J_{B_2}[\mathbf{I}_n \otimes \mathbf{d}_2]\mathbf{B}_2^{-1}(\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x)\right) \end{aligned} \quad (4.19)$$

The above equation may be expressed as

$$\mathbf{V}_a = \mathbf{T}_a + \mathbf{d}'_2, \quad (4.20)$$

where

$$\mathbf{T}_a = \mathbf{B}_2^{-1}\left(\frac{d}{dt}[\mathbf{B}_{2d}\mathbf{V}_d] - \mathbf{K}_x\mathbf{T}_x - J_{B_2}[\mathbf{I}_n \otimes \mathbf{f}_2]\mathbf{B}_2^{-1}(\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x)\right), \quad (4.21)$$

$$\text{and } \mathbf{d}'_2 = -\mathbf{B}_2^{-1}\left(\mathbf{K}_x\mathbf{d}_2 + J_{B_2}[\mathbf{I}_n \otimes \mathbf{d}_2]\mathbf{B}_2^{-1}(\mathbf{B}_{2d}\mathbf{V}_d - \mathbf{K}_x\mathbf{S}_x)\right) \quad (4.22)$$

It is seen from the above equation that  $\mathbf{d}'_2$  contains the effects of disturbance terms  $\mathbf{d}_2$ , which was not considered in [50].

The dynamics of  $\mathbf{S}_v$  may now be considered. The time derivative of  $\mathbf{S}_v$  in (4.6) is seen to be  $\dot{\mathbf{S}}_v = \mathbf{V} - \mathbf{V}_a$ , and using (4.1) and (4.20) it becomes

$$\dot{\mathbf{S}}_v = \mathbf{f}_1 + \mathbf{B}_1 \mathbf{u} - \mathbf{T}_a + \mathbf{d}_1 - \mathbf{d}_2' \quad (4.23)$$

Thus, it is seen that a ML strategy passes on the effect of the disturbances  $\mathbf{d}_2$  in the outer loop to the inner loop as  $\mathbf{d}_2'$  (4.22) as in the above equation, which can then be incorporated in the design process. Using the augmented disturbance signal, the SMC as in (3.22) may still be designed by following the steps outlined in Section 3.4.  $\mathbf{S}_{v_i}$  can thus be made to satisfy the reaching condition as in (3.18) and the  $\mathbf{S}_{v_i}$  response is guaranteed to be better than

$$\dot{S}_{v_i} = -\eta_{v_i} \text{sgn}[S_{v_i}] \quad (4.24)$$

as in (3.19). As in Section 3.4, the  $\text{sgn}[\cdot]$  term is replaced by a continuous term  $\text{sat}(S_{v_i}/\phi_{v_i})$ , where  $\phi_{v_i}$  represents the  $i^{\text{th}}$  component of the selected boundary layer thickness vector  $(\Phi_v)$ . With the reaching times  $t_{0_i}$  as given in (3.25), all the  $S_{v_i}$ 's will be bounded after some finite time  $t_{0_m}$  ( $= \max[t_{0_i}, i = 1, \dots, n]$ , where  $\max[\cdot, \dots, \cdot]$  gives the maximum of its arguments) as

$$|S_{v_i}| \leq \phi_{v_i} \quad (4.25)$$

With the velocity error  $\mathbf{S}_v$  bounded as above, the effect of the  $[\mathbf{B}_2 \mathbf{S}_v]_i$  term in the  $S_{x_i}$  dynamics in (4.12) is seen to be bounded by the sum  $\sum_j (|\mathbf{B}_2|_{ij} \phi_{v_j})$  and may be considered as an additional disturbance term for all  $t > t_{0_m}$ . It can be shown that the error  $S_{x_i}$  is globally uniformly ultimately bounded (see Appendix F) as

$$|S_{x_i}| \leq \frac{[|\mathbf{B}_2| \Phi_v + \mathbf{D}_2]_i}{K_{x_i}} \quad (4.26)$$

Thus it is seen that the  $\mathbf{S}_x$  and  $\mathbf{S}_v$  errors defined in (4.5) and (4.6) remain within bounds as specified in (4.26) and (4.25) respectively. The bounds on  $\mathbf{S}_v$  (4.25) is directly governed by the choice of  $\Phi_v$ . The bound on  $\mathbf{S}_x$  (4.26) may be lowered by choosing a higher value for the  $K_{x_i}$ , however, it is observed that the bound on  $K_{x_i} S_{x_i}$  does not change. It directly depends on the size of the unmatched uncertainties  $\mathbf{D}_2$  and the selected boundary layer thicknesses  $\Phi_v$ .

Another point of interest is to find out the magnitude of the difference between the  $V_d$  and  $V_a$  signals. From (4.9) it is seen that

$$V_d - V_a = [I - B_2^{-1}B_{2d}]V_d + B_2^{-1}K_x S_x \quad (4.27)$$

The difference  $V_d - V_a$  is seen to be equal to 0 if and only if  $S_x = 0$ , since it also implies that  $B_2^{-1}B_{2d} = I$ . However, as  $S_x$  is only guaranteed to be within some bounds, there will be a finite error between the two signals.

Thus it is seen that the SMC method can be applied to the unmatched uncertainty case using a ML framework and bounds for the errors in the loops may be derived as shown here. The method developed for a general mechanical system is next validated by applying it to the aircraft longitudinal dynamics.

### 4.3 SMC Design for Aircraft Velocity Tracking

In this section, the ML controller design for the unmatched uncertainty case as discussed in the previous section is applied to the aircraft example in Section 3.5.1. The state equations for this case are already reported in (3.27). The matched dynamics representing the velocity dynamics in (4.1) remain the same as earlier. Thus, the  $V$  in this chapter represents the velocity vector  $[U, W, Q]^T$ . However, the unmatched uncertainties, which were not considered in Chapter 3, appear in the  $X$  dynamics as in (4.2). Rearranging the last three equations of (3.27) with the corresponding states being given by  $X = [p_x, p_z, \theta]^T$ , the governing equations may be rewritten as

$$\begin{pmatrix} \dot{p}_x \\ \dot{p}_z \\ \dot{\theta} \end{pmatrix} = \begin{pmatrix} U \cos(\theta) + W \sin(\theta) \\ U \sin(\theta) - W \cos(\theta) \\ Q \end{pmatrix} + \begin{pmatrix} d_{2x} \\ d_{2z} \\ d_{2\theta} \end{pmatrix} \quad (4.28)$$

The  $f_2$  as defined in (4.2) is seen from the above equation as

$$f_2 = \begin{bmatrix} \cos(\theta) & \sin(\theta) & 0 \\ \sin(\theta) & -\cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{pmatrix} U \\ W \\ Q \end{pmatrix} = B_2 V \quad (4.29)$$

From the above equation, it is seen that the position state dynamics  $\mathbf{X}$  as given in (4 28) is in the form of (4 3). It is easily verified that the matrix  $\mathbf{B}_2$  in the above equation is non-singular. As in Section 3 5 1, the nominal ZD (3 28) is seen to be BIBS.

The error  $\mathbf{S}_x$  (4 5) in the position variables is defined as  $[S_x, S_z, S_\theta]^T$  and is given by

$$\begin{pmatrix} S_x \\ S_z \\ S_\theta \end{pmatrix} = \begin{pmatrix} p_x - p_{xd} \\ p_z - p_{zd} \\ \theta - \theta_d \end{pmatrix} \quad (4 30)$$

Note that  $\mathbf{S}_x$  represents a vector quantity, whereas the  $S_x$  is a scalar quantifying the  $x$  position error. Similarly,  $\mathbf{K}_x$  represents  $\text{diag}[K_x, K_z, K_\theta]$ . While  $K_x$  is a scalar quantity representing the feedback gain of  $S_x$ , the  $\mathbf{K}_x$  is a  $3 \times 3$  matrix. Similarly, the velocity error  $\mathbf{S}_v = \mathbf{V} - \mathbf{V}_a$  in (4 6), where the augmented signal  $\mathbf{V}_a = [U_a, W_a, Q_a]^T$  will be chosen as in (4 9), represents the column vector  $[S_U, S_W, S_Q]^T$ .

With the  $\mathbf{B}_2$  matrix as defined in (4 29), the  $\mathbf{S}_x$  dynamics in (4 12) may be evaluated to get

$$\begin{aligned} S_x &= -K_x S_x + S_U \cos(\theta) + S_W \sin(\theta) + d_{2x}, \\ S_z &= -K_z S_z + S_U \sin(\theta) - S_W \cos(\theta) + d_{2z}, \text{ and} \\ S_\theta &= -K_\theta S_\theta + S_Q + d_{2\theta}, \end{aligned} \quad (4 31)$$

and the augmented signal  $\mathbf{V}_a$  in this case can be derived from (4 9) as

$$\begin{pmatrix} U_a \\ W_a \\ Q_a \end{pmatrix} = \begin{pmatrix} U_d \cos(S_\theta) - W_d \sin(S_\theta) - K_x S_x \cos(\theta) - K_z S_z \sin(\theta) \\ U_d \sin(S_\theta) + W_d \cos(S_\theta) - K_x S_x \sin(\theta) + K_z S_z \cos(\theta) \\ Q_d - K_\theta S_\theta \end{pmatrix} \quad (4 32)$$

Its derivative  $\mathbf{V}_a$  in (4 19) may be evaluated as shown below. As  $\mathbf{B}_2$  in (4 29) for this problem is a function of  $\theta$  only, it is seen that for a column vector  $\mathbf{C} = [C_x, C_z, C_\theta]^T$ ,



$J_{B_2}[I \otimes C]$  as required in (4 21) and (4 22) may be evaluated as

$$J_{B_2}[I \otimes C] = C_\theta M_{1\theta} = C_\theta \begin{bmatrix} -\sin(\theta) & \cos(\theta) & 0 \\ \cos(\theta) & \sin(\theta) & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad (4 33)$$

Moreover, the following result may be easily established by matrix multiplication for the system under study

$$-B_2^{-1}M_{1\theta}B_2^{-1} = M_{1\theta} \quad (4 34)$$

Combining (4 33) and (4 34), it is seen that

$$-B_2^{-1}J_{B_2}[I_n \otimes C]B_2^{-1} = C_\theta M_{1\theta} \quad (4 35)$$

From (4 15) and (4 16), it is seen that  $\frac{d}{dt}[B_2^{-1}] = -B_2^{-1}J_{B_2}[I_n \otimes X]B_2^{-1}$  Here  $C = X$ . Thus, using  $C_\theta = \theta = Q + d_{2\theta}$  from (4 28), the above equation gives  $\frac{d}{dt}[B_2^{-1}]$  as

$$\frac{d}{dt}[B_2^{-1}] = -B_2^{-1}J_{B_2}[I_n \otimes X]B_2^{-1} = (Q + d_{2\theta})M_{1\theta} \quad (4 36)$$

The quantity  $T_a$  in (4 21) and  $d'_2$  in (4 22) may be simplified using the equality in (4 35) to get

$$\begin{aligned} T_a &= B_2^{-1} \left( \frac{d}{dt}[B_{2d}V_d] - K_x T_x \right) + Q M_{1\theta} (B_{2d}V_d - K_x S_x), \text{ and} \\ d'_2 &= -B_2^{-1}K_x d_2 + d_{2\theta} M_{1\theta} (B_{2d}V_d - K_x S_x) \end{aligned} \quad (4 37)$$

The various terms in  $T_a$  may now be evaluated as follows

$$B_2^{-1} \frac{d}{dt}[B_{2d}V_d] = \begin{pmatrix} U_d \cos(S_\theta) - W_d \sin(S_\theta) + \theta_d U_d \sin(S_\theta) + \theta_d W_d \cos(S_\theta) \\ U_d \sin(S_\theta) + W_d \cos(S_\theta) - \theta_d U_d \cos(S_\theta) + \theta_d W_d \sin(S_\theta) \\ Q_d \end{pmatrix} \quad (4 38)$$

From the  $S_x$  dynamics in (4 31), and the definition of  $T_x$  (4 11), one can obtain

$$-B_2^{-1}K_x T_x = \begin{pmatrix} K_x^2 S_x \cos(\theta) + K_z^2 S_z \sin(\theta) - K_x S_U \cos^2(\theta) - K_z S_U \sin^2(\theta) \\ -K_x S_W \sin(\theta) \cos(\theta) + K_z S_W \sin(\theta) \cos(\theta) \\ K_x^2 S_x \sin(\theta) - K_z^2 S_z \cos(\theta) - K_x S_W \sin^2(\theta) - K_z S_W \cos^2(\theta) \\ -K_x S_U \sin(\theta) \cos(\theta) + K_z S_U \sin(\theta) \cos(\theta) \\ K_\theta^2 S_\theta - K_\theta S_Q \end{pmatrix} \quad (4 39)$$

The third term of  $\mathbf{T}_a$  is obtained as

$$Q M_{1\theta} (\mathbf{B}_{2d} \mathbf{V}_d - \mathbf{K}_x \mathbf{S}_x) = Q \begin{pmatrix} -U_d \sin(S_\theta) - W_d \cos(S_\theta) + K_x S_x \sin(\theta) - K_z S_z \cos(\theta) \\ U_d \cos(S_\theta) - W_d \sin(S_\theta) - K_x S_x \cos(\theta) - K_z S_z \sin(\theta) \\ 0 \end{pmatrix} \quad (4.40)$$

The complete  $\mathbf{T}_a$  in (4.21) may be obtained by summing up the contributions of the three terms given in (4.38), (4.39), and (4.40) above. The  $\mathbf{T}_a$  is seen to be a  $3 \times 1$  vector whose components will be represented as  $[T_a^U, T_a^W, T_a^Q]^T$

Similarly the two terms in  $\mathbf{d}'_2$  in (4.37) may be evaluated as

$$-\mathbf{B}_2^{-1} \mathbf{K}_x \mathbf{d}_2 = \begin{pmatrix} -K_x d_{2x} \cos(\theta) - K_z d_{2z} \sin(\theta) \\ -K_x d_{2x} \sin(\theta) + K_z d_{2z} \cos(\theta) \\ -K_\theta d_{2\theta} \end{pmatrix}, \text{ and} \quad (4.41)$$

$$d_{2\theta} M_{1\theta} (\mathbf{B}_{2d} \mathbf{V}_d - \mathbf{K}_x \mathbf{S}_x) = d_{2\theta} \begin{pmatrix} -U_d \sin(S_\theta) - W_d \cos(S_\theta) + K_x S_x \sin(\theta) - K_z S_z \cos(\theta) \\ U_d \cos(S_\theta) - W_d \sin(S_\theta) - K_x S_x \cos(\theta) - K_z S_z \sin(\theta) \\ 0 \end{pmatrix} \quad (4.42)$$

A conservative bound  $\mathbf{D}'_2$  on the disturbance term  $\mathbf{d}'_2$  can be obtained, by taking the sum of the absolute values of the two contributing terms in (4.41) and (4.42), as

$$\mathbf{D}'_2 = \begin{pmatrix} K_x D_{2x} |\cos(\theta)| + K_z D_{2z} |\sin(\theta)| \\ + D_{2\theta} [|U_d \sin(S_\theta)| + |W_d \cos(S_\theta)| + K_x |S_x| + K_z |S_z|] \\ K_x D_{2x} |\sin(\theta)| + K_z D_{2z} |\cos(\theta)| \\ + D_{2\theta} [|U_d \cos(S_\theta)| + |W_d \sin(S_\theta)| + K_x |S_x| + K_z |S_z|] \\ K_\theta D_{2\theta} \end{pmatrix} \quad (4.43)$$

The time derivative of the augmented signal  $\mathbf{V}_a$  in (4.32) may be obtained using the above developments and  $\mathbf{V}_a = \mathbf{T}_a + \mathbf{d}'_2$  from (4.20). With  $\mathbf{d}'_2$  and its bound  $\mathbf{D}'_2$  (4.43) as obtained above, the total disturbance term in  $\mathbf{S}_v$  dynamics (4.23) is seen to be bounded by  $\mathbf{D}_1 + \mathbf{D}'_2$ . The  $\Psi_i$ ,  $i = 1, 2, 3$  (3.34) would now include the terms

arising due to  $\mathbf{D}'_2$  also. However, the gains  $k_i$ ,  $i = 1, 2, 3$  will have the same functional dependence on  $\Psi_i$  as in the Section 3.5.1. Thus the control law in (3.35) is modified with the new  $\mathbf{V}_a$  signals, and gives the new control law as

$$\begin{aligned} F_{x_{\text{com}}} &= \frac{1}{\hat{R}_m} \left( T_a^U + QW + g_0 \sin(\theta) - k_1 \text{sat}\left(\frac{S_U}{\phi_U}\right) \right), \\ F_{z_{\text{com}}} &= \frac{1}{\hat{R}_m} \left( T_a^W - QU - g_0 \cos(\theta) - k_2 \text{sat}\left(\frac{S_W}{\phi_W}\right) \right), \text{ and} \\ M_{\text{com}} &= \frac{1}{\hat{c}_7} \left( T_a^Q - k_3 \text{sat}\left(\frac{S_Q}{\phi_Q}\right) \right) \end{aligned} \quad (4.44)$$

With the above control law, the associated tracking errors  $\mathbf{S}_v$  are guaranteed to stay bounded inside the boundary layers  $\Phi_v = [\phi_U, \phi_W, \phi_Q]^T$  as discussed earlier. The results obtained from the simulation using the parameters of the aircraft problem considered in Section 3.5.1 are next presented.

### 4.3.1 Simulation Results

The numerical values of the unmatched uncertainties and disturbances and their bounds are given in Appendix D. The variation in the reciprocal of aircraft mass  $R_m$  and inverse of the pitching moment of inertia  $c_7$  as considered for the simulation are as shown in Fig. 4.2. The pilot maintains the equilibrium value of the control inputs till 0.5s and then applies an elevator doublet of magnitude  $\pm 15^\circ$  and a simultaneous throttle doublet of  $\pm 25$  units with a total time period of 1.0s. The inputs are then restored to the equilibrium values at 1.5s and maintained thereafter. The  $\Delta a_e$  uncertainty as given for the case UC1 in the Appendix D is used in the simulation. For comparison purposes, responses were obtained using the control law in (3.35) which was designed under the assumption of  $\mathbf{d}_2 = 0$ , to show the effect of the presence of these disturbances. These responses are termed as  $R_0$  in the following discussion. The responses were obtained for four sets of  $K_i$ ,  $i = 1, \dots, 4$  (the corresponding responses obtained are accordingly termed  $R_i$ ) to find out the effect of variation of the individual feedback gains in the outer loop. Note that  $K_i$ 's are vectors given as  $[K_x, K_z, K_\theta]^T$ . The gain values are taken as  $K_1 = [0.1, 0.1, 10.0]^T$ ,  $K_2 = [1.0, 1.0, 1.0]^T$ ,  $K_3 = [5.0, 5.0, 5.0]^T$ , and

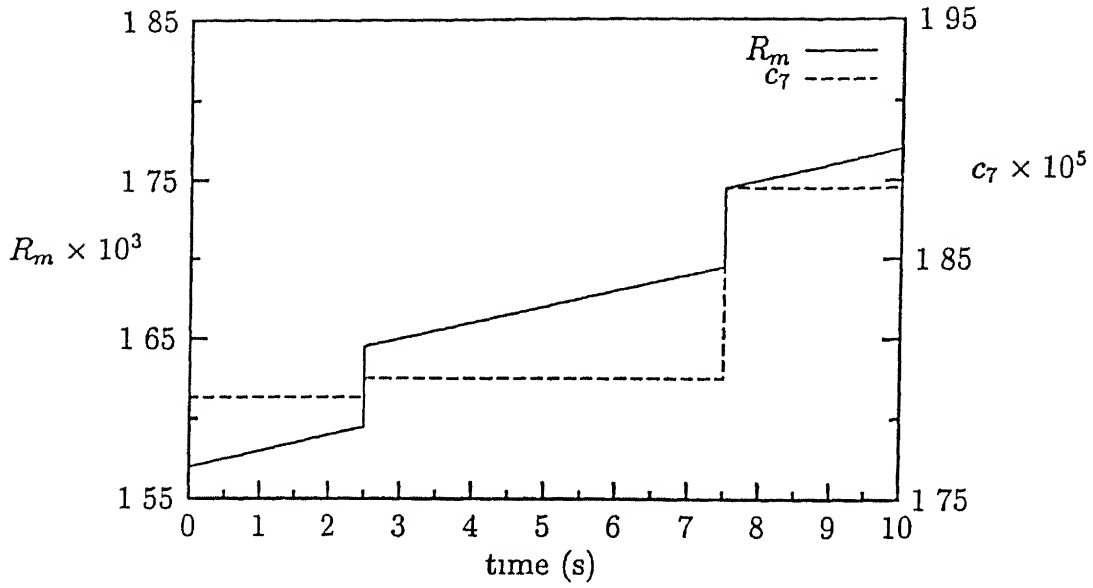


Fig. 4.2 Variation in the  $R_m$  and the  $c_7$  parameters of the aircraft

$K_4 = [1 \ 0, \ 1 \ 0, \ 10 \ 0]^T$  Also,  $\Phi_v$  is taken as  $[0 \ 5, \ 0 \ 5, \ 5 \ 0 \times 10^{-4}]^T$  and  $\eta_v = 1 \ 0$ . Numerical simulation was done using the fourth order Runge-Kutta algorithm with a time step of  $50\mu s$ .

With the boundary layers for  $S_v$  selected as  $\Phi_v$  and  $B_2$  as defined in (4.29), a conservative estimate of the bounds on  $|S_x|$  may be derived from (4.26) as

$$\begin{aligned}
 |S_x| &\leq \frac{\phi_U + \phi_W + D_{2x}}{K_x}, \\
 |S_z| &\leq \frac{\phi_U + \phi_W + D_{2z}}{K_z}, \text{ and} \\
 |S_\theta| &\leq \frac{\phi_Q + D_{2\theta}}{K_\theta}.
 \end{aligned} \tag{4.45}$$

Using numerical values, the bounds on  $S_x$ ,  $S_z$ , and  $S_\theta$  may be seen to be 20.0, 20.0, and 0.03 respectively for the gains in case  $R_1$ , 2.0, 2.0, and 0.3 in case  $R_2$ , 0.4, 0.4, and 0.06 for  $R_3$ , and 2.0, 2.0, and 0.03 for  $R_4$ . Note that  $R_0$  does not satisfy any such bounds.

From (4.45) it is clear that the  $S_x$  can be made arbitrarily small by an appropriate choice of  $K_x$ . This improvement in position tracking is obtained at the cost of a decreased velocity tracking performance in the sense that the controller is tracking  $V_a$ .

(4.32) instead of the desired  $\mathbf{V}_d$ . Therefore, it is important to look at the difference between the two signals. It follows directly from (4.27) that

$$\begin{pmatrix} U_d - U_a \\ W_d - W_a \\ Q_d - Q_a \end{pmatrix} = \begin{pmatrix} U_d[1 - \cos(S_\theta)] + W_d \sin(S_\theta) + K_x S_x \cos(\theta) + K_z S_z \sin(\theta) \\ -U_d \sin(S_\theta) + W_d[1 - \cos(S_\theta)] + K_x S_x \sin(\theta) - K_z S_z \cos(\theta) \\ K_\theta S_\theta \end{pmatrix} \quad (4.46)$$

Although the  $S_x$  can be made small as discussed earlier, the  $[K_x S_x]_i$  terms as in the above equation are seen from (4.45) to be bounded. Under the condition of small  $S_\theta$  ( $\cos(S_\theta) = 1$ , and  $\sin(S_\theta) = S_\theta$ ) for an appropriately large  $K_\theta$ , and using the bounds on the  $S_x$  from (4.45),  $\mathbf{V}_d - \mathbf{V}_a$  in the above equation can be simplified and approximate bounds on its variations are obtained as

$$\begin{pmatrix} |U_d - U_a| \\ |W_d - W_a| \\ |Q_d - Q_a| \end{pmatrix} = \begin{pmatrix} |W_d||S_\theta| + 2(\phi_U + \phi_W) + D_{2x} + D_{2z} \\ |U_d||S_\theta| + 2(\phi_U + \phi_W) + D_{2x} + D_{2z} \\ \phi_Q + D_{2\theta} \end{pmatrix} \quad (4.47)$$

For aircraft trajectories in the low angle of attack regimes  $U_d \gg W_d$ , and hence the above equation indicates that the error  $W_d - W_a$  is expected to be larger than  $U_d - U_a$ . Note that even if  $S_\theta = 0.0$ , there will be a finite error between the desired and the augmented velocity signals leading to a compromised velocity tracking. The magnitude of this error is seen from the above equation to depend on the selected boundary layer thicknesses  $\Phi_v$  and the bounds on the unmatched disturbances and uncertainties as given by  $\mathbf{D}_2$ .

The tracking error with respect to the desired response  $\mathbf{V}_d$  of the velocity outputs ( $U$ ,  $W$  and  $Q$ ) are shown in Figs. 4.3, 4.4, and 4.5 respectively for the five responses ( $R_0$  to  $R_4$ ). With the inner loop control law, the velocities were seen to be tracking the augmented signals  $\mathbf{V}_a$  within the specified boundary layers ( $\Phi_v$ ). Thus the tracking errors  $\mathbf{V} - \mathbf{V}_d$  are presented in these figures instead of the  $\mathbf{S}_v$  in (4.6), as the actual tracking errors are of direct interest. It is observed from these figures that velocity tracking in  $R_0$  has the best response in all these figures. However, as the augmented velocity signals are tracked for the various gain cases all the other cases show a com-

promised velocity tracking. As discussed earlier the errors  $W - W_d$  ( $\approx W_a - W_d$ ) in Fig. 4.4 are seen to be much larger than the  $U - U_d$  ( $\sim U_a - U_d$ ) signal in Fig. 4.3.

Figs. 4.6, 4.7, and 4.8 show the errors in  $\theta$ ,  $p_x$  and  $p_z$  from their desired values  $X_d$ . Here, as expected, it was found that  $R_0$  shows the worst response. In fact the errors in the  $\theta$ ,  $p_x$ , and  $p_z$  at  $t = 10.0$ s are seen to be about 0.4rad, 161ft, and 1048ft respectively. Responses for the other cases are a lot better, and as would be expected the best responses are obtained for the higher feedback gains. The position variable responses for the  $R_0$  case are not shown in the figures as errors in these variables are very large.

It is seen from Fig. 4.6 that increasing the gain  $K_\theta$  results in better  $\theta$  tracking and smaller  $S_\theta$  as is also evident from (4.45). As the  $K_\theta$  gain is increased from 1.0 in  $K_2$  to 5.0 in  $K_3$  and finally to 10.0 in cases  $K_1$  and  $K_4$ , better responses are obtained. Also seen from the figure is the fact that the responses  $R_1$  and  $R_4$  with the same value of  $K_\theta = 10.0$  almost overlap. An increase in  $K_\theta$  would give smaller deviations  $|\mathbf{V}_d - \mathbf{V}_a|$  for the translational velocity signals ( $U$  and  $W$ ) as would be expected from (4.47). This is also seen from the  $\mathbf{V} - \mathbf{V}_d$  plots for the two translational velocities in Figs. 4.3 and 4.4. The responses  $R_1$  and  $R_4$  in these figures are seen to be much better than the others and are almost overlapping. However, the better  $\theta$  tracking would be achieved only with an associated increase in the  $Q_a - Q_d$  error. Since  $S_Q = Q - Q_a$  is guaranteed to be smaller than  $\phi_Q = 5 \times 10^{-4}$ , this may be seen from the  $Q - Q_d$  response in Fig. 4.5 also. The figure shows larger deviations from the  $Q_d$  as the  $K_\theta$  gains are increased from  $K_2$  to  $K_3$  to the maximum value of 10.0 in the gains  $K_1$  and  $K_4$ . Here also, the  $R_1$  and  $R_4$  responses are seen to be coinciding. The  $|Q_d - Q_a|$  in (4.47) is bounded by  $\phi_Q + D_{2\theta} = 0.3005$  from the numerical values used. All the responses in Fig. 4.5 are seen to satisfy this bound.

Also as the  $K_x$  and  $K_z$  feedback gains are increased from  $K_1$  to  $K_2$  to  $K_3$ , a better position tracking of the remaining variables, i.e. the  $p_x$  and  $p_z$  is seen from the Figs. 4.7 and 4.8. It is observed in these figures also that as the corresponding  $K_x$  and  $K_z$  gains are same in the gain sets  $K_2$  and  $K_4$ , the responses  $R_2$  and  $R_4$  are seen to be

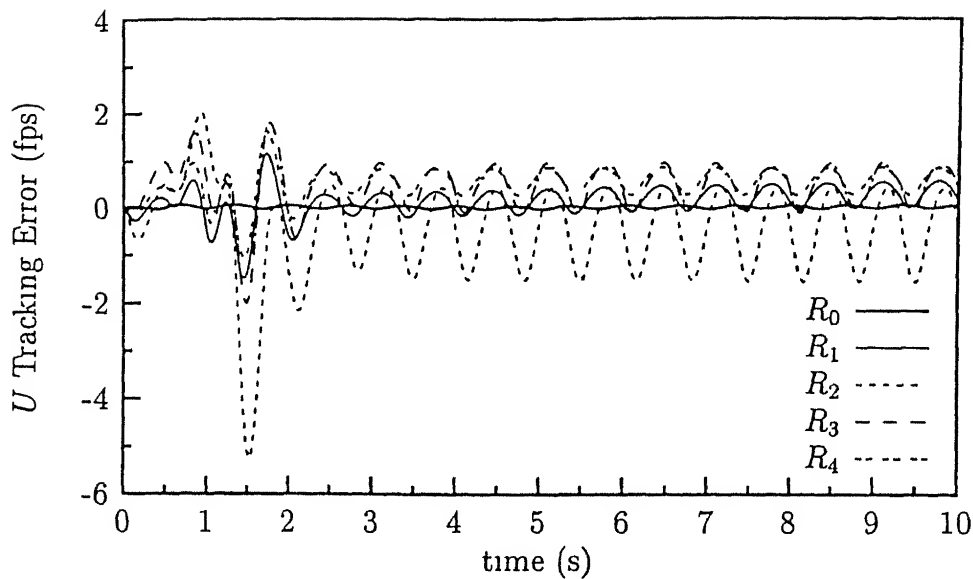


Fig. 4.3 Tracking error  $U - U_d$  (fps).

almost same, with their curves almost overlapping. Thus it is seen that, the gains have a decoupled effect on the related position tracking error, i.e. a change only in  $K_\theta$  effects almost primarily the  $S_\theta$ , similarly a change in  $K_x$  changes the  $S_x$ , and so on. In all cases an increase in the gains is seen to lead to better position tracking as was expected. However, it is observed that as the gain  $K_\theta$  is increased to a maximum in the gain sets  $K_1$  and  $K_4$  with the corresponding gains  $K_x$  and  $K_z$  remaining the same, the deviation of the actual translational velocities from their desired signals are minimized as is expected from the discussions above. Thus, a feasible choice of the gains would have a large  $K_\theta$ , with  $K_x$  and  $K_z$  selected possibly smaller to have an acceptably large  $S_x$  and  $S_z$  position errors. The high value of  $K_\theta$  would lead to a lesser deviation in the generated  $U_a$  and  $W_a$  signals from their desired values and still achieve an acceptably small  $S_\theta$  error, by marginally higher errors between the  $Q_a$  and  $Q_d$  signals, while allowing for slightly larger errors in the  $p_x$  and  $p_z$ .

In all the cases the bounds on the position errors estimated using the (4.45) are seen to be satisfied in the Figs. 4.6, 4.7 and 4.8. Thus, it is seen that with the outer loop feedback, better position tracking may be obtained at the cost of velocity

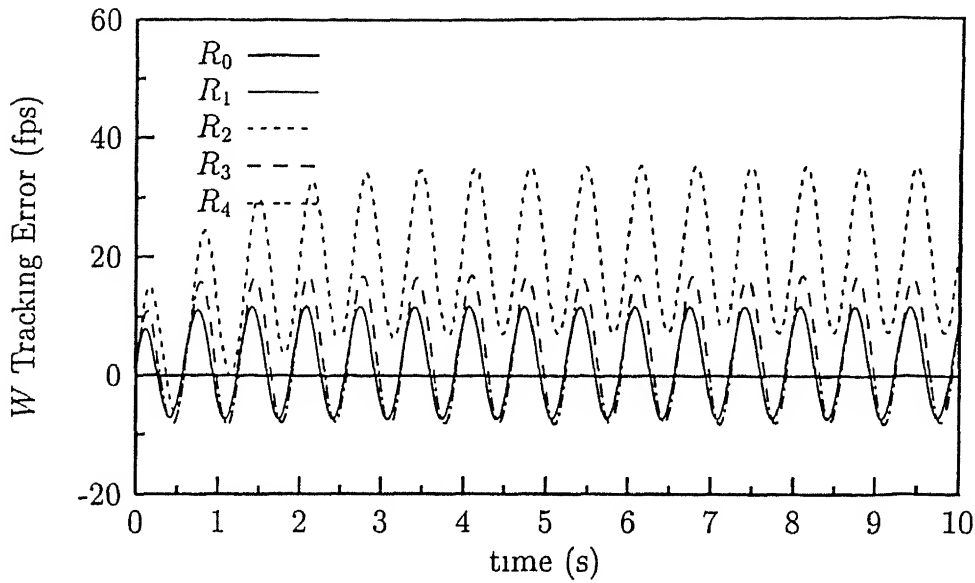


Fig. 4.4 Tracking error  $W - W_d$  (fps) Note that responses  $R_1$  and  $R_4$  overlap

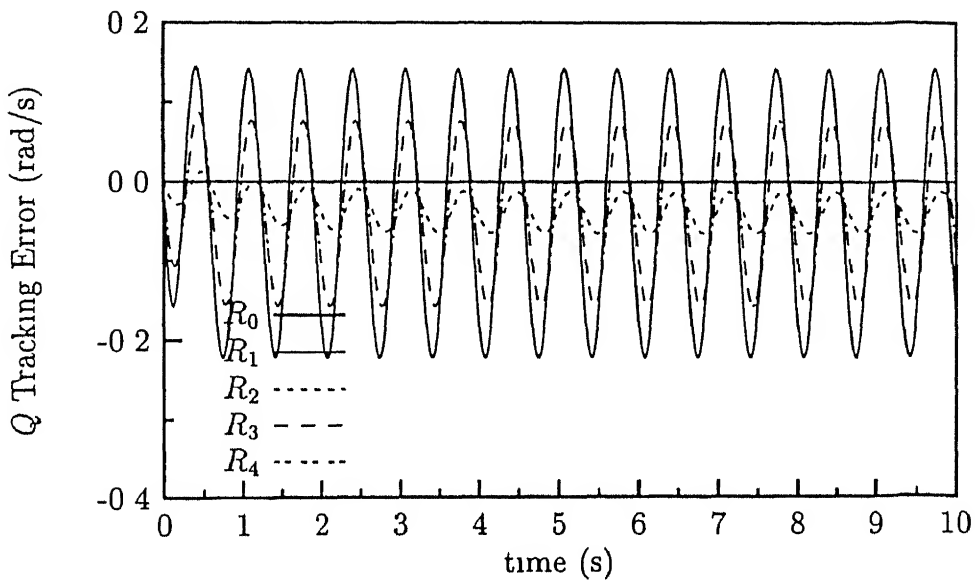


Fig. 4.5 Tracking error  $Q - Q_d$  (rad/s) Note that responses  $R_1$  and  $R_4$  are overlapping



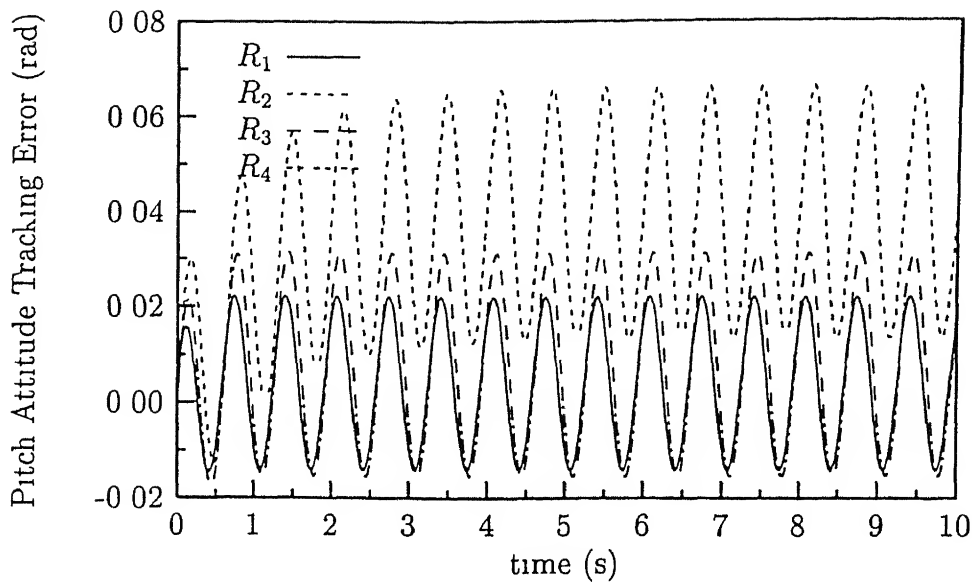


Fig. 4.6 The position tracking error  $S_\theta = \theta - \theta_d$  (rad) Responses  $R_1$  and  $R_4$  are overlapping

tracking accuracy This then sets up a tradeoff for the control law designer, and the actual gain values may be appropriately selected for the various operational regimes and requirements

The commanded forces and moments along with their actually achieved values in the  $R_4$  case are shown in Figs 4 9, 4 10, and 4 11 respectively Thus, the results of the numerical simulation show that the error bounds, as calculated using (4 45), are satisfied and validate the the SMC control laws in (4 44) For the general mechanical systems and the aircraft problem, as considered in Sections 4 2 and 4 3, with velocities as the primary outputs, the method has essentially been applied to systems with a strong relative degree of 1 The method is next extended for systems having higher relative degrees

## 4.4 ML Analysis for Higher Order SISO Systems

In this section, the ML strategy is applied to a higher order single input (SI) system with unmatched uncertainties The controller design for the unmatched uncertainty case

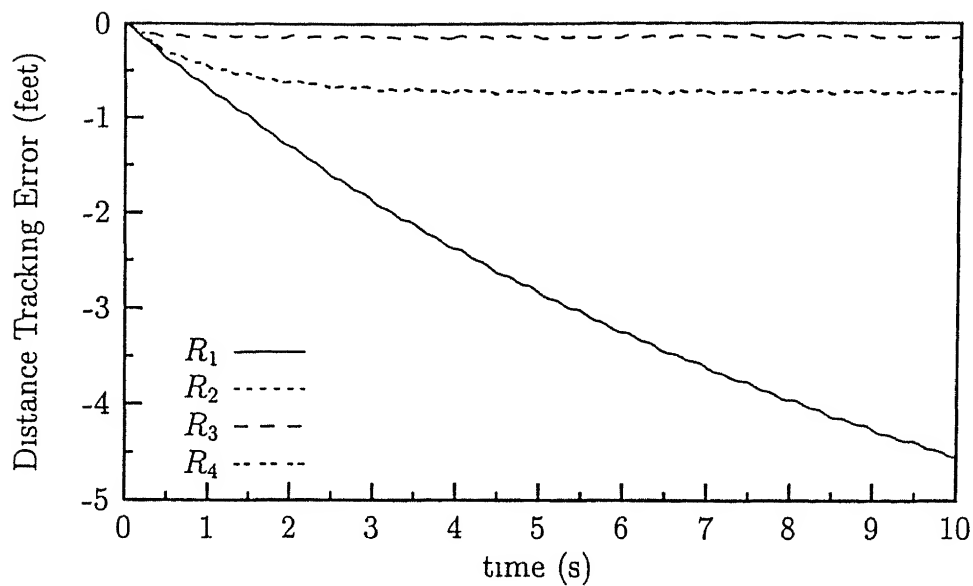


Fig. 4.7 The position tracking error  $S_x = p_x - p_{x_d}$  (ft) Responses  $R_2$  and  $R_4$  overlap

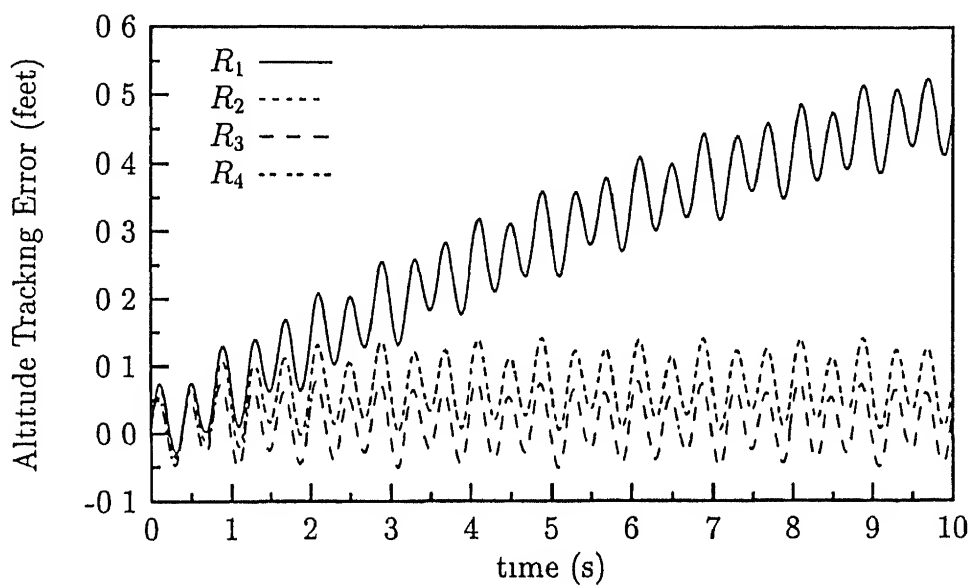


Fig. 4.8 The position tracking error  $S_z = p_z - p_{z_d}$  (ft) Note that  $R_2$  and  $R_4$  are overlapping

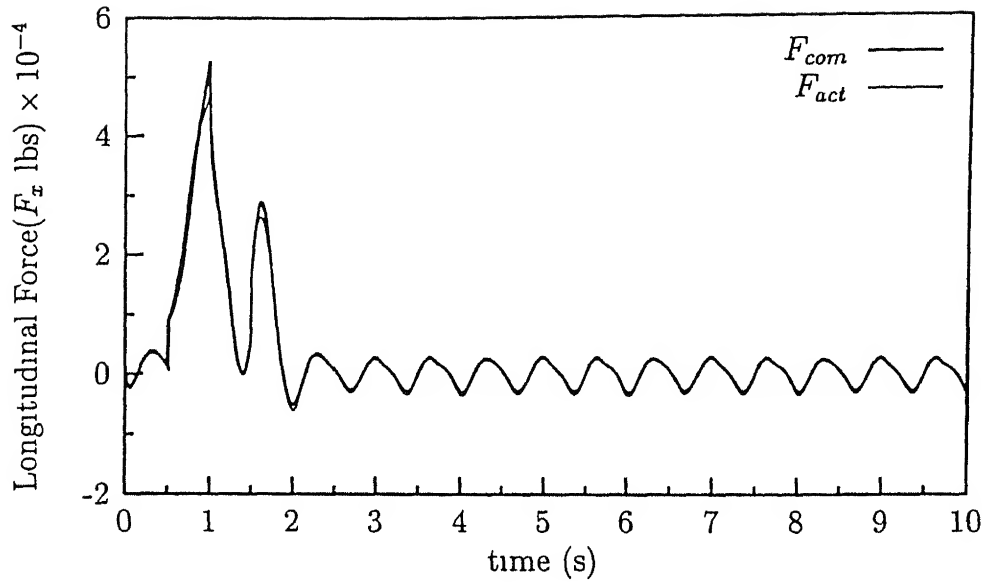


Fig 4.9 The command and achieved  $F_x$

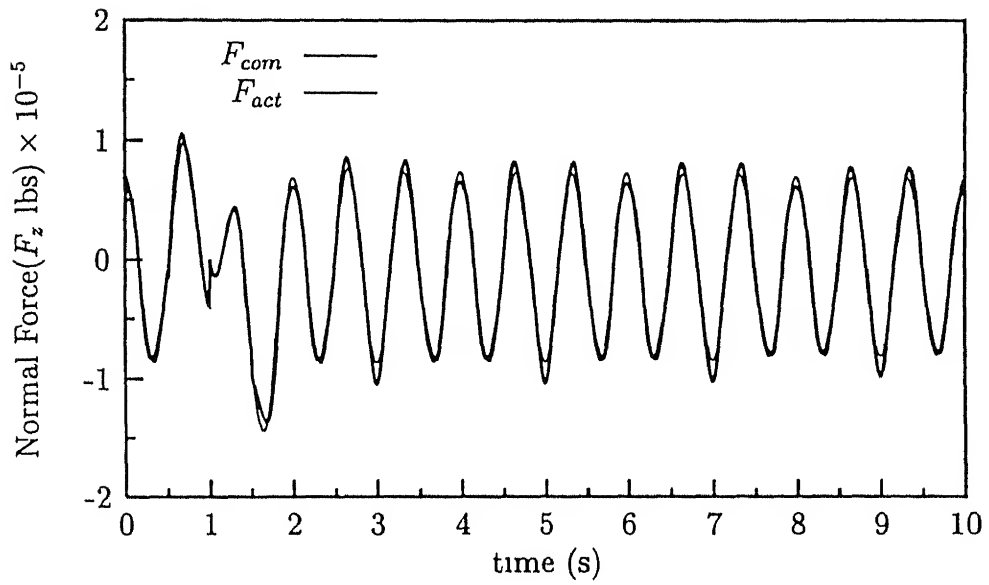


Fig. 4.10 The command and achieved  $F_z$

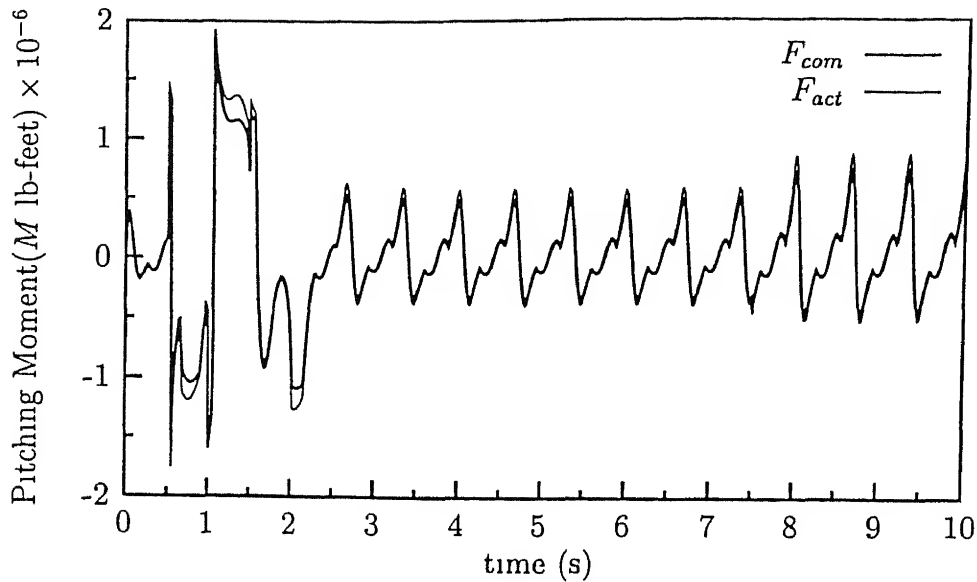


Fig. 4.11 The command and achieved  $M$

has been considered by many researchers Spurgeon [51] and Spurgeon and Davies [52] however fail to address the effect of the disturbances and uncertainties on the ZD of the system. They also require an assumption on the decomposability of uncertainty into matched and unmatched portions. Hui and Zak [70] using similar assumptions show the practical stability of the system using both state and estimator feedback. Under the above condition on the uncertainties Liao et al. [53] design continuous control laws to guarantee global stability and uniform boundedness of the tracking error. The effect of the disturbances on the ZD is considered. However, the verification of some of the assumptions on the disturbances is not trivial. Qu [71] introduced equivalently matched uncertainties which satisfy some Lyapunov related bounds and designed continuous control laws to achieve global asymptotic stabilization. Qu [72] relaxed the standard matching conditions to generalized matching conditions and a recursive procedure to design a continuous control law was proposed. Cong and Landers [73] design control laws under some conditions to be satisfied by the input distribution matrix. The effect on the ZD is not considered though. Li et al. [68], using singular perturbation methods (SPMs) design a high gain control law using stable combinations of variables, which

they call the stable combined variable perturbation method (SCVPM), under conditions to be met by the disturbance terms affecting the ZD. They relax the requirement of the decomposability assumption. Li et al. [67] generalize the results of their earlier work to give more results about the types of Lyapunov stability achievable under varying conditions. Wu and Chou [74] use a time varying singular perturbation method. In the next section, a ML framework is applied to higher order nonlinear systems and a SMC law is developed. It is shown that the method degenerates to a conventional SMC design, and bounds on the tracking errors in the various loops are obtained. The proposed method differs in the selection of the gain of the switching term.

#### 4.4.1 ML Analysis

The system under consideration is given as [68]

$$\begin{aligned} \dot{\mathbf{x}} &= \mathbf{f}(\mathbf{x}) + \mathbf{g}(\mathbf{x})u + \Delta\mathbf{f}(\mathbf{x}) + \Delta\mathbf{g}(\mathbf{x})u, \text{ and} \\ y &= h(\mathbf{x}), \end{aligned} \quad (4.48)$$

where,  $\mathbf{x} \in \mathcal{R}^n$  and  $u, y \in \mathcal{R}$ . The functions in the above equations are smooth vector fields with appropriate dimensions. The arguments of the functions are dropped for brevity. The nominal system is the system defined above with the uncertain terms  $\Delta\mathbf{f}$ , and  $\Delta\mathbf{g}u = 0$ . The relative degree of the output, or equivalently the control characteristic index is assumed to be  $\rho$ . Under a suitable coordinate transformation from  $\mathbf{x}$  to  $\mathbf{z} = [\xi^T \eta^T]^T$ , where  $\xi = [y_1, y_2, \dots, y_\rho]^T \in \mathcal{R}^\rho$ , and  $\eta \in \mathcal{R}^{n-\rho}$ , the nominal system in (4.48) may be expressed in a reduced form as

$$\begin{aligned} y_i &= y_{i+1}, \quad i = 1, 2, \dots, \rho - 1 \\ y_\rho &= a(\xi, \eta) + b(\xi, \eta)u, \text{ and} \\ \dot{\eta} &= q(\xi, \eta), \end{aligned} \quad (4.49)$$

with  $y_1$  as the scalar output. The functions  $a$ ,  $b$ ,  $q$  are as defined in standard textbooks [21].  $b$  is assumed to be invertible for all  $\mathbf{z}$ . In the presence of uncertainties in (4.48), some uncertain terms will be present in the above set of equations. Li et al. [67,

68] require the knowledge of the characteristic indices of the uncertainties in the actual system as their design procedure is based on it. For the following analysis uncertain terms are assumed present in all the equations, and the actual system is then given as

$$\begin{aligned} y_i &= y_{i+1} + d_i, \quad i = 1, 2, \dots, \rho - 1 \\ y_\rho &= a(z) + b(z)u + d_\rho + \beta(z)u, \text{ and} \\ \eta &= q(z) + q_1(z, u), \end{aligned} \quad (4.50)$$

where,  $d_i$ ,  $i = 1, \dots, \rho$  are taken to represent the disturbances as well as the functional uncertainties. This may also include the effect of  $\Delta g u$ . Their bounds are assumed to be known and are given as  $|d_i| < D_i$ . Similarly  $|\beta| < B$ .  $q$  and  $q_1$  are assumed to satisfy conditions as specified in [67, 68]. Specifically, it is assumed that the system is minimum phase,  $q$  is Lipschitz in  $\xi$  and the effect of the disturbances on the ZD ( $q_1$ ) is bounded. Note that Li et al. [67, 68] assume that  $d_i = 0$ ,  $i = 1, \dots, \sigma$ , where  $\sigma > 1$  represents the characteristic index of the uncertainty  $\Delta f$ . Their control design procedure depends on the value of  $\sigma$ . In the method proposed here, this assumption is not required. Since all other assumptions on the ZD are taken as in [67, 68], the corresponding results hold true here also. Therefore in the following analysis, the ZD has not been considered. Thus only the first  $\rho$  equations of the system dynamics (4.50) are used.

The desired tracking signal is assumed to be given as  $\xi_d = [y_{1d}, y_{2d}, \dots, y_{\rho d}]^T$ . Following the ML structure as shown in Fig. 4.1, augmented signals  $y_{ia}$  and its time derivative  $y_{ia}$ ,  $i = 1, \dots, \rho$  will be defined as was done in the Section 4.2. Conventionally the errors are defined as

$$\bar{e}_i = y_i - y_{id}, \quad i = 1, \dots, \rho \quad (4.51)$$

New tracking errors with respect to the augmented signals are defined as

$$e_i = y_i - y_{ia}, \quad i = 1, \dots, \rho \quad (4.52)$$

The analysis for the case of  $\rho = 3$  is presented here. It can however be similarly

extended for  $\rho > 3$ . From (4 50), the  $\xi$  dynamics in this case becomes

$$y_1 = y_2 + d_1, \quad (4 53)$$

$$y_2 = y_3 + d_2, \text{ and} \quad (4 54)$$

$$y_3 = a(z) + b(z)u + d_3 + \beta(z)u \quad (4 55)$$

Define  $y_{1a} = y_{1d}$  and  $y_{1a} = y_{1d} = y_{2d}$

Consider the dynamics in (4 53). The error is  $e_1 = y_1 - y_{1a}$ . Note that  $e_1 = \bar{e}_1$ . Taking its time derivative  $\dot{e}_1 = \dot{y}_2 + \dot{d}_1 - \dot{y}_{2d}$ . Using  $y_2 = y_{2a} + e_2$  from (4 52) it becomes

$$\dot{e}_1 = \dot{y}_{2a} + \dot{e}_2 + \dot{d}_1 - \dot{y}_{2d} \quad (4 56)$$

The command signal  $y_{2a}$  for the inner loop is selected, following the method of selection of  $V_a$  (4 9) as in Section 4 2, to cancel out the known terms and introducing a stabilizing feedback term as

$$y_{2a} = y_{2d} - K_1 e_1, \quad (4 57)$$

where  $K_1$  is a positive real number. With  $y_{2a}$  as chosen above,  $e_1$  in (4 56) becomes

$$\dot{e}_1 = -K_1 e_1 + \dot{e}_2 + \dot{d}_1 \quad (4 58)$$

The time derivative of  $y_{2a}$  may be derived using the above equation as

$$\begin{aligned} y_{2a} &= y_{3d} - K_1 e_1, \text{ or} \\ &= y_{3d} + K_1^2 e_1 - K_1 e_2 - K_1 d_1 \end{aligned} \quad (4 59)$$

The above equation may be rewritten as

$$y_{2a} = y_2' + d_{2c} \quad (4 60)$$

where,  $d_{2c} = -K_1 d_1$  represents the disturbance terms and  $y_2'$  includes all the remaining terms in (4 59). The inner loop will be designed so that  $y_{2a}$  and its time derivative are tracked

Next consider the dynamics in (4.54). The error  $e_2$  is defined as  $e_2 = y_2 - y_{2a}$ . Using  $y_3 = y_{3a} + e_3$  from (4.52), the time derivative of  $e_2$  is obtained using (4.54) and (4.60) as

$$\begin{aligned} e_2 &= y_{3a} + e_3 + d_2 - y_{2a} \\ &= y_{3a} + e_3 + d_2 - y_2' - d_{2c} \end{aligned} \quad (4.61)$$

The command signal  $y_{3a}$  for the next inner loop is selected as was done in the case of  $y_{2a}$  as

$$\begin{aligned} y_{3a} &= y_2' - K_2 e_2, \text{ or} \\ &= y_{3d} + K_1^2 e_1 - (K_1 + K_2) e_2, \end{aligned} \quad (4.62)$$

where  $K_2$  is a positive real number. With  $y_{3a}$  as chosen above,  $e_2$  in (4.61) becomes

$$e_2 = -K_2 e_2 + e_3 + d_2 + K_1 d_1 \quad (4.63)$$

The time derivative of  $y_{3a}$  may be derived using the above equation and (4.58) as

$$\begin{aligned} y_{3a} &= y_{4d} + K_1^2 e_1 - (K_1 + K_2) e_2, \text{ or} \\ y_{3a} &= y_{4d} - K_1^3 e_1 + (K_1^2 + K_1 K_2 + K_2^2) e_2 - (K_1 + K_2) e_3 \\ &\quad - (K_1 + K_2) d_2 - K_1 K_2 d_1 \end{aligned} \quad (4.64)$$

The above equation is rewritten as

$$y_{3a} = y_3' + d_{3c} \quad (4.65)$$

where,  $d_{3c}$  denotes all  $d_1, d_2$  terms and the remaining terms represented by  $y_3'$ . Using  $y_{2a}$  from (4.57) and the definition of  $\bar{e}_i$  from (4.51),  $e_2$  may be rewritten as

$$\begin{aligned} e_2 &= y_2 - y_{2d} + K_1 e_1, \text{ or} \\ &= \bar{e}_2 + K_1 \bar{e}_1 \end{aligned} \quad (4.66)$$

The  $y_{3a}$  (4.62) and its time derivative in (4.64) should be tracked by the next inner loop. For  $i = 3$ , the  $y_3$  dynamics (4.55) is considered next. Here  $e_3$  is defined as



$e_3 = y_3 - y_{3a}$ . Its time derivative  $y_3 - y_{3a}$  is obtained using (4.55) and (4.64) as

$$\begin{aligned} e_3 &= a(z) + b(z)u + d_3 + \beta(z)u - y_{3a}, \text{ or} \\ &= a + bu + d_3 + \beta u - y'_3 - d_{3c} \end{aligned} \quad (4.67)$$

From (4.64), it is seen that  $d_3 - d_{3c} = d_3 + (K_1 + K_2)d_2 + K_1K_2d_1 = d'_3$ . Let the bound on  $d'_3$  be represented as  $D'_3$ . Note that  $d'_3$  includes the effect of disturbances and uncertainties in the outer loops, i.e.  $d_1$  and  $d_2$ . Also, let  $|\beta b^{-1}| < \alpha < 1$ . This condition guarantees that  $b + \beta$  is invertible over the entire  $z$  space. Then a SMC law may be designed as in Section 2.2 as

$$u = b^{-1}[y'_3 - a - K_3e_3 - K_4\text{sgn}[e_3]], \quad (4.68)$$

where  $K_3, K_4 > 0$  can be appropriately selected. With  $u$  as selected above,  $e_3$  in (4.67) becomes

$$e_3 = -K_3e_3 - (1 + \beta b^{-1})K_4\text{sgn}[e_3] + \beta b^{-1}(y'_3 - a - K_3e_3) + d'_3 \quad (4.69)$$

Following the developments in Section 2.2,  $K_4$  is selected as

$$K_4 \geq \frac{\alpha|y'_3 - a - K_3e_3| + D'_3 + \eta_K}{1 - \alpha} \quad (4.70)$$

where  $\eta_K > 0$ . With this choice, the  $e_3$  dynamics in (4.69) can be guaranteed (using developments in Appendix A) to have a decay response better than

$$e_3 = -K_3e_3 - \eta_K\text{sgn}[e_3] \quad (4.71)$$

The choice of  $u$  in (4.68) is thus seen to give a proportional plus constant rate reaching law and the time to reach  $e_3 = 0$  starting from a non-zero initial condition  $e_3(0)$  can be evaluated as in (A.7)

Using  $y_{3a}$  from (4.62) and  $e_2$  from (4.66) and noting that  $e_1 = \bar{e}_1$ ,  $e_3$  may be simplified as

$$e_3 = \bar{e}_3 + (K_1 + K_2)\bar{e}_2 + K_1K_2\bar{e}_1 \quad (4.72)$$

This is the conventionally chosen SS with the poles at  $-K_1, -K_2$ . The newly defined tracking errors  $e_i$  are obtained as in (4.66) and (4.72). These are rewritten collectively to get

$$\begin{aligned} e_1 &= \bar{e}_1, \\ e_2 &= \bar{e}_2 + K_1 \bar{e}_1, \text{ and} \\ e_3 &= \bar{e}_3 + (K_1 + K_2) \bar{e}_2 + K_1 K_2 \bar{e}_1 \end{aligned} \quad (4.73)$$

The  $e_i$ 's are seen to be stable combinations of the conventional errors. Note that [68] also uses stable combinations of variables with SPMs. The  $e_i$  dynamics here is seen from (4.58), (4.63), and (4.69) as

$$\begin{aligned} e_1 &= -K_1 e_1 + e_2 + d_1, \\ e_2 &= -K_2 e_2 + e_3 + d_2 + K_1 d_1, \text{ and} \\ e_3 &= -K_3 e_3 - (1 + \beta b^{-1}) K_4 \text{sgn}[e_3] + \beta b^{-1} (y'_3 - a - K_3 e_3) + d'_3, \end{aligned} \quad (4.74)$$

where the  $e_3$  dynamics is shown to have a decay characteristic better than (4.71)

Using  $y'_3$  as defined in (4.64) and (4.65), and  $e_i$  as defined in (4.73), the  $y'_3 - K_3 e_3$  term in  $u$  in (4.68) may be simplified to get

$$y'_3 - K_3 e_3 = y_{4d} - K_1 K_2 K_3 \bar{e}_1 - (K_1 K_2 + K_2 K_3 + K_3 K_1) \bar{e}_2 - (K_1 + K_2 + K_3) \bar{e}_3 \quad (4.75)$$

which is seen to be the error and its derivatives feedback term in the conventional SMC design (as in Section 2.2). Thus it is observed that the ML approach applied to the unmatched uncertainty case leads to the conventional SMC law in (4.68), while incorporating the effect of the unmatched disturbances and uncertainties through the  $d'_3 = d_3 - d_{3c}$  term in (4.67) which is bounded by  $D'_3$ , which is reflected in the selection of the gain of the switching term  $K_4$  in (4.70)

Note that the analysis can be continued for  $\iota > 3$  in a similar fashion with similar results. Hence the analysis has been shown up to  $\iota = 3$ . Also the  $e_3$  dynamics is known to be better than the dynamics specified in (4.71), and hence, it is obvious that  $e_3 \rightarrow 0$  as it satisfies a sliding condition. To alleviate chattering, a  $\text{sat}[e_3/\phi]$  term is

used instead of the  $\text{sgn}[e_3]$  term, where  $\phi$  is a selected boundary layer thickness. With this  $|e_3|$  is ultimately bounded by  $\phi$ , and once  $e_3$  reaches the boundary layer, the  $e_2$  can be shown to decay and be ultimately bounded with  $|e_2| \leq \frac{\phi + D_2 + K_1 D_1}{K_2}$  (refer Appendix F). With  $e_3$  and  $e_2$  bounded as above,  $e_1$  is also seen to be ultimately bounded with  $|e_1| \leq \frac{|e_2| + D_1}{K_1}$ . Thus it is seen that

$$\begin{aligned} |e_3| &\leq \phi, \\ |e_2| &\leq \frac{\phi + D_2 + K_1 D_1}{K_2}, \text{ and} \\ |e_1| &\leq \frac{\phi + D_2 + (K_1 + K_2) D_1}{K_1 K_2} \end{aligned} \quad (4.76)$$

From the definition of the  $e_i$ ,  $i = 1, 2, 3$  in (4.73) and its dynamics in (4.74), it becomes clear that first the SS  $e_3$  is reached, then the trajectory starts moving along surfaces with lower dimensions in the  $\bar{e}$  space in a sequential manner, i.e. a representative point would first try to reach  $e_3 = 0$ , when it is sufficiently small then  $e_2$  is made small and so on.

The bounds for higher order systems  $\rho > 3$  can be similarly derived. From the above analysis, it is seen that if the conventional SMC design is performed, with  $K_4$  as selected in (4.70), then the output tracking error  $e_1 = \bar{e}_1$  will be ultimately bounded as in (4.76) for the unmatched uncertainty case. Given positive real numbers  $K_1$  and  $K_2$ , there is a unique surface  $e_3 = 0$  (4.72) which satisfies the sliding condition, however conversely, given a surface  $e_3 = 0$  with poles at  $-K_1$  and  $-K_2$ , the corresponding  $e_i$  dynamics (4.74) cannot be uniquely defined as it depends on the order of choice of  $K_1$  and  $K_2$ . The output tracking error bound however remains the same. The choice of  $K_1$  and  $K_2$  can be done so as to keep the  $|e_1|$  under some desired value. For example, in the case of  $\rho = 3$ , it is seen from (4.76) that a smaller  $|e_1|$  will be achieved when  $K_1$  and  $K_2$  are sufficiently large and  $K_1 + K_2 < K_1 K_2$ . The area above the curve in Fig. 4.12 gives the region of the  $K_1 - K_2$  space in which these conditions are satisfied. Similar results may be obtained for the higher order systems too.

Under the assumptions made on the  $\eta$  dynamics in (4.50), and the fact that the  $e_i$  errors are ultimately bounded as in (4.76), the ultimate boundedness of the states and

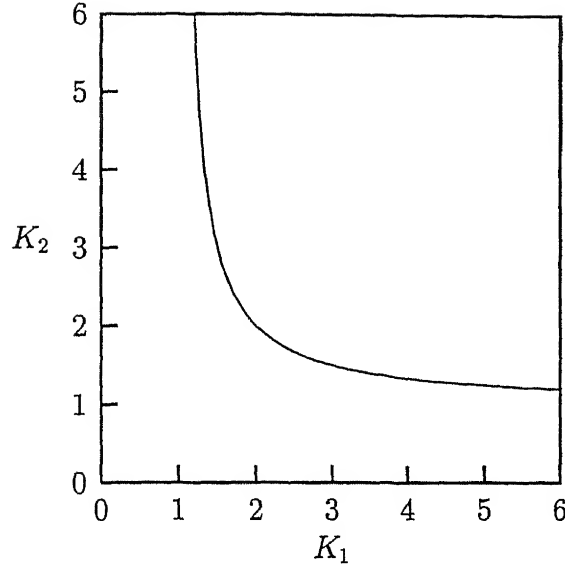


Fig 4.12 The  $K_1 - K_2$  space

thus the practical stability [70] of the complete system (4 50) may be easily established using Lyapunov method as is reported in [21, 67, 68] Thus it is concluded that, the conventional SMC design can be done for the general uncertainty case with a new method of switching gain selection as in (4 70), and the tracking error bounds can be derived as above The method developed here is applied to an example problem in the next section

#### 4.4.2 Numerical Example and Simulation

The example considered here is taken from Li et al [67] It is a four state problem with the functions in (4 48) given as

$$f(x) = \begin{pmatrix} x_3 \\ x_1^2 - x_2 + 2x_1^2x_3 \\ x_1^2 - x_3 \\ x_1 + x_4 \end{pmatrix}, \quad g(x) = \begin{pmatrix} 0 \\ 2x_3 \\ 1 \\ 0 \end{pmatrix}, \text{ and} \quad (4.77)$$

$$\Delta f(x) = \begin{pmatrix} 0.5 \exp(x_1) \\ 0.5 \exp(x_3) \\ 0.5 \exp(x_4) \\ 0 \end{pmatrix}, \quad \Delta g(x) = \begin{pmatrix} 0 \\ 0.5 \sin(x_2) \\ 0.5 \cos(x_3) \\ 0 \end{pmatrix} \quad (4.78)$$

The output  $y = x_4$ . The above set of equations may be rewritten in a reduced form in the new set of coordinates [67] given by  $\xi = [x_4, x_1 + x_4, x_1 + x_3 + x_4]^T$  and  $\eta = x_2 - x_3^2$  as in (4.50). The control characteristic index of the nominal system is seen to be  $\rho = 3$ . The resulting disturbance vector is obtained as

$$d = \begin{pmatrix} 0 \\ 0.5 \exp(x_1) \\ 0.5 \exp(x_1) + 0.5 \exp(x_4) + 0.5 \cos(x_3)u \end{pmatrix} \quad (4.79)$$

The SS was selected to have both of its poles at  $-10$ , i.e.  $e_3 = \bar{e}_3 + 20\bar{e}_2 + 100\bar{e}_1$ . Also  $\phi$ ,  $K_3$ , and  $\eta_K$  were taken as  $0.05$ ,  $5$ , and  $1.0$  respectively. The initial condition was  $x = [2.0, 2.0, 2.0, 2.0]^T$  and the desired output was taken to be  $\sin(\pi t)$ . It is easily established that  $\alpha < 1$  for this example.  $e_3(0)$  is calculated to be  $223.17$ . With the choices of  $K_3$  and  $\eta_K$  as above the reaching time may be evaluated from (A.8) as  $1.359$ s.

Simulation was done using the fourth order Runge-Kutta algorithm with a time varying step size. This was necessary as the system equations were found to be ill conditioned and application of a constant step Runge-Kutta algorithm required a prohibitively small time step. These issues and an adaptive step selection procedure are discussed in Zhao and Utkin [75]. In the present work, a simpler method involving the doubling and halving of step sizes was used. The  $e_3$  is seen to go inside the selected boundary layer in a very small time, approximately  $0.076$ s which is well smaller than the estimated reaching time, and then stays there. Note that  $d_1 = 0$  from (4.79). Since  $\xi_1 = x_4$  should track  $\sin(\pi t)$ , and  $\xi_2 = x_1 + x_4$  should track  $\pi \cos(\pi t)$ , an estimate of the bound on the magnitude of  $x_1 = \pi \cos(\pi t) - \sin(\pi t)$  was taken as  $\pi + 1$  and is used to evaluate the bound on  $d_2$  in (4.79) as  $D_2 = 31.45$  approximately. Once sliding begins, the error  $e_2$  is expected to decay and be bounded as specified in (4.76) by  $3.15$ . This

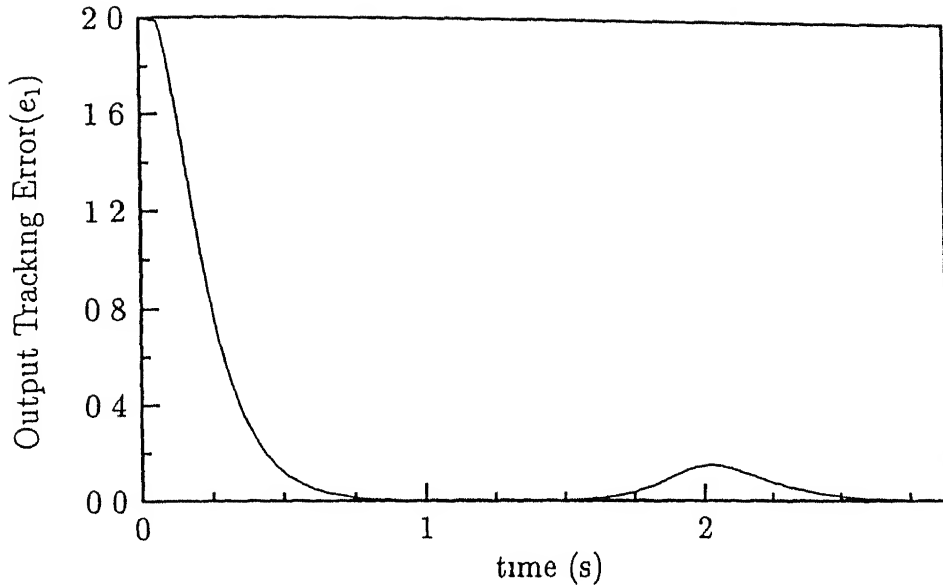


Fig. 4.13 Output tracking error  $e_1 (= \bar{e}_1)$

is achieved by  $t = 0.23283$ s, following which the  $e_1$  should decay and remain bounded by 0.315. This bound is seen to be satisfied for all  $t > 0.38127$ s. Fig. 4.13 shows the time variation of the conventional error signal  $\bar{e}_1$ . It is seen that  $e_1$  decays and stays within its bounds. The variation of  $e_2$  signal defined in (4.73) is shown in Fig. 4.14. Thus, all the error signals are seen to be varying between specified bounds.

## 4.5 Conclusions

In this chapter, robust nonlinear control law design using a ML strategy for the unmatched uncertainty case is studied. The outer loop tracking errors are used to augment the command signals for the inner loop dynamics. A SMC law is used in the inner loop to track the augmented signals. The method is directly applicable to almost all mechanical systems with velocities as the primary outputs. The ultimate boundedness of the tracking errors in the two loops is established. Control laws are derived for the aircraft longitudinal dynamics and simulation results for the velocity tracking mode are presented. The choice of parameters may be done based on a tradeoff between the errors in the inner and outer loops. The ML method is then applied to higher order

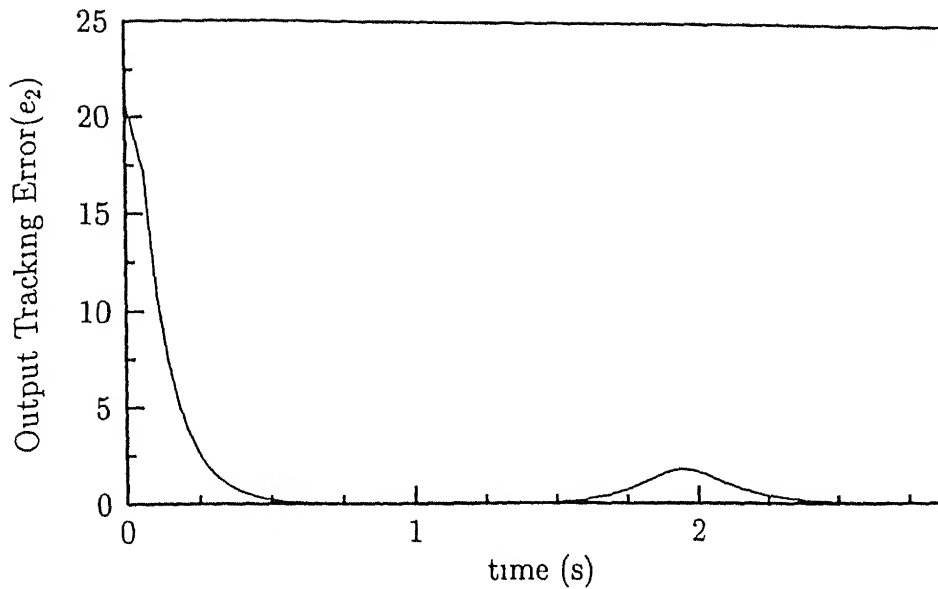


Fig. 4.14 Output tracking error  $e_2$

single input systems (with relative degree  $> 1$ ) with unmatched uncertainties. The ML analysis is seen to give control laws equivalent to the conventional SMC design, however, the selection of the switching term gain is slightly modified. Bounds on the defined tracking errors are developed. Thus, it is concluded that a conventional SMC design can be implemented for the case of unmatched uncertainty also and the bounds for the tracking errors may be obtained. Minimization of these bounds and the method proposed in Chapter 2 can guide the selection of the SMC parameters. The method is verified by applying it to an example problem taken from published literature.

# Chapter 5

## SMC for Systems with Input Dynamics

### 5.1 Introduction

As discussed earlier, the SMC uses a discontinuous/switching control law, because of the  $\text{sgn}[\cdot]$  term in (2.9), and the associated invariance to matched disturbances and uncertainties accrue because of the assumption of exact switching. The SMC method can therefore not be applied to systems where discontinuities in the input are not permissible, as in chemical systems where the inputs such as flow rates cannot be varied discontinuously. Also, any practical system will have its inherent delays and a finite bandwidth, which rules out the possibility of an infinite switching frequency in practice. Thus it is not possible to ensure that motion will be restricted to the SS (ideal sliding), however motion close to the SS (real sliding) may be guaranteed [54, 55]. This was done by using continuous approximations to the discontinuous control laws [56]. The use of a boundary layer [21] as in the earlier chapters is one such method and the motion is guaranteed to lie within a boundary layer of the SS. An adaptive method of alleviation of chattering was proposed by Chang et al [76].

Elmalı and Olgac [77] used a first order filter to smoothen out the response of the switching function ( $s$ ) and then used the *signum* of the filter output to design SMC laws. The method using a second order sliding mode results in less frequent switchings than the conventional method. Emel'yanov et al [54] and Levant [55] used higher



order sliding modes for this problem Chiacchiarini et al [60] using a similar approach obtained a continuous control action which is the output of a series of integrators Ramirez [57, 58] using a differential algebraic approach, expressed the system in a generalized controller canonical form involving the inputs, the states and their higher order derivatives, and synthesized SMC laws with applications to nonlinear chemical processes [57] Ramirez et al [59] augmented the system equations with the input dynamic equations and represented the extended system in a canonical form This method was applied to the vertical flight regulation of a nonlinear helicopter model Most of these works require higher order derivatives of the outputs or the  $x$ -dynamics (5.2), which involves derivatives of the uncertainty or disturbance terms present therein Thus, the analysis of robustness properties becomes rather involved and has been addressed in very few works [60]

In this chapter, the ML strategy as outlined in the previous chapter, is applied to this problem As seen earlier in Section 4.2, the effect of disturbances in the outer loop is easily passed on to the inner loop, and thus the propagation of disturbances and as a result the robustness studies are more easily done in this procedure, as will be shown in this chapter The method however requires higher order derivatives of the desired response signals The inputs applied to any system are generally outputs of an actuator system with a finite bandwidth This is modeled in the present work as a first order dynamic system This dynamic system is added to the original dynamic system forming an augmented state space Following the developments in Chapter 4, the tracking of position variables is done in the outer loop by generating augmented velocity command signals, which are tracked in the inner loop by synthesizing augmented input signals, which are tracked in the innermost loop The resulting control law uses the full augmented state feedback, and has a discontinuity in the first derivative of the input It thus gives a continuous response in the system state space and the discontinuity is limited to the controller state space Control law is synthesized for a general SI mechanical system and applied to the nonlinear spring mass problem, considered earlier in Section 2.4.1, and simulation results are presented Time domain

rewritten as

$$\begin{aligned} s_x &= f_2 + b_2 u + d_x - x_{3d} + \lambda e, \text{ or} \\ &= f_2 + b_2 u_a + b_2 s_u + d_x - x_{3d} + \lambda e, \end{aligned} \quad (5.5)$$

using  $u = u_a + s_u$  from (5.4). As in Section 4.2,  $u_a$  would be required for the inner loop control law design, the control signal  $u_a$  is required to be continuous. Thus, it is selected by replacing the *signum* term in (2.7) by a  $k_x s_x$  term as in (4.9) and is of the form

$$u_a = \hat{b}_2^{-1}(x_{3d} - f_2 - ae - be - k_x s_x), \quad (5.6)$$

where,  $a, b > 0$  are selected as in Section 2.3 with the poles selected as  $-\lambda, -\epsilon$ . Thus,  $a = \lambda\epsilon$  and  $b = \lambda + \epsilon$  from (2.8). Thus, the  $-ae - be - k_x s_x$  term in the above equation may be written as  $-(k_x + \epsilon)s_x - \lambda e$ . Using  $u_a$ , as chosen in the above equation,  $s_x$  in (5.5) becomes

$$s_x = \delta b_2(x_{3d} - f_2 + \lambda e) - (1 + \delta b_2)(k_x + \epsilon)s_x + b_2 s_u + d_x \quad (5.7)$$

It is seen that from the above equation that calculation of bounds for  $s_x$  requires knowledge about the  $s_u$  bounds, and that is developed next.

The inner loop control law is to be designed so that  $u$  tracks  $u_a$ , i.e.,  $s_u \rightarrow 0$ . As in the Section 4.2, the time derivative of  $u_a$  in (5.6) is required. It may be derived as

$$u_a = \frac{d}{dt}[\hat{b}_2^{-1}](x_{3d} - f_2 - ae - be - k_x s_x) + \hat{b}_2^{-1} \frac{d}{dt}[x_{3d} - f_2 - ae - be - k_x s_x] \quad (5.8)$$

From the above equation it is seen that a higher order derivative of  $x_{3d}$  would be required. The remaining terms, i.e.,  $\hat{b}_2, f_2, s_x$  and their derivatives are functions of the state vector  $\mathbf{x}$  and  $\dot{\mathbf{x}}$ . Accelerometers in mechanical systems are quite commonly used. Hence the assumption of  $\ddot{\mathbf{x}}$  being available for feedback is quite justified and will be used in the following developments. However, this is not a necessary condition. In case the acceleration signals are not available for feedback, the above derivation of  $u_a$  would have a disturbance term as was the case in Section 4.2 (4.20). This disturbance term would then be passed on to the inner loop as was done in the previous chapter. The

control law design for both the cases is outlined in the example problem considered in the next section. For the rest of this section, it is assumed that the accelerometer signals are available for feedback

Since  $x_{3d} - ae - be - k_x s_x = x_{3d} - ae - be - k_x e - k_x \lambda e = x_{3d} - (k_x \lambda + a)e - (k_x + b)e$ , its time derivative may be easily obtained as

$$\frac{d}{dt}[x_{3d} - ae - be - k_x s_x] = x_{4d} - (k_x + b)(x - x_{3d}) - (k_x \lambda + a)e \quad (5.9)$$

Using (E.3) and the notations in Appendix E, the derivative  $\frac{d}{dt}[\hat{b}_2^{-1}]$  in (5.8) may be expressed as  $-\hat{b}_2^{-2} R_{b_2} \mathbf{x}$ . Similarly  $\frac{d}{dt}[f_2]$  may be expressed as  $R_{f_2} \mathbf{x}$ . Using these time derivatives and (5.9),  $u_a$  in (5.8) may be obtained as

$$\begin{aligned} u_a &= -\hat{b}_2^{-2}(x_{3d} - f_2 - ae - be - k_x s_x)R_{b_2} \mathbf{x} \\ &\quad + \hat{b}_2^{-1}[x_{4d} - (k_x + b)(x - x_{3d}) - (k_x \lambda + a)e - R_{f_2} \mathbf{x}], \text{ or} \\ u_a &= \hat{b}_2^{-1}[x_{4d} - (k_x + b)(x - x_{3d}) - (k_x \lambda + a)e \\ &\quad - R_{f_2} \mathbf{x} - \hat{b}_2^{-1}(x_{3d} - f_2 - ae - be - k_x s_x)R_{b_2} \mathbf{x}] \end{aligned} \quad (5.10)$$

Thus with the signals  $u_a$  and  $u_a$  synthesized in the outer loop as defined in (5.6) and (5.10), the design of the inner loop control law is done so as to make  $s_u$  in (5.4) go to 0. Taking the time derivative of  $s_u$ , it follows from (5.1) that

$$s_u = f_1 + b_1 w + d_u - u_a \quad (5.11)$$

The input  $w$  is selected as was done in Section 2.2 to satisfy a constant plus proportional rate reaching law as

$$w = \hat{b}_1^{-1}(u_a - f_1 - k_u s_u - k_d \text{sgn}[s_u]) \quad (5.12)$$

where,  $k_u, k_d > 0$ . The control law thus requires that all the states  $\mathbf{x}$  and the input  $u$  be available for feedback. With  $w$  as selected above, the  $s_u$  in (5.11) becomes

$$s_u = \delta b_1(u_a - f_1 + k_u s_u) - k_u s_u - (1 + \delta b_1)k_d \text{sgn}[s_u] + d_u \quad (5.13)$$

If  $k_d$  is selected following (4.70) as

$$k_d = \frac{\beta_1 |u_a - f_1 + k_u s_u| + D_u + \eta_u}{1 - \beta_1}, \quad (5.14)$$

with  $\eta_u > 0$ , then following developments in Section 2.2,  $s_u$  can be shown to have decay characteristics better than

$$\dot{s}_u = -k_u s_u - \eta_u \text{sgn}[s_u] \quad (5.15)$$

Thus  $s_u \rightarrow 0$  in a finite time which may be derived using (A.7) and will then stay there. For implementation purposes, the  $\text{sgn}[\cdot]$  term is replaced by a  $\text{sat}[s_u/\phi_u]$  as in Section 3.4, where  $\phi_u$  is an appropriately selected boundary layer thickness. Note that this leaves  $w$  as a continuous signal with discontinuities in its first derivative only. Thus, using a continuous  $w$  makes the actually applied  $u$  continuous up to its second derivative. In this case,  $s_u$  will be ultimately bounded with

$$|s_u| \leq \phi_u \quad (5.16)$$

within a finite time which may be evaluated as in (A.8)

Then the  $b_2 s_u$  term in (5.7) will be bounded by  $|b_2| \phi_u$ . With the further assumption that  $\delta b_2(x_{3d} - f_2 + \lambda e)$  in (5.7) is bounded as  $\beta_2 |x_{3d} - f_2 + \lambda e|$ , it can be shown as in Appendix F that  $s_x$  will be ultimately bounded with

$$|s_x| \leq \frac{\beta_2 |(x_{3d} - f_2 + \lambda e)| + |b_2| \phi_u + D_x}{(1 - \beta_2)(k_x + \epsilon)} \quad (5.17)$$

Thus, the errors defined in (5.3) and (5.4) are ultimately bounded as shown above. The designed control law is applied to the nonlinear spring mass problem considered in Section 2.4.1.

### 5.2.1 A Nonlinear Spring Mass Damper System

The system equations are as given in Section 2.4.1. The  $u$  dynamics is assumed to be a first order actuator system with a bandwidth of 10 rad/s, i.e.  $\dot{u} = -10u + 10w + d_u$ .  $d_u$  is taken as  $0.15 + 0.09 \cos(3\pi t)$  bounded by  $D_u = 0.25$ . The controller parameters were taken as follows:  $\lambda = 6$ ,  $\epsilon = 2$ , and  $k_x, k_u = 10$ .  $\phi_u = 0.1$  and  $\eta_u = 1.0$  were used in the simulation. With this  $a = 12$  and  $b = 8$ . As  $\hat{b}_2 = 1$  and  $\beta_2 = 0$ ,  $u_a$  in (5.6) becomes

$$u_a = x_{3d} - f_2 - 6e - 12s_x \quad (5.18)$$

$u_a$  is next calculated from (5.10) as

$$\begin{aligned} u_a &= x_{4d} - 18e - 72e - R_{f_2}x \\ &= x_{4d} - 18(x - x_{3d}) - 72(x - x_{2d}) - R_{f_2}x \end{aligned} \quad (5.19)$$

$R_{f_2}x$  can be evaluated from the functions given in Section 2.4.1 as  $(\mu_0 - 3\mu_1x^2)x - (\nu_0 + 2\nu_1|x|\text{sgn}[x])x$ . Thus,  $u_a$  becomes

$$u_a = x_{4d} + 18x_{3d} + 72x_{2d} - (\mu_0 - 3\mu_1x^2 + 72)x + (\nu_0 + 2\nu_1|x|\text{sgn}[x] - 18)x \quad (5.20)$$

Note that if the accelerometer is not available for feedback, the  $x$  term in the above equation may instead be written using (5.2) as  $x = f_2 + \hat{b}_2u + \hat{b}_2\delta b_2u + d_x$ . In this the first two terms are exactly known and the remaining two terms being uncertain will be passed onto the inner loop as a disturbance term (as in Section 4.2). The  $u_a$  may then be expressed as

$$\begin{aligned} u_a &= [x_{4d} + 18x_{3d} + 72x_{2d} - (\mu_0 - 3\mu_1x^2 + 72)x \\ &\quad + (\nu_0 + 2\nu_1|x|\text{sgn}[x] - 18)(f_2 + \hat{b}_2u)] \\ &\quad + (\nu_0 + 2\nu_1|x|\text{sgn}[x] - 18)(\hat{b}_2\delta b_2u + d_x) \end{aligned} \quad (5.21)$$

The  $u_a$  as derived in (5.20) or (5.21) in the presence and absence of accelerometers respectively may be rewritten as  $T_u + d'_u$ , where  $T_u$  is the term in the above equations not having any uncertainties or disturbances, and the  $d'_u$  contains the effect of the disturbances and uncertainties. Thus it is seen that for the case of acceleration signals being present,  $d'_u = 0$ , and the right hand side of (5.20) gives  $T_u$ . For the other case,  $d'_u$  is seen to be the last term in (5.21). It is assumed that a bound on  $d'_u$  may be estimated as  $D'_u$ . Thus for the case where the accelerometers are absent,  $s_u$  in (5.11) becomes

$$\dot{s}_u = f_1 + b_1w + (d_u - d'_u) - T_u \quad (5.22)$$

The input  $w$  for this may be designed as in (5.12). Note that this approach requires higher switching gains, because of the presence of two disturbance terms. This is expected to give rise to more chattering effects.

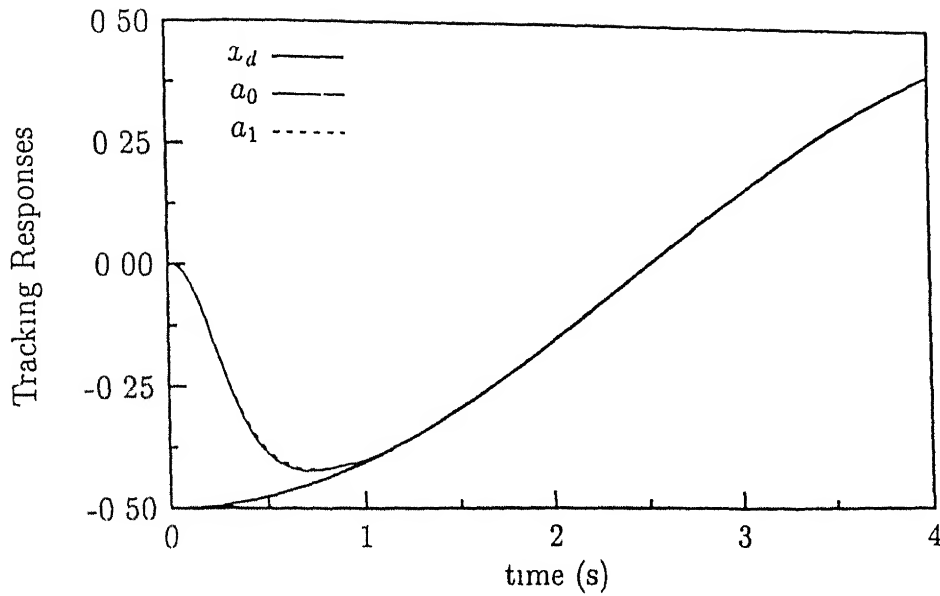


Fig. 5.1 The tracking responses for Cases  $a_0$  and  $a_1$

Simulation was done using the fourth order Runge-Kutta algorithm with a time step of 1ms. In the following figures, the responses labeled  $a_0$  are obtained in the case of accelerometers being not used. The other case is labeled  $a_1$ . Fig. 5.1 shows the tracking response obtained for the selected tracking signal. A good tracking performance is seen in both the cases. The bound on the tracking error as given in (5.17) is seen to depend on the functional like  $(x_{3d} - f_2 + \lambda \dot{e})$ , and thus numerical values of these bounds are difficult to be evaluated. The figure qualitatively shows that these are indeed bounded and quite small. Figs. 5.2 and 5.3 show the  $u$  dynamics (5.1) with the signal  $u_a$  to be tracked for cases  $a_0$  and  $a_1$  respectively. It is observed that  $u$  in both the cases starts tracking  $u_a$  within about 0.5s. In both cases the input error was seen to lie inside the specified boundary layer. It was however observed from the two figures that the input tracking in the case  $a_0$  is slightly faster than the  $a_1$  response. This may be attributed to the fact that higher switching gain in this case leads to better  $u_a$  tracking. Thus it is seen that the ML strategy can be used to design continuous SMC laws. In the next section, the method developed for SI systems is extended to MI systems.

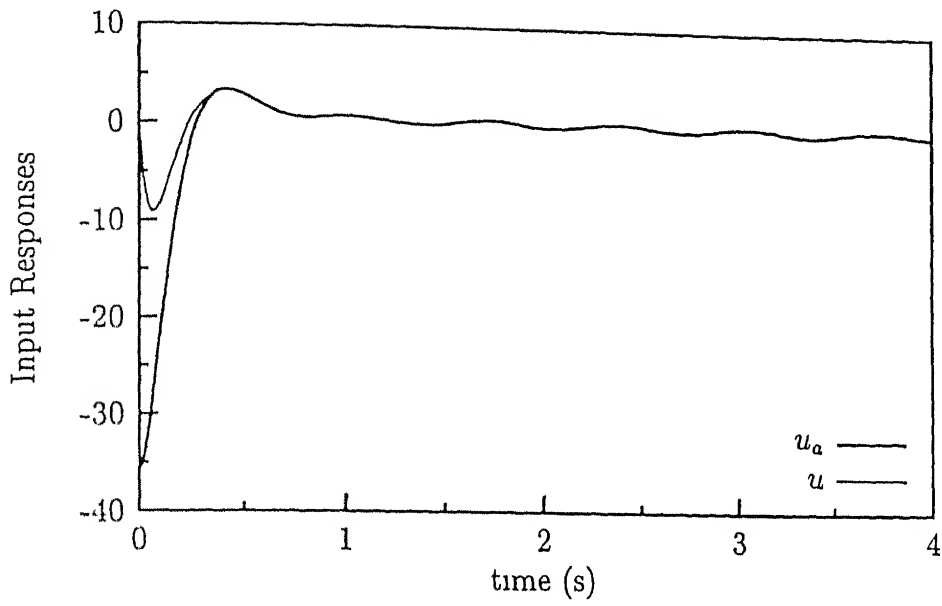


Fig. 5.2 The  $u$  dynamics for the  $a_0$  case

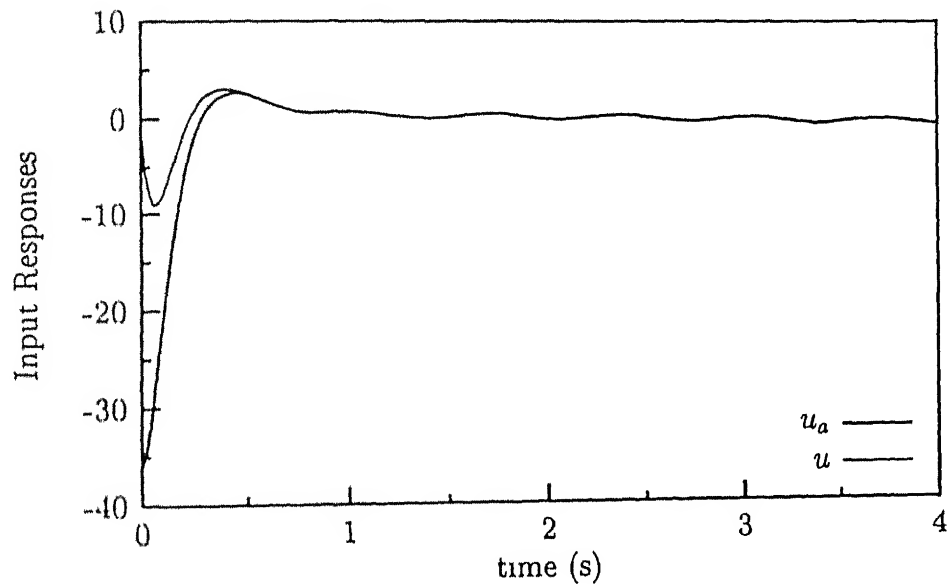


Fig. 5.3: The  $u$  dynamics for the  $a_1$  case

### 5.3 Aircraft Longitudinal Control with First Order Input Dynamics

The method applied to a SI system in the previous section is extended to a MI aircraft control problem considered in Section 4.3. In this section it is assumed that accelerometers to measure the  $\mathbf{V}$  vector are present, i.e.  $U$ ,  $W$ ,  $Q$  are available for feedback. It is also assumed that the dynamics of the force vector is decoupled. Augmenting the input dynamics equations to the MI aircraft system of equations in (4.1) and (4.3), the complete set of governing equations becomes

$$\mathbf{u} = \mathbf{g}(\mathbf{u}, \mathbf{X}, \mathbf{V}) + \mathbf{B}_0(\mathbf{u}, \mathbf{X}, \mathbf{V})\mathbf{w} + \mathbf{d}_0, \quad (5.23)$$

$$\mathbf{V} = \mathbf{f}_1(\mathbf{X}, \mathbf{V}) + \mathbf{B}_1(\mathbf{X}, \mathbf{V})\mathbf{u} + \mathbf{d}_1, \text{ and} \quad (5.24)$$

$$\mathbf{X} = \mathbf{B}_2(\mathbf{X})\mathbf{V} + \mathbf{d}_2 \quad (5.25)$$

Here  $\mathbf{w} \in \mathcal{R}^n$  represents the actuator input, and the matrices  $\mathbf{B}_i$ ,  $i = 0, 1, 2$  are assumed to be invertible over the domain of interest, and  $\mathbf{d}_0$  represents the disturbances and uncertainties in the input dynamics and is given to be bounded by  $\mathbf{D}_0$ . Let  $\mathbf{Z} = [\mathbf{V}^T \mathbf{X}^T]^T$ . The other assumptions/bounds in Section 4.2 are taken to be valid.

Proceeding as in Section 4.2, the error functions for the position, velocity and input variables are defined as  $\mathbf{S}_x$ ,  $\mathbf{S}_v$  and  $\mathbf{S}_u$  as

$$\mathbf{S}_x = \mathbf{X} - \mathbf{X}_d, \quad (5.26)$$

$$\mathbf{S}_v = \mathbf{V} - \mathbf{V}_a, \text{ and} \quad (5.27)$$

$$\mathbf{S}_u = \mathbf{u} - \mathbf{u}_a \quad (5.28)$$

where,  $\mathbf{V}_a$ ,  $\mathbf{u}_a$  are yet to be defined. The procedure is developed using the ML strategy as outlined in Section 5.2. The control law for an inner loop is therefore designed based on the error dynamics of the immediate outer loop. Thus  $\mathbf{S}_x$  dynamics is set by synthesizing  $\mathbf{V}_a$  and its time derivative  $\dot{\mathbf{V}}_a$  for tracking in the inner loop. Similarly to obtain a desirable  $\mathbf{S}_v$  dynamics,  $\mathbf{u}_a$  and  $\dot{\mathbf{u}}_a$  signals will be generated as shown in the sequel. The actuator input  $\mathbf{w}$  for the input dynamics (5.23) is designed so that  $\mathbf{u}$  tracks  $\mathbf{u}_a$  in the inner most loop.



Following the developments in Section 4.2,  $V_a$  may be derived as in (4.9). For this choice,  $S_x$  has been earlier shown to satisfy the dynamics in (4.10) as

$$S_x = -K_x S_x + B_2 S_v + d_2, \quad (5.29)$$

$V_a$  is required for tracking in the inner loop as in Section 4.2 and is derived as in (4.19). The  $S_v$  dynamics can be obtained using (5.27) and (5.24) as

$$\begin{aligned} S_v &= V - V_a, \text{ or} \\ &= f_1 + B_1 u + d_1 - V_a \end{aligned} \quad (5.30)$$

From (5.28),  $u = u_a + S_u$ , and using  $V_a = T_a + d'_2$  from (4.20), the above equation may be rewritten as

$$S_v = f_1 + B_1 u_a + B_1 S_u + d_1 - T_a - d'_2 \quad (5.31)$$

The command signal  $u_a$  should be selected so as to make the  $S_v$  errors small. Therefore, it is selected to cancel out the known terms and introduce a stabilizing feedback as in Section 3.4. Since  $u_a$  would be required for tracking in the inner loop, the discontinuous  $\text{sgn}[\ ]$  term in (3.13) is replaced by a  $K_v S_v$  term as in (4.9).  $u_a$  is thus selected as

$$u_a = \hat{B}_1^{-1}(T_a - f_1 - K_v S_v), \quad (5.32)$$

where,  $K_v = \text{diag}[K_U, K_W, K_Q]$ , all of which are positive real numbers.  $\hat{B}_1$  represents the nominal  $B_1$  matrix as defined in Section 3.4. Note that  $u_a$  represents the desired command forces which is different from the actually applied forces as discussed in Section 3.3. The effect of this uncertainty is incorporated into the design procedure (by defining the  $\Delta_t$  matrix in 3.15) as was done in Section 3.4. Using  $u_a$  as chosen in (5.32),  $S_v$  in (5.31) may be obtained as in (3.17) as

$$\dot{S}_v = -[I + \Delta_t]K_v S_v + \Delta_t(T_a - f_1) + B_1 S_u + d_1 - d'_2 \quad (5.33)$$

The  $S_v$  dynamics thus involves the  $B_1 S_u$  term, and thus the dynamics of  $S_u$  need to be considered before any bounds on the  $S_v$  errors can be developed. For this, the

time derivative of  $\mathbf{u}_a$  in (5.32) is next developed. For the tracking mode, since  $\hat{\mathbf{B}}_1$  in (3.29) is a constant matrix (Section 3.5.1),  $\mathbf{u}_a$  is seen to be

$$\begin{aligned}\mathbf{u}_a &= \hat{\mathbf{B}}_1^{-1} \frac{d}{dt} [\mathbf{T}_a - \mathbf{f}_1 - \mathbf{K}_v \mathbf{S}_v], \text{ or} \\ &= \hat{\mathbf{B}}_1^{-1} [\mathbf{T}_a - M_{f_1} \mathbf{Z} - \mathbf{K}_v \mathbf{S}_v],\end{aligned}\quad (5.34)$$

where  $\frac{d}{dt}[\mathbf{f}_1] = M_{f_1} \mathbf{Z}$ , using the notation given in (E.3) in Appendix E. Note that  $\mathbf{S}_v = \mathbf{V} - \mathbf{V}_a$  from (5.27). Thus, using  $\mathbf{V}_a$  from (4.20),  $\mathbf{S}_v = \mathbf{V} - \mathbf{T}_a - \mathbf{d}'_2$ . Putting this in the above equation,  $\mathbf{u}_a$  may be rewritten as

$$\mathbf{u}_a = \hat{\mathbf{B}}_1^{-1} [\mathbf{T}_a - M_{f_1} \mathbf{Z} - \mathbf{K}_v (\mathbf{V} - \mathbf{T}_a) + \mathbf{K}_v \mathbf{d}'_2] \quad (5.35)$$

Now it remains to evaluate  $\mathbf{T}_a$ . This may be derived starting from the definition of  $\mathbf{T}_a$  in (4.37). Its time derivative may be evaluated as

$$\begin{aligned}\mathbf{T}_a &= \frac{d}{dt} [\mathbf{B}_2^{-1}] \left( \frac{d}{dt} [\mathbf{B}_{2d} \mathbf{V}_d] - \mathbf{K}_x \mathbf{T}_x \right) + \mathbf{B}_2^{-1} \left( \frac{d^2}{dt^2} [\mathbf{B}_{2d} \mathbf{V}_d] - \mathbf{K}_x \mathbf{T}_x \right) \\ &\quad + \frac{d}{dt} [Q M_{1\theta}] (\mathbf{B}_{2d} \mathbf{V}_d - \mathbf{K}_x \mathbf{S}_x) + Q M_{1\theta} \left( \frac{d}{dt} [\mathbf{B}_{2d} \mathbf{V}_d] - \mathbf{K}_x \mathbf{S}_x \right)\end{aligned}\quad (5.36)$$

$\frac{d}{dt} [\mathbf{B}_2^{-1}]$  is already derived in (4.36). Also  $\mathbf{S}_x = \mathbf{T}_x + \mathbf{d}_2$  from (4.11). In the above equation  $\frac{d}{dt} [Q M_{1\theta}]$  may be evaluated as  $Q M_{1\theta} + Q J_{M_{1\theta}} [I_n \otimes \mathbf{X}]$ . From  $M_{1\theta}$  as defined in (4.33), it is easily obtained for the column vector  $C$  as used in (4.33), that

$$J_{M_{1\theta}} [I \otimes C] = C_\theta M_{2\theta} = C_\theta \begin{bmatrix} -\cos(\theta) & -\sin(\theta) & 0 \\ -\sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad (5.37)$$

Thus,  $J_{M_{1\theta}} [I_n \otimes \mathbf{X}]$  becomes  $(Q + d_{2\theta}) M_{2\theta}$  as  $C$  here is  $\mathbf{X}$  and  $C_\theta = \theta = Q + d_{2\theta}$  from (4.28). Thus,  $\frac{d}{dt} [Q M_{1\theta}] = Q M_{1\theta} + Q^2 M_{2\theta} + (d_{2\theta} Q) M_{2\theta}$ . Using these equalities in (5.36),  $\mathbf{T}_a$  may be obtained as

$$\begin{aligned}\mathbf{T}_a &= (2Q M_{1\theta} + d_{2\theta} M_{1\theta}) \left( \frac{d}{dt} [\mathbf{B}_{2d} \mathbf{V}_d] - \mathbf{K}_x \mathbf{T}_x \right) + \mathbf{B}_2^{-1} \left( \frac{d^2}{dt^2} [\mathbf{B}_{2d} \mathbf{V}_d] - \mathbf{K}_x \mathbf{T}_x \right) \\ &\quad + (Q M_{1\theta} + Q^2 M_{2\theta} + (d_{2\theta} Q) M_{2\theta}) (\mathbf{B}_{2d} \mathbf{V}_d - \mathbf{K}_x \mathbf{S}_x) - Q M_{1\theta} \mathbf{K}_x \mathbf{d}_2, \text{ or}\end{aligned}\quad (5.38)$$

$$\begin{aligned}
= & 2QM_{1\theta}(\frac{d}{dt}[B_{2d}V_d] - K_x T_x) + B_2^{-1}(\frac{d^2}{dt^2}[B_{2d}V_d] - K_x T_x) \\
& + (QM_{1\theta} + Q^2 M_{2\theta})(B_{2d}V_d - K_x S_x) - QM_{1\theta}K_x d_2 \\
& + d_{2\theta}M_{1\theta}(\frac{d}{dt}[B_{2d}V_d] - K_x T_x) + (d_{2\theta}Q)M_{2\theta}(B_{2d}V_d - K_x S_x)
\end{aligned} \tag{5 39}$$

Also needed in the above equation is  $-K_x T_x$ . From its definition  $T_x = -K_x S_x + B_2 S_v$  in (4 11),  $T_x = -K_x S_x + \frac{d}{dt}[B_2]S_v + B_2 S_v$ . Since  $V_a = T_a + d'_2$  from (4 20),  $S_v$  may be obtained from (5 27) as  $V - T_a - d'_2$ . Also, using (4 16) and (4 33),  $\frac{d}{dt}[B_2]$  may be written as  $(Q + d_{2\theta})M_{1\theta}$ . Using this,  $S_v$  as developed, and  $S_x$  from (4 11),  $T_x$  may be expressed as

$$\begin{aligned}
T_x = & -K_x(T_x + d_2) + (Q + d_{2\theta})M_{1\theta}S_v \\
& + B_2(V - T_a - d'_2)
\end{aligned} \tag{5 40}$$

Using the definition of  $d'_2$  from (4 20),  $B_2 d'_2 = -K_x d_2 + d_{2\theta}B_2 M_{1\theta}(B_{2d}V_d - K_x S_x)$ . Using the reverse equality from (4 34), i.e. replacing  $M_{1\theta}$  by  $-B_2^{-1}M_{1\theta}B_2^{-1}$  in this equation  $B_2 d'_2$  becomes equal to  $-K_x d_2 - d_{2\theta}M_{1\theta}B_2^{-1}(B_{2d}V_d - K_x S_x)$ , which simplifies to  $-K_x d_2 - d_{2\theta}M_{1\theta}V_a$  from the definition of  $V_a$  in (4 9). Using this in (5 40) and substituting  $V_a + S_v$  by  $V$ , as is evident from (5 27), gives

$$T_x = -K_x T_x + QM_{1\theta}S_v + B_2(V - T_a) + d_{2\theta}M_{1\theta}V \tag{5 41}$$

Using  $T_x$  as above in (5 39) gives  $T_a$  as

$$\begin{aligned}
T_a = & 2QM_{1\theta}(\frac{d}{dt}[B_{2d}V_d] - K_x T_x) + B_2^{-1}[\frac{d^2}{dt^2}[B_{2d}V_d] + K_x^2 T_x \\
& - QK_x M_{1\theta}S_v] - B_2^{-1}K_x B_2(V - T_a) + (QM_{1\theta} + Q^2 M_{2\theta})(B_{2d}V_d - K_x S_x) \\
& - QM_{1\theta}K_x d_2 + d_{2\theta}M_{1\theta}(\frac{d}{dt}[B_{2d}V_d] - K_x T_x) \\
& + (d_{2\theta}Q)M_{2\theta}(B_{2d}V_d - K_x S_x) - d_{2\theta}B_2^{-1}K_x M_{1\theta}V
\end{aligned} \tag{5 42}$$

The term  $\mathbf{B}_2^{-1} \frac{d^2}{dt^2} [\mathbf{B}_{2d} \mathbf{V}_d]$  in the above equation may be evaluated as

$$\mathbf{B}_2^{-1} \frac{d^2}{dt^2} [\mathbf{B}_{2d} \mathbf{V}_d] = \begin{pmatrix} \cos(S_\theta)[U_d + 2W_d Q_d - U_d Q_d^2 + W_d Q_d] - \sin(S_\theta)[W_d - 2U_d Q_d - W_d Q_d^2 - U_d Q_d] \\ \cos(S_\theta)[W_d - 2U_d Q_d - W_d Q_d^2 - U_d Q_d] + \sin(S_\theta)[U_d + 2W_d Q_d - U_d Q_d^2 + W_d Q_d] \\ Q_d \end{pmatrix} \quad (5.43)$$

Note that the second derivative terms  $U_d$  and so on as required in the above equation are evaluated as in (D.9) in the Appendix D. These signals are seen to include higher order derivatives of the pilot inputs  $U_p$ . Thus the so designed control law will be sensitive to the rate of application of pilot inputs. However, this must be passed through a low pass filter to avoid any pilot induced oscillations.

Thus  $\mathbf{T}_a$  may be completely evaluated using (5.43) in (5.42). Using  $\mathbf{f}_1$  as defined in (3.27), the term  $M_{f_1} \mathbf{Z}$  in  $\mathbf{u}_a$  (5.35) may be obtained as

$$\begin{aligned} M_{f_1} \mathbf{Z} &= \begin{pmatrix} -QW - QW - g_0 \cos(\theta) \\ QU + QU - g_0 \sin(\theta) \\ 0 \end{pmatrix} - d_{2\theta} \begin{pmatrix} g_0 \cos(\theta) \\ g_0 \sin(\theta) \\ 0 \end{pmatrix}, \text{ or} \\ &= \mathbf{f}_{1a} - d_{2\theta} \mathbf{f}_{1d} \end{aligned} \quad (5.44)$$

Using (5.42) and the above equation in (5.35),  $\mathbf{u}_a$  may be evaluated. For simplicity, it is rewritten as

$$\mathbf{u}_a = \mathbf{T}_u + \mathbf{d}'_u, \quad (5.45)$$

where, the first term is completely known and the  $\mathbf{d}'_u$  contains the effect of all the disturbances present. Thus, the term  $\mathbf{T}_u$  may be obtained as

$$\begin{aligned} \mathbf{T}_u &= \hat{\mathbf{B}}_1^{-1} [2QM_{1\theta} (\frac{d}{dt} [\mathbf{B}_{2d} \mathbf{V}_d] - \mathbf{K}_x \mathbf{T}_x) + \mathbf{B}_2^{-1} (\frac{d^2}{dt^2} [\mathbf{B}_{2d} \mathbf{V}_d] \\ &\quad + \mathbf{K}_x^2 \mathbf{T}_x - Q\mathbf{K}_x M_{1\theta} \mathbf{S}_v) - [\mathbf{B}_2^{-1} \mathbf{K}_x \mathbf{B}_2 + \mathbf{K}_v] (\mathbf{V} - \mathbf{T}_a) \\ &\quad + (QM_{1\theta} + Q^2 M_{2\theta}) (\mathbf{B}_{2d} \mathbf{V}_d - \mathbf{K}_x \mathbf{S}_x) - \mathbf{f}_{1a}] \end{aligned} \quad (5.46)$$

Similarly, the total disturbance component of  $\mathbf{u}_a$  is evaluated from (5.35), (5.42), and

(5.44) as

$$\begin{aligned} \mathbf{d}'_u = & \hat{\mathbf{B}}_1^{-1}[-Q M_{1\theta} \mathbf{K}_x \mathbf{d}_2 + d_{2\theta} M_{1\theta} \left( \frac{d}{dt} [\mathbf{B}_{2d} \mathbf{V}_d] - \mathbf{K}_x \mathbf{T}_x \right) \\ & + (d_{2\theta} Q) M_{2\theta} (\mathbf{B}_{2d} \mathbf{V}_d - \mathbf{K}_x \mathbf{S}_x) - d_{2\theta} \mathbf{B}_2^{-1} \mathbf{K}_x M_{1\theta} \mathbf{V} + d_{2\theta} \mathbf{f}_{1d} + \mathbf{K}_v \mathbf{d}'_2] \end{aligned} \quad (5.47)$$

A conservative bound ( $\mathbf{D}'_u$ ) on this term may be found as in Section 4.3

Now that  $\mathbf{u}_a$  (5.32) and its time derivative  $\dot{\mathbf{u}}_a$  (5.45) have been evaluated, consider the  $\mathbf{S}_u$  (5.28) dynamics. Its time derivative may be expressed as  $\dot{\mathbf{S}}_u = \dot{\mathbf{u}} - \dot{\mathbf{u}}_a$ , and using (5.23) and  $\mathbf{u}_a$  as defined in (5.45), it is rewritten as  $\dot{\mathbf{S}}_u = \mathbf{g} + \mathbf{B}_0 \mathbf{w} + \mathbf{d}_0 - \mathbf{T}_u - \mathbf{d}'_u$ . The input  $\mathbf{w}$  may be selected, following the procedure in Section 3.4 to ensure that  $\mathbf{S}_u$  satisfies a constant rate reaching law, as

$$\mathbf{w} = \mathbf{B}_0^{-1}(\mathbf{T}_u - \mathbf{g} - \mathbf{K}_\eta \text{sgn}[\mathbf{S}_u]), \quad (5.48)$$

where  $\mathbf{K}_\eta \text{sgn}[\mathbf{S}_u]$  is a  $n$  vector with its  $i^{\text{th}}$  component as  $K_{\eta_i} \text{sgn}[S_{u_i}]$  as in Section 3.4.  $K_{\eta_i}$  is selected as  $D_{0_i} + D'_{u_i} + \eta_i$ , where all  $\eta_i > 0$ . With this, the  $S_{u_i}$  response can be shown (as in Section 3.4) to be better than the response of

$$S_{u_i} = -\eta_i \text{sgn}[S_{u_i}] \quad (5.49)$$

The  $\text{sgn}[\ ]$  term in the control law (5.48) is replaced by an equivalent  $\text{sat}[S_{u_i}/\phi_{u_i}]$  term as in (3.22). Also let  $\Phi_u$  represent the vector of boundary layer thicknesses as  $[\phi_{u_i}]^T$ ,  $i = 1, \dots, n$ . Thus as in Section 3.4, the  $S_{u_i}$  is guaranteed to be inside a boundary layer of thickness  $\phi_{u_i}$ , i.e.

$$|S_{u_i}| \leq \phi_{u_i} \quad (5.50)$$

within a finite time as given in (3.25)

With  $\mathbf{S}_u$  shown to be bounded by  $\Phi_u$ , the bounds for the  $\mathbf{S}_v$  and  $\mathbf{S}_x$  errors may now be derived. Note that the  $\mathbf{S}_v$  dynamics in (5.33) involves  $\mathbf{d}'_2$  which is bounded by  $\mathbf{D}'_2$  (4.43). This bound is seen to depend on  $\mathbf{S}_x$ . Also, the  $\mathbf{S}_x$  dynamics as derived in (5.29) depends on  $\mathbf{S}_v$ . Thus, the  $\mathbf{S}_v$  and  $\mathbf{S}_x$  dynamics are seen to be inter-dependent on one other. Under the assumption that  $\mathbf{S}_x$  can be shown to be bounded, and  $(\mathbf{T}_a - \mathbf{f}_1)$  term

is bounded, and noticing that  $D_t$  is a diagonal matrix as given in (3.33), it follows from the  $S_v$  dynamics (5.33) that the  $S_v$  error satisfies

$$|S_v| \leq \frac{[|B_1|\Phi_u + D_1 + D'_2 + D_t(|T_a - f_1|)]_i}{K_{v_i}(1 - D_t(i, i))} \quad (5.51)$$

With  $|S_v|$  bounded as above, the  $S_x$  error can be shown to be bounded, as in (4.26), by

$$|S_x| \leq \frac{[|B_2|S_v + D_2]_i}{K_{x_i}} \quad (5.52)$$

The velocity and the position tracking errors  $S_v$  and  $S_x$  errors are expected to be bounded as shown above. As discussed above, the  $|S_v|$  and  $|S_x|$  are dependent on each other, resulting in simultaneous linear equations as shown in (G.5) with the bounds as variables. These bounds should be positive to be practically meaningful. It is shown in the Appendix G that this requires that  $K_v$  should be sufficiently large, or more specifically  $K_U, K_W \gg 2D_{2\theta}$ . The actual bounds may be derived by solving the linear equation set in (G.5). It may be easily shown that these errors are uniformly ultimately bounded as in Appendix F with respect to these bounds. However, the  $|S_v|$  depends on functionals like  $[|T_a - f_1|]_i$ , which cannot be easily estimated and hence the numerical values of these bounds cannot be derived, and thus detailed derivations are not presented. It suffices to know that these quantities are bounded. Thus, the ML strategy is easily applicable to a MI problem as shown here. Simulation results for the aircraft longitudinal dynamics is presented next. The qualitative nature of variation of the error bounds for different sets of gains are also studied.

### 5.3.1 Simulation Results

Simulation was done on the aircraft example considered in Section 4.3. In this example, the pilot maintains the equilibrium values of throttle gear and elevator till 0.5s, and then applies one complete cycle of the sinusoid elevator and throttle gear commands simultaneously. The elevator command is assumed to be  $\Delta U_p(1) = \delta_{el} = 20 \sin(2t - 1.0)$  while the throttle command is taken as  $\Delta U_p(2) = \delta_{tg} = 8 \sin(2t - 1.0)$ . The pilot then maintains the control inputs at the equilibrium values after  $\pi + 0.5$ s. Note that

the  $U_p$  commands are continuous, however,  $U_p$  is not. The input dynamics (5.23) for each component of the force vector was taken to be a first order system as  $\mathbf{u}_i = -20\mathbf{u}_i + 20\mathbf{w}_i + \mathbf{d}_0$ . The disturbance vector  $\mathbf{d}_0$  was taken to be

$$\begin{aligned} d_{F_x} &= 10.5 + 8.5 \cos(7\pi t), \\ d_{F_z} &= 10.5 - 8.5 \cos(6\pi t), \text{ and} \\ d_M &= 10.5 + 5.5 \cos(5\pi t), \end{aligned} \quad (5.53)$$

with the bound  $D_u = 20.0$ .  $K_4$  used for  $R_4$  in Section 4.3 was taken as  $\mathbf{K}_x = [1.0, 1.0, 10.0]^T$ .  $\eta_i$  and  $\phi_{u_i}$  were taken as 1.0 and 50.0 respectively. For comparison purposes, the response that would be obtained by neglecting the presence of the input dynamics, i.e. by using the control law in (4.44), is obtained and is labeled as  $R_0$  in the following discussions and figures. The responses for different choices of  $\mathbf{K}_v = [K_U, K_W, K_Q]^T$  are presented next.  $\mathbf{K}_{v_1}$  is chosen as  $[10.0, 10.0, 10.0]^T$ ,  $\mathbf{K}_{v_2} = [10.0, 30.0, 20.0]^T$ , and  $\mathbf{K}_{v_3} = [20.0, 30.0, 20.0]^T$ . The corresponding responses are termed  $R_1$ ,  $R_2$ , and  $R_3$  respectively. From  $\hat{\mathbf{B}}_1$  as defined in (3.29) and the nominal parameters as given in Appendix D, it is clear that  $\hat{\mathbf{B}}_1^{-1}$  will have large diagonal entries leading to a large  $\mathbf{d}'_u$ , as can be seen from (5.47), and thus the gains  $\mathbf{K}_\eta$  are expected to be quite large. Thus a smaller time step for the Runge-Kutta algorithm needs to be taken. Here it was selected as  $50\mu\text{s}$  for  $R_0$ ,  $5\mu\text{s}$  for  $R_1$ , and  $R_2$ , and  $2.5\mu\text{s}$  for the higher gain case of  $\mathbf{K}_{v_3}$ .

Figs. 5.4, 5.5, and 5.6 present the  $\mathbf{S}_v = \mathbf{V} - \mathbf{V}_a$  responses obtained for the various gain cases  $\mathbf{K}_v$  for the velocity variables  $U$ ,  $W$ , and  $Q$  respectively. Note that with the ML strategy, the velocities  $\mathbf{V}$  are supposed to track the  $\mathbf{V}_a$  signals as discussed in the previous section. For the  $R_0$  response, which is the case where no input dynamics are present, the  $\mathbf{S}_v$  errors should be bounded by the boundary layer thicknesses  $\Phi_v = [0.5, 0.5, 5.0 \times 10^{-4}]^T$  as selected in Section 4.2. That this condition is actually satisfied is easily seen from the  $R_0$  response in these figures. The  $\mathbf{S}_v$  responses for the gain cases  $\mathbf{K}_{v_i}$ ,  $i = 1, 2, 3$  in the Figs. 5.4, 5.5, and 5.6 show that, with the specified input dynamics, larger deviations are seen at the smaller gain values  $\mathbf{K}_{v_1}$ , and these are seen to decrease with higher  $\mathbf{K}_v$  gains as is seen from the  $R_2$  and  $R_3$  responses. These errors

creep into the system because of the additional input dynamics. Thus, it is observed from the figures that an increase of the  $\mathbf{K}_v$  gains leads to smaller  $\mathbf{S}_v$  as was expected from (5.51)

It is also clear from the figures that an increase in  $K_U$  leads to a smaller value of  $S_U$  only. This is seen in the  $U - U_a$  response in Fig. 5.4. The  $K_U$  gain has the same value in the gain sets  $\mathbf{K}_{v_1}$  and  $\mathbf{K}_{v_2}$  while the other  $K_W$  and  $K_Q$  gains are increased. The  $U - U_a$  response for these cases are seen to be almost same as from responses  $R_1$  and  $R_2$  as in Fig. 5.4 and are found to overlap. However, as the  $K_W$  and  $K_Q$  gains are increased from  $\mathbf{K}_{v_1}$  to  $\mathbf{K}_{v_2}$ , the corresponding  $R_2$  responses in the Figs. 5.5 and 5.6 show a marked improvement over the  $R_1$  responses, with almost no effect on the  $S_U$ . Similarly, as the  $K_U$  gain is increased from  $\mathbf{K}_{v_2}$  to  $\mathbf{K}_{v_3}$ ,  $R_3$  in Fig. 5.4 shows a distinct improvement over the  $R_1$  and  $R_2$  responses. Here, the gains  $K_W$  and  $K_Q$  are the same and the  $R_2$  and  $R_3$  responses for the associated velocity variables  $W$  and  $Q$  show almost no improvement with these responses almost overlapping as in Figs. 5.5 and 5.6. Thus the feedback gains  $\mathbf{K}_v$  have a decoupled effect on the related velocity errors. It is thus observed from the figures that as the magnitudes of the gain  $\mathbf{K}_v$  are increased, the system performance approaches the  $R_0$  performance in the limit, as would have been expected, since the  $R_0$  effectively has 'unity' as the specified input dynamics ( $\mathbf{u}_{\text{com}} = \mathbf{w}$ ), implying a infinity bandwidth dynamic system.

As discussed earlier, as the  $K_Q$  gains are increased, better  $Q_a$  tracking is expected and this would result in better  $\theta$  tracking. Similarly, for the higher  $K_U$  and  $K_W$  gains better  $U$  and  $W$  tracking of the augmented signals are observed. This implies that larger  $\mathbf{K}_v$  gains should result in better position tracking performances. The obtained position error ( $\mathbf{S}_x$  responses are shown in Figs. 5.7, 5.8, and 5.9 for the considered gain cases. A distinct improvement in the tracking performances is observed as the gains are increased due to the better velocity tracking performance and is seen to approach the  $R_0$  response. The  $\mathbf{S}_x$  errors in the high gain cases of  $R_2$  and  $R_3$  are seen to be almost overlapping in these figures. The effect of the  $\mathbf{K}_x$  gains on the  $\mathbf{S}_x$  errors has been discussed in Section 4.3.1. However, as discussed in the previous section, the  $\mathbf{S}_x$



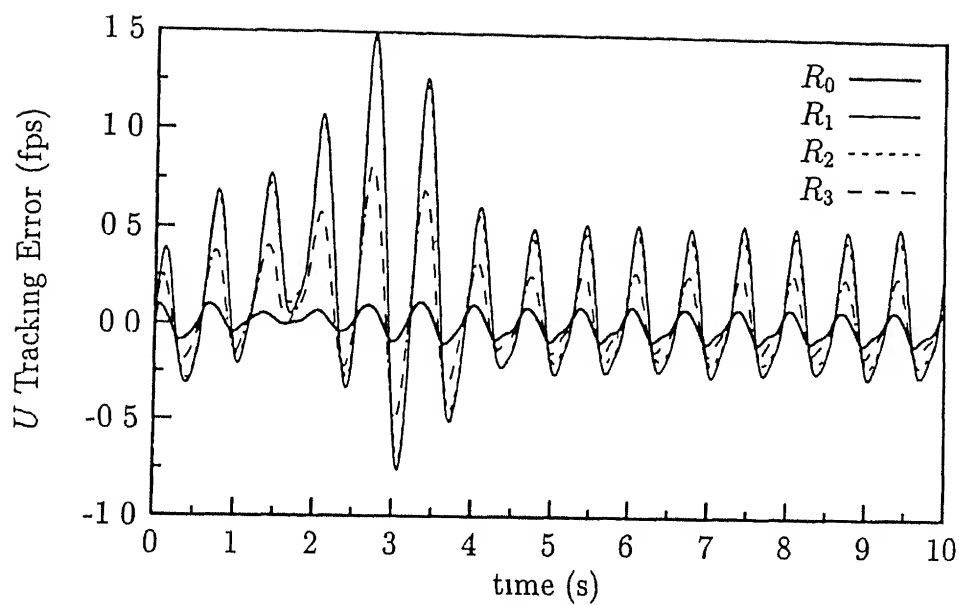


Fig. 5.4 The  $S_U = U - U_a$  response Note that responses  $R_1$  and  $R_2$  overlap

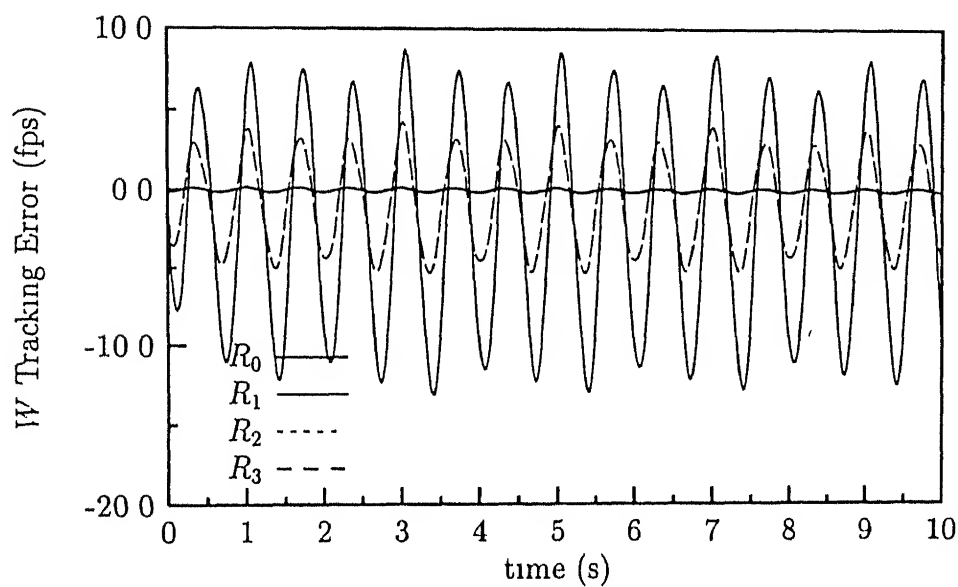


Fig. 5.5 The  $S_W = W - W_a$  response The  $R_2$  and  $R_3$  are seen to be overlapping

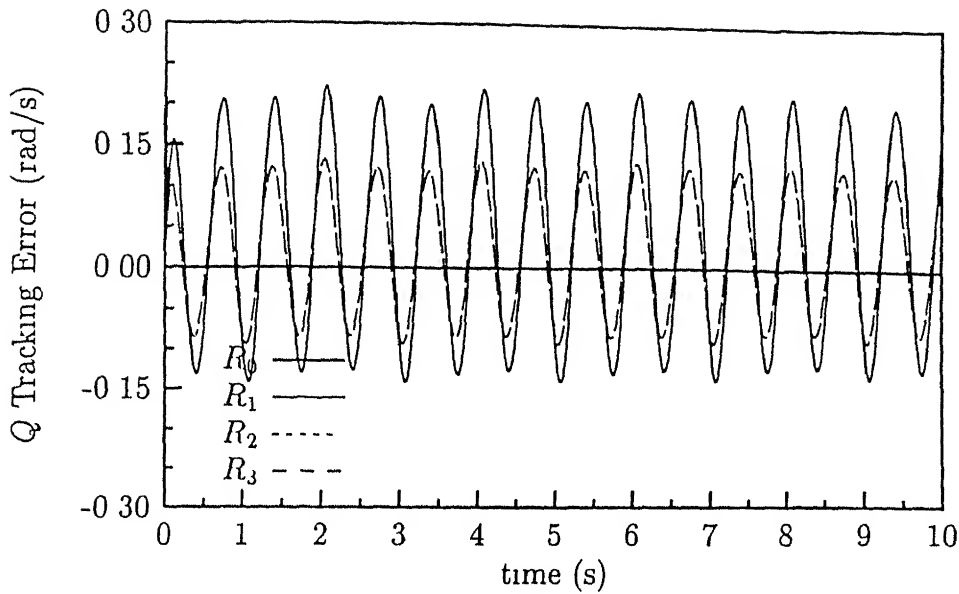


Fig. 5.6 The  $S_Q = Q - Q_a$  response The  $R_2$  and  $R_3$  are seen to be overlapping and  $S_v$  errors are inter-dependent (as shown in Appendix G) and the effect of varying the gains  $K_x$  and  $K_v$  simultaneously needs further study

The tracking error of the input dynamics ( $u - u_a$ ) is as shown in Figs 5.10, 5.11, and 5.12. It is seen from these figures that the  $S_u$  error (5.28) remains inside the selected boundary layer thicknesses ( $\phi_{u_i} = 50.0$ )

It may be concluded that as the  $K_v$  gain terms are increased the  $S_v$  error, introduced due to the input dynamics, decreases. Thus it is seen that the input dynamics can be easily incorporated in a SMC approach with an attendant increase in velocity and position tracking errors, which can however be minimized by choosing appropriate gains as shown above. The simulation results validate the control design method for the MIMO case. The various loop errors are seen to be bounded though by unknown quantities. A detailed parametric study of the involved feedback gains needs to be done for their proper selection.

This chapter so far considers the development of a SMC design method for the case of specified first order input dynamics. However, the method is not limited to this class of systems only and may be easily extended to the case of higher order input dynamics.

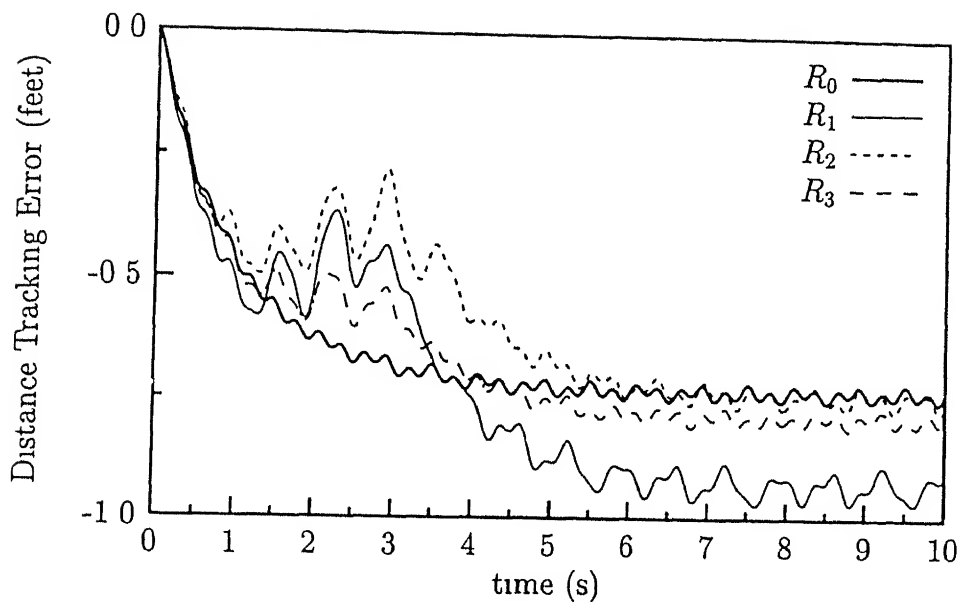


Fig. 5.7 The  $p_x - p_{x_d}$  responses

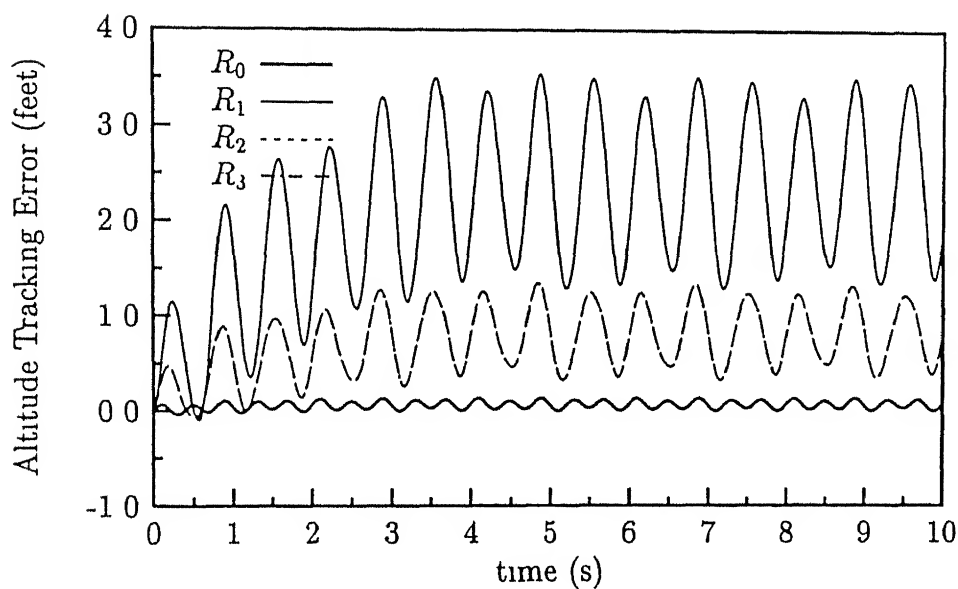


Fig. 5.8 The  $p_z - p_{z_d}$  responses. Note that the  $R_2$  and  $R_3$  responses overlap

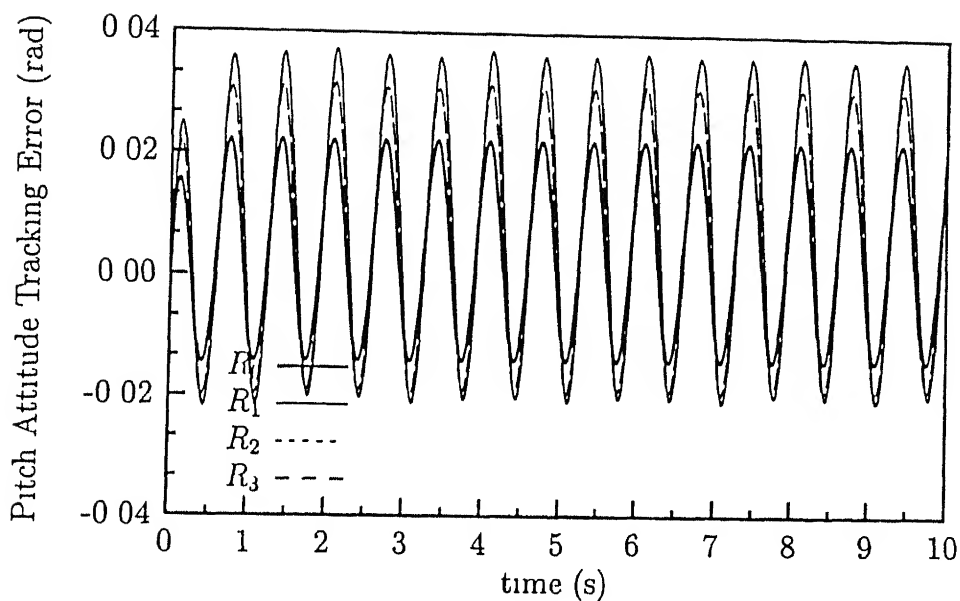


Fig. 5.9 The  $\theta - \theta_d$  responses The  $R_2$  and  $R_3$  responses almost overlap

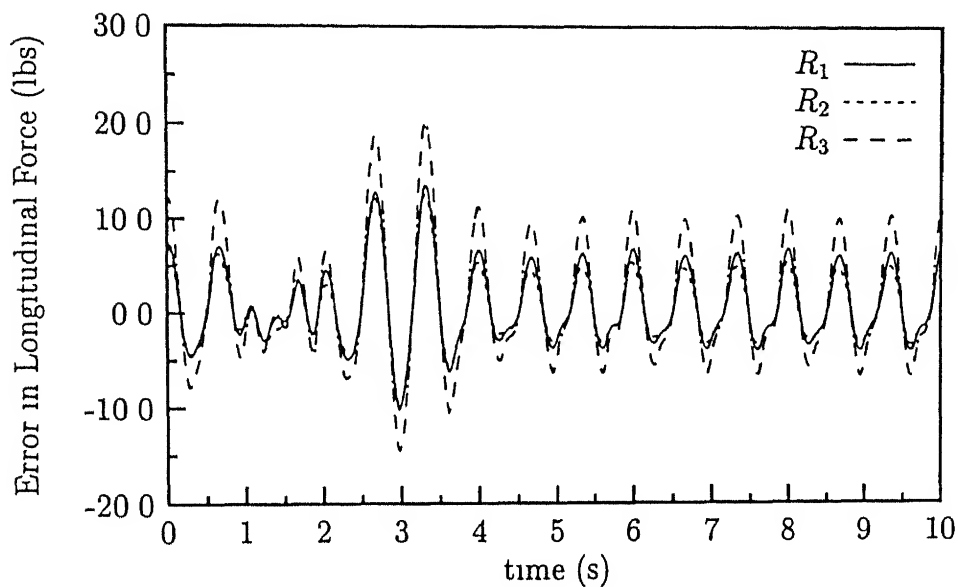


Fig. 5.10 The  $F_x - F_{x_a}$  responses

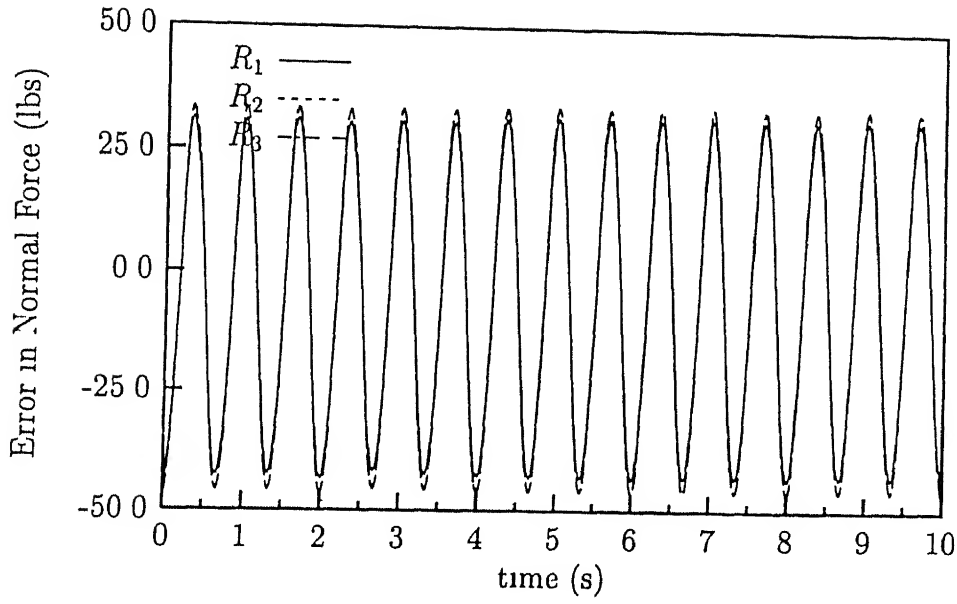


Fig. 5.11 The  $F_z - F_{z_a}$  responses

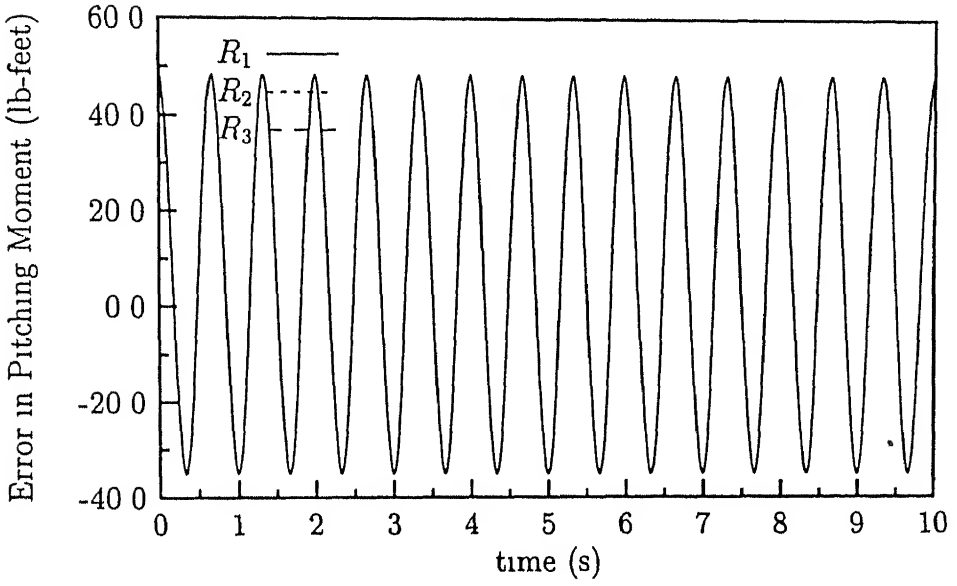


Fig. 5.12 The  $M - M_a$  responses

using the ML analysis as was done in Section 4.4.1. The derivations for  $\mathbf{u}_a$  in (5.32) and  $\mathbf{u}_a = \mathbf{T}_u + \mathbf{d}'_u$  as in (5.46) and (5.47) would still remain the same as in Section 5.3. In case of specified second order input dynamics, for e.g., another derivative of  $\mathbf{T}_u$  would be required and the  $\mathbf{d}'_u$  term would be passed on to the inner loops as was done in Sections 4.2 and 4.4.1. From its definition in (5.46),  $\mathbf{T}_u$  would require another derivative of the desired model responses. Thus the simple disturbance propagation method offered by the ML approach may be utilized to handle higher order input dynamics also.

## 5.4 Conclusions

In this chapter, a robust control law design method, using a ML strategy, for a nonlinear system with specified input dynamics under unmatched uncertainties is developed. The method does away with the requirement of higher order derivatives of the disturbances and uncertainties, leading to a simplified robustness analysis. A discontinuous SMC law or its continuous approximation is designed in the inner-most loop so that the control inputs track a desired input signal generated in the outer loops. Thus, the method results in continuous control inputs with discontinuities in its first or second derivatives only. Since, it has been developed using a model following (MF) framework, higher order derivatives of the model (desired) responses are needed. The method uses a full state feedback, including a measurement of the applied inputs. The method is first developed for a SI nonlinear spring-mass-damper system. It is shown that accelerometer signals are not necessary, although if present, they can be made use of. Simulation results for the problem establish the applicability of the method. The method is then applied to the MI aircraft problem with unmatched uncertainties as considered in Section 4.3. The bounds for the position and velocity errors are developed. Results obtained from numerical simulation for different gain sets are presented and compared. The ML strategy based SMC law synthesis method for a system with a specified input dynamics thus offers an alternate approach to the problem. Also, the involved robustness issues are much easily tackled in this framework as compared to the other methods.

## Chapter 6

# Conclusions & Scope for Further Work

The thesis is a study on some practical application aspects of the SMC design method. The nonlinear longitudinal dynamics of a generic aircraft with the force-moment vector as the input has been treated as a benchmark problem. The capability of generating a desired force-moment vector, given the airframe and engine characteristics, needs further study. The control laws are developed under the assumption that an inverse map from the force space to the actual control surface deflections exists. Although control laws have been developed for the longitudinal dynamics only, the method may easily be extended to the complete aircraft dynamics. The main results of the study are as follows

1. A new method of selection of parameters for the constant plus proportional rate reaching law based SMC based on the criterion of the time to a pre-specified level of output tracking error (OTE) is proposed. It is established the method guarantees a robust performance in the reaching phase also and gives faster tracking performances as compared to controllers based on the reaching time criterion.
2. The SMC has been used to design controllers for the aircraft dynamics which is nonlinear in the input. This is achieved by using a force control approach (FCA), treating the force-moment vector as pseudo-inputs. It is assumed that there are methods to generate any forces and moments as commanded by the

control law The error between the commanded and the generated forces is modelled as a bounded multiplicative uncertainty The conventional MIMO SMC design method is extended to include this uncertainty Analytical control laws are developed for the tracking and trimming modes for the longitudinal aircraft dynamics in the presence of matched uncertainties

- 3 The multi-loop (ML) strategy has been utilized to propose a method of designing SMC laws in the presence of unmatched disturbances and uncertainties The position and velocity tracking errors are derived and shown to be uniformly ultimately bounded Analytical control laws are synthesized for the tracking mode and verified through numerical simulation using the parameters of the F-16 aircraft
- 4 Using the better disturbance propagation property of the ML approach, a procedure for the selection of the gain of the switching term is proposed which permits extension of the conventional SMC design methods to the unmatched uncertainty case The switching surface parameters can be selected using the developed bounds on the output tracking error
- 5 The ML structure has been extended to generate SMC laws for systems with specified input dynamics in the presence of matched and unmatched uncertainties and disturbances Robustness analysis has been carried out and the ultimate boundedness of the position, velocity and input tracking errors are established Simulation results are obtained for a nonlinear spring mass system and the aircraft longitudinal dynamics and establish the efficacy of the proposed approach

Thus, the present work establishes that the ML (multi-loop) strategy can be used to advantage in designing SMC laws for mechanical and in particular aircraft systems, considering some of the practical issues involved With the FCA as proposed in this study, and an estimate of the aircraft mass and inertia parameters, the developed control laws can be used to generate force-moment specifications to be met by the aerodynamics and propulsion groups at preliminary design stages of a development



project for the aircraft to have desired the HQs. The explicit model following structure allows for easy alterations in the desired model responses at any design stage or even in flight.

The capabilities of the SMC method need to be extended for it to become a powerful alternative to the conventional FCS design methods. For this, further studies along the following directions will be beneficial.

- 1 The work relies on the existence of a map from the force space to the effector space. The capability of varying all the components of the force-moment vector independently needs further study. It will be interesting to find out the minimum number of control effectors required for this purpose and their design. This issue needs further detailed study, before the FCA (force control approach) can actually be applied to the full envelope FCS design problem.
- 2 The control laws developed in this work use a full state feedback. The case of output feedback and the design of nonlinear observers based on the SMC approach to generate estimates of the remaining states should be studied.
- 3 It is desirable to extend the present study to include bounded control input and rate saturations.
- 4 The specification of model responses based on the handling quality (HQ) requirements and its selection in the case of an existing airframe with a given limited force generation capability should be studied. The advantage of a model following approach may be utilized by specifying different linear model responses for different operating conditions, which could depend not only on the input and rate saturations but also on the need to limit some particular states of the aircraft. These model responses may then be scheduled instead of the controllers as in the gain-scheduled FCS design approach. This could also be achieved by specifying the desired response through a single nonlinear system.
- 5 The control laws synthesized in this work are analog. Most of the controller implementations, however, are now done on digital computers. Thus it is desirable

to consider SMC design for sampled data feedback systems

- 6 The results for second order systems (c f Chapter 2) would be of use for many mechanical systems, for e g , robot applications Thus, further study needs to be carried out to develop better estimates of the time to reach a specified level of output tracking error

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# Appendix A

## The $s$ response

The  $s$  dynamics is shown to be given in (2.18) as

$$s = -\epsilon s - \eta' \text{sgn}[s], \quad (\text{A } 1)$$

where,  $\eta'$  depends on disturbances and uncertainties and is thus an unknown function of the time variable  $t$ . However, it is known to be bounded and  $\eta' \geq \eta$ , where  $\eta$  is a constant, for all  $t$ . Let the response of the above system be indexed by the gain of the switching term, i.e. as  $s_{\eta'}$ . Here, the decay performance of  $s_{\eta'}$  is studied. In particular, consider the case of  $s$  decaying from an initial positive value of  $s_0$  at  $t = 0$ . The above reaching law shows that  $s = 0$  is an equilibrium point of the system and further that once  $s$  reaches zero, it will stay there for all future time instants. Starting from a positive  $s_0$ , the  $s$  will always be non-negative. The  $\text{sgn}[s]$  term is thus replaced by  $+1$  in the above equation. Thus, the  $s$  dynamics becomes

$$\begin{aligned} s &= -\epsilon s - \eta', \text{ or} \\ &= -\epsilon s - \eta + (\eta - \eta'(t)) \end{aligned} \quad (\text{A } 2)$$

The  $\eta - \eta'(t) = n(t)$  term is seen to be non-positive. The solution of the above equation may be written [69] as

$$s_{\eta'}(t) = s_0 e^{-\epsilon t} + \int_0^t e^{-\epsilon(t-\tau)} [-\eta + n(\tau)] d\tau, \text{ or}$$

$$\leq s_0 e^{-\epsilon t} + \int_0^t e^{-\epsilon(t-\tau)} [-\eta] d\tau, \quad (\text{A } 3)$$

since  $n(\cdot) \leq 0$  for all  $t$ . For negative initial values of  $s_0$ , it can be similarly shown that

$$s_{\eta'}(t) \geq s_0 e^{-\epsilon t} + \int_0^t e^{-\epsilon(t-\tau)} [\eta] d\tau, \quad (\text{A } 4)$$

The right hand side of the above inequalities (A 3) and (A 4) represents  $s_{\eta}$ , i.e. the initial condition response of

$$\dot{s} = -\epsilon s - \eta \text{sgn}[s] \quad (\text{A } 5)$$

These inequalities may be rewritten as a single inequality as

$$|s_{\eta'}(t)| \leq |s_{\eta}(t)|, \quad (\text{A } 6)$$

which implies that if  $\eta'(t) > \eta$  for all  $t$ , the decay of  $s$  exhibited by (A 1) is guaranteed to be better than the response of (A 5) as given in (A 6). Therefore, the reaching time, i.e. the time taken to arrive at  $s = 0$  starting from  $s_0$  will be bounded as

$$t_{reach} \leq \frac{1}{\epsilon} \ln \left( \frac{\epsilon |s_0| + \eta}{\eta} \right), \quad (\text{A } 7)$$

which is the reaching time for (A 5) [37]. The (A 6) also implies that increasing the magnitude of  $\eta$  leads to a faster decay of  $s$  and lower reaching times.

If, the  $\text{sgn}[s]$  term is replaced by a continuous approximation as  $\text{sat}[s/\phi]$  in (A 5), where  $\phi$  represents an appropriately selected boundary layer thickness, then the  $s$  dynamics is given by  $\dot{s} = -\epsilon s - \eta \text{sat}(s/\phi)$ . The time taken from an initial condition of  $s_0$  at  $t = 0$  to reach the boundary layer may be evaluated as

$$t_{reach} = \frac{1}{\epsilon} \ln \left( \frac{\epsilon |s_0| + \eta}{\epsilon \phi + \eta} \right) \quad (\text{A } 8)$$

# Appendix B

## Proof of Claim 1

The following proof shows how a  $\delta > 0$  may be selected, under the assumptions in the Claim 1 and starting from the premise that the (2.32) is true, i.e.,

$$Q = \delta P + H \quad (\text{B } 1)$$

The  $P$  and  $Q$  matrices in the above equation are as given in (2.25) and (2.29) respectively

**Proof:**

From the  $P$  and  $Q$  matrices as given, the elements of the symmetric matrix  $H = Q - \delta P$  from (B.1) are obtained as

$$\begin{aligned} h_{11} &= 2\alpha^2\epsilon - \delta(\alpha^2 + \beta) \\ h_{12} &= 2\alpha\epsilon - \beta - \delta\alpha \\ h_{22} &= 2\epsilon - \delta, \end{aligned} \quad (\text{B } 2)$$

where,  $h_{ij}$  represents the element  $H(i, j)$ . It is required that  $H$  be at least a positive semi-definite matrix. The positive definiteness of this matrix would require that  $h_{11}, h_{22} > 0$  and  $\det[H] > 0$ , where  $\det[\cdot]$  represents the determinant of its argument. The two former inequalities gives

$$\begin{aligned} \delta &< 2\epsilon \frac{\alpha^2}{\alpha^2 + \beta}, \text{ and} \\ \delta &< 2\epsilon \end{aligned} \quad (\text{B } 3)$$

It is seen that these inequalities are in agreement with one another. For the last condition, the  $\det[H]$  may be easily obtained from its elements as defined in (B 2) as  $h_{11}h_{22} - h_{12}^2$  and after some algebraic simplification it may be written as

$$\det[H] = \beta[\delta^2 - 2(\alpha + \epsilon)\delta + 4\alpha\epsilon - \beta] \quad (\text{B } 4)$$

The positive definiteness of  $P$  and  $Q$  imposes the condition that  $0 < \beta < 4\alpha\epsilon$  as has been discussed in Section 2.3. Since  $\beta > 0$ , the term factored out in the above equation is dropped in the further developments. The above equation thus shows that  $\det[H]/\beta$  is thus a quadratic function ( $Q_f$ ) in  $\delta$  as

$$Q_f(\delta) = \delta^2 - 2(\alpha + \epsilon)\delta + 4\alpha\epsilon - \beta, \quad (\text{B } 5)$$

and the constant term in the above equation is seen to be positive from the bounds to be satisfied by  $\beta$  as given in (2.30). The roots  $r_1, r_2$  of this quadratic equation may be easily calculated as

$$r_1, r_2 = (\alpha + \epsilon) \pm \sqrt{(\alpha - \epsilon)^2 + \beta} \quad (\text{B } 6)$$

Note that  $\sqrt{(\alpha - \epsilon)^2 + \beta}$  can always be represented as  $(\alpha - \epsilon) + \delta_1$  where  $\delta_1 > 0$  may be uniquely found. Thus, the roots in (B 6) may be simplified to get

$$r_1, r_2 = 2\alpha + \delta_1, 2\epsilon - \delta_1 \quad (\text{B } 7)$$

Note that a small positive value for  $\beta$  would imply a small  $\delta_1$ . It can be shown that even for values of  $\beta$  as large as permissible by its bounds, the  $r_2 = 2\epsilon - \delta_1 > 0$ . Since the coefficient of the second order term in  $Q_f$  in (B 5) is seen to be positive, it implies that the  $Q_f$  has a minimum, and the corresponding value of  $\delta$  ( $= \delta_m$ ) which gives the function minimum can be evaluated as

$$\delta_m = \alpha + \epsilon, \quad (\text{B } 8)$$

which being the arithmetic mean of  $r_1$  and  $r_2$  will always lie between the two roots. Combined with the fact that  $Q_f = 0$  at the roots  $\delta = r_1$  and  $r_2$  (B 7), it is seen that the  $Q_f \leq 0$  is possible only for values of  $\delta$  between the two roots and it would be

positive everywhere outside of this set. Moreover, at  $\delta = 0$  the value of  $Q_f$  is seen to be  $4\alpha\epsilon - \beta$ , which is positive as discussed earlier.

Thus it is evident that a positive  $\delta$  can always be selected from the sets given by  $(0, 2\alpha]$  or  $(0, 2\epsilon)$ , whichever is smaller. The two may be combinedly expressed by letting  $\gamma = \min[2\alpha, 2\epsilon]$ , where  $\min[ \ , \ ]$  is taken to give the minimum of its arguments. Thus, the permissible values of  $\delta$  may be specified by an open set as

$$\delta \in (0, \gamma) \tag{B 9}$$

Moreover, in the limit of  $\beta \rightarrow 0$ , a choice of  $\delta \rightarrow \gamma$  would be achieved. It is thus established that a positive  $\delta$  always exists which would result in  $H$  being a positive definite matrix, thus satisfying the Claim 1. ■

$a = pq, b = p + q$  from (2.8), the  $S_p = e + pe$  may be simplified as

$$\begin{aligned} S_p &= -ae - (b - p)e + h_i \\ &= -pqe - qe + h_i, \text{ or} \\ S_p &= -qS_p + h_i \end{aligned} \quad (\text{C } 2)$$

Similarly,  $S_q$  can be obtained as

$$S_q = -pS_q + h_i \quad (\text{C } 3)$$

Thus the time derivative of the candidate Lyapunov function as in (C.1) may be rewritten for the case 'i', using the  $y^T P \bar{q} = S_p h_i$  as defined above and  $S_p$  and  $S_q$  as in (C.2) and (C.3), as

$$\begin{aligned} V_i &= -y^T Q y + 2S_p h_i + M [(-qS_p + h_i) \text{sgn}[S_p] + (-pS_q + h_i) \text{sgn}[S_q]], \text{ or} \\ &= -y^T Q y + 2S_p h_i - M[q|S_p| + p|S_q|] + M[\text{sgn}[S_p] + \text{sgn}[S_q]]h_i \end{aligned} \quad (\text{C } 4)$$

It is seen from Fig C.1, that the two planes,  $S_p = 0$  and  $S_q = 0$ , divide the  $e - e$  plane into four regions.  $V_i$  as evaluated above is checked for sign definiteness in each of these regions for the two cases. First the Case *CP* is considered

#### Case *CP*

In this case ( $i = p$ ) and  $h_p = -\eta' \text{sgn}[S_p]$ . Thus, it is obvious that

$$\begin{aligned} h_p &> 0, \text{ when } S_p < 0, \text{ and} \\ h_p &< 0, \text{ when } S_p > 0 \end{aligned} \quad (\text{C } 5)$$

Let  $V_p$  represent  $V$  for this case. Note that, the  $-y^T Q y - M[q|S_p| + p|S_q|]$  term in  $V_i$  in (C.4) is always negative definite. The sign definiteness of the remaining terms are established in the four regions

1. Region 1. In this region  $S_p > 0$  and  $S_q > 0$ . Thus,  $[\text{sgn}[S_p] + \text{sgn}[S_q]] = 2$  and  $V$  in (C.4) reduces to

$$V_p = -y^T Q y - M[q|S_p| + p|S_q|] + 2S_p h_p + 2M h_p \quad (\text{C } 6)$$

With  $h_p < 0$  (C.5), it can be seen that  $V_p < 0$  in this region

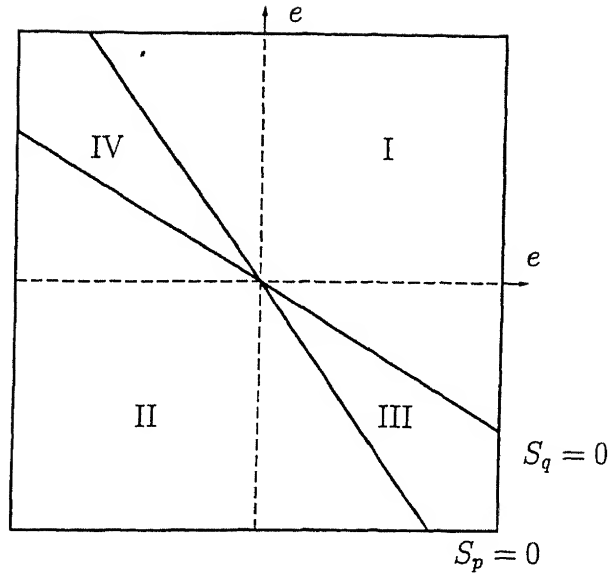


Fig C.1 The  $e$ - $e$  plane

2 Region 2 In this region  $S_p < 0$  and  $S_q < 0$  and  $V$  becomes

$$V_p = -y^T Q y - M[q|S_p| + p|S_q|] + 2S_p h_p - 2M h_p \quad (C 7)$$

In this region,  $h_p > 0$  which makes  $V_p < 0$

3 Region 3 In this region  $S_p > 0$  and  $S_q < 0$  and with  $[\text{sgn}[S_p] + \text{sgn}[S_q]] = 0$ ,  $V$  may be obtained as

$$V_p = -y^T Q y - M[q|S_p| + p|S_q|] + 2S_p h_p \quad (C 8)$$

From (C 5),  $h_p < 0$  ensures that  $V_p$  is negative

4 Region 4 In this region  $S_p < 0$  and  $S_q > 0$  and  $V$  becomes

$$V_p = -y^T Q y - M[q|S_p| + p|S_q|] + 2S_p h_p \quad (C 9)$$

$h_p > 0$  in this region, and thus the time derivative of  $V$  can be seen to be negative.

The above checks establish that  $V$  in (2 40) is a Lyapunov function for Case  $CP$ . Note that the  $S_p h_p$  term in the above equations may be rewritten as  $-\eta'|S_p|$  which is always



negative. The  $V_p$  in the four regions as in (C 6) - (C 9) may be jointly expressed by the following inequality

$$V_p \leq -y^T Q y - M[q|S_p| + p|S_q|] - 2\eta'|S_p| \quad (\text{C } 10)$$

It is evident that  $V$  in (2 40) remains positive definite with the  $V_p$  above being negative definite for all  $M \geq 0$ , and thus the  $V$  is seen to be a valid Lyapunov function for the  $CP$  case

The candidate function is next checked for the Case  $CQ$

Case  $CQ$ .

In this case with  $i = q$ ,  $h_q$  is given as  $-\eta' \text{sgn}[S_q]$ , and thus,

$$\begin{aligned} h_q &> 0, \text{ when } S_q < 0, \text{ and} \\ h_q &< 0, \text{ when } S_q > 0 \end{aligned} \quad (\text{C } 11)$$

Let  $V_q$  represent  $V$  for this case

- 1 Region 1 In this region  $S_p > 0$  and  $S_q > 0$   $V$  in (C 4) reduces to

$$V_q = -y^T Q y - M[q|S_p| + p|S_q|] + 2S_p h_q + 2M h_q \quad (\text{C } 12)$$

With  $h_q < 0$  from (C 11), it can be seen that  $V_q < 0$  in this region

- 2 Region 2 In this region  $S_p < 0$  and  $S_q < 0$  and  $V$  becomes

$$V_q = -y^T Q y - M[q|S_p| + p|S_q|] + 2S_p h_q - 2M h_q \quad (\text{C } 13)$$

In this region,  $h_q > 0$  which makes  $V_q < 0$

- 3 Region 3 In this region  $S_p > 0$  and  $S_q < 0$  and  $V$  becomes

$$V_q = -y^T Q y - qM|S_p| - pM|S_q| + 2S_p h_q \quad (\text{C } 14)$$

Note that the first three terms are negative, however the last term is positive as  $h_q > 0$  (C 11). The above equation may be rewritten as

$$V_q = -y^T Q y - pM|S_q| - (qM - 2h_q)|S_p| \quad (\text{C } 15)$$

It is known that  $\eta'$  and therefore  $|h_q|$  is bounded. Thus if  $(qM - 2h_q) > 0$ , then  $V_q$  becomes negative in this region

4 Region 4 In this region  $S_p < 0$  and  $S_q > 0$  and  $V$  becomes

$$V_q = -y^T Q y - qM|S_p| - pM|S_q| + 2S_p h_q \quad (\text{C } 16)$$

As in the Region 3, here also the first three terms are negative, but with  $h_q < 0$  (C 11), the last term is positive. Rewriting the above equation as

$$V_q = -y^T Q y - pM|S_q| - (qM + 2h_q)|S_p| \quad (\text{C } 17)$$

If  $(qM + 2h_q) > 0$ , then the time derivative of  $V$  can be seen to be negative. Here,  $h_q$  is negative and hence the inequality is the same as in the previous region

Thus it is seen that, if

$$M > \frac{2|h_q|}{q} = \frac{2\eta_M}{q}, \quad (\text{C } 18)$$

then  $V$  (2.40) becomes a Lyapunov function for Case CQ, since  $|h_q| \leq \eta_M$ . In particular, if  $M$  is selected as

$$M = \frac{2\eta_M}{q - \delta_q}, \quad (\text{C } 19)$$

where  $0 < \delta_q < q$ , then  $qM - 2h_q$  term in (C 15) and (C 17) may be replaced by  $\delta_q M$ . The  $V_q$  in (C 12) - (C 17) for the four regions may then be rewritten jointly as

$$V_q \leq -y^T Q y - pM|S_q| - \delta_q M|S_p| \quad (\text{C } 20)$$

This proves the claim ■

# Appendix D

## The Aircraft Parameters, Disturbances, and Uncertainties

In this work, the model responses are generated by

$$\Delta X = A_m \Delta X + B_m \Delta U_p, \quad (\text{D } 1)$$

where  $\Delta X = X - X_{eq}$ , where  $X = [V_t, \alpha, Q, \theta]^T$  represents the vector of desired state trajectories and  $\Delta U_p = U_p - U_{eq}$ , where  $U_p$  represents the pilot inputs, namely the elevator stick and throttle gear deflections. The  $X_{eq}$  and  $U_{eq}$  denotes the quantities at the equilibrium condition. Note that the aircraft states in the chapters are taken as  $[U, W, Q, \theta]^T$ . Thus, appropriate transformations for the first two states needs to be performed. The remaining states (namely,  $p_x$  and  $p_z$ ) not specified in the above equation evolve according to (3.1). The matrices  $A_m$  and  $B_m$  were taken as

$$A_m = \begin{bmatrix} 23580E+0 & 48254E+3 & -35039E+2 & -60960E+3 \\ -30237E-3 & -11753E+1 & 85488E+0 & -81518E-2 \\ -24369E-2 & -12663E+2 & -58805E+1 & -45627E+1 \\ 00000E+0 & 00000E+0 & 10000E+1 & 00000E+0 \end{bmatrix}$$

$$B_m = \begin{bmatrix} 40239E+0 & 17039E+0 \\ -31570E-4 & -21507E-2 \\ 00000E+0 & -18243E+0 \\ 00000E+0 & 00000E+0 \end{bmatrix} \quad (D\ 2)$$

The above model gives desired trajectories in the  $V_t - \alpha$  terms where as these are required to be given in the  $U - W$  frame in the chapters. The quantities may be transferred from  $V_t - \alpha$  reference frame to the  $U - W$  using the following formulae [10]

$$\begin{aligned} U &= V_t \cos(\alpha), \text{ and} \\ W &= V_t \sin(\alpha), \end{aligned} \quad (D\ 3)$$

or inversely as

$$\begin{aligned} V_t &= U^2 + W^2, \text{ and} \\ \tan(\alpha) &= W/U \end{aligned} \quad (D\ 4)$$

The  $U_d$  and  $W_d$  required in the work are evaluated by taking the derivative of D 4 which on simplification using (D 3) gives

$$\begin{aligned} U_d U_d + W_d W_d &= V_{t_d} V_{t_d}, \text{ and} \\ -W_d U_d + U_d W_d &= V_{t_d}^2 \alpha_d \end{aligned} \quad (D\ 5)$$

The above equation may be solved for  $U_d$  and  $W_d$ , in terms of the known  $V_{t_d}$ ,  $\alpha_d$ , and therefore  $U_d$ ,  $W_d$  and the time derivatives  $V_{t_d}$  and  $\alpha_d$  to get

$$\begin{aligned} U_d &= \frac{U_d V_{t_d}}{V_t} - W_d \alpha_d, \text{ and} \\ W_d &= \frac{W_d V_{t_d}}{V_t} + U_d \alpha_d \end{aligned} \quad (D\ 6)$$

The second derivatives of the model response are developed by taking a time derivative of (D 1) and simplifying it to get

$$\begin{aligned} \Delta X &= A_m \Delta X + B_m \Delta U_p, \text{ or} \\ \Delta X &= A_m^2 \Delta X + A_m B_m \Delta U + B_m \Delta U_p \end{aligned} \quad (D\ 7)$$

Thus, the second derivatives  $V_{t_d}$  and  $\alpha_d$  are easily calculated. Note that they contain the derivative of the applied pilot inputs. It now remains to transform these into  $U_d$  and  $W_d$  as are required in (5.43). For this, taking another time derivative of (D.5) and rearranging terms, it is seen that

$$\begin{aligned} U_d U_d + W_d W_d &= V_{t_d}^2 + V_{t_d} V_{t_d} - U_d^2 - W_d^2, \text{ and} \\ -W_d U_d + U_d W_d &= 2V_{t_d} V_{t_d} \alpha_d + V_{t_d}^2 \alpha_d \end{aligned} \quad (\text{D.8})$$

The above linear equations may be solved for the unknowns  $U_d$  and  $W_d$  to get

$$\begin{aligned} U_d &= \frac{1}{V_{t_d}^2} [U_d (V_{t_d}^2 + V_{t_d} V_{t_d} - U_d^2 - W_d^2) - W_d (2V_{t_d} V_{t_d} \alpha_d + V_{t_d}^2 \alpha_d)], \text{ and} \\ W_d &= \frac{1}{V_{t_d}^2} [W_d (V_{t_d}^2 + V_{t_d} V_{t_d} - U_d^2 - W_d^2) + U_d (2V_{t_d} V_{t_d} \alpha_d + V_{t_d}^2 \alpha_d)] \end{aligned} \quad (\text{D.9})$$

The remaining second order derivative in (5.43), i.e. the  $Q_d$  is directly available from (D.7)

The uncertainties and disturbances considered in this work are

- **Uncertainty in the Mass and Inertia:** The nominal values of reciprocal of aircraft mass,  $\hat{R}_m = 1.5 \times 10^{-3}$ , and inverse of the pitching moment of inertia,  $\hat{c}_7 = 1.75 \times 10^{-5}$  have been used. The range of their possible variations have been taken as  $1.0 \times 10^{-3} \leq R_m \leq 2.0 \times 10^{-3}$  and  $1.0 \times 10^{-5} \leq c_7 \leq 2.5 \times 10^{-5}$ . The actual values of these parameters as used in the simulation are reported in Fig. D.1. The bounds  $D_{b1}$  and  $D_{b2}$  can be evaluated as 1/3 and 3/7 respectively.
- **Uncertainty in Aerodynamic Inversion and/or Modeling:** It is assumed that a maximum 20 percentage of error can occur, which means that  $|\delta_{ae}| \leq 0.20$ . For simulation purposes two different sets of variation in  $\delta_{ae}$  has been used as

<i>UC1</i> <i>Uncertainty set 1</i>	<i>UC2</i> <i>Uncertainty set 2</i>	
$\delta_{ae}(1) = 0.05 + 0.145 \cos(3\pi t)$	$\delta_{ae}(1) = -0.19,$	
$\delta_{ae}(2) = -0.02 + 0.15 \cos(5\pi t), \text{ and}$	$\delta_{ae}(2) = 0.175, \text{ and}$	
$\delta_{ae}(3) = 0.1 + 0.08 \cos(3\pi t)$	$\delta_{ae}(3) = 0.185$	(D.10)

for the 3-component force vector

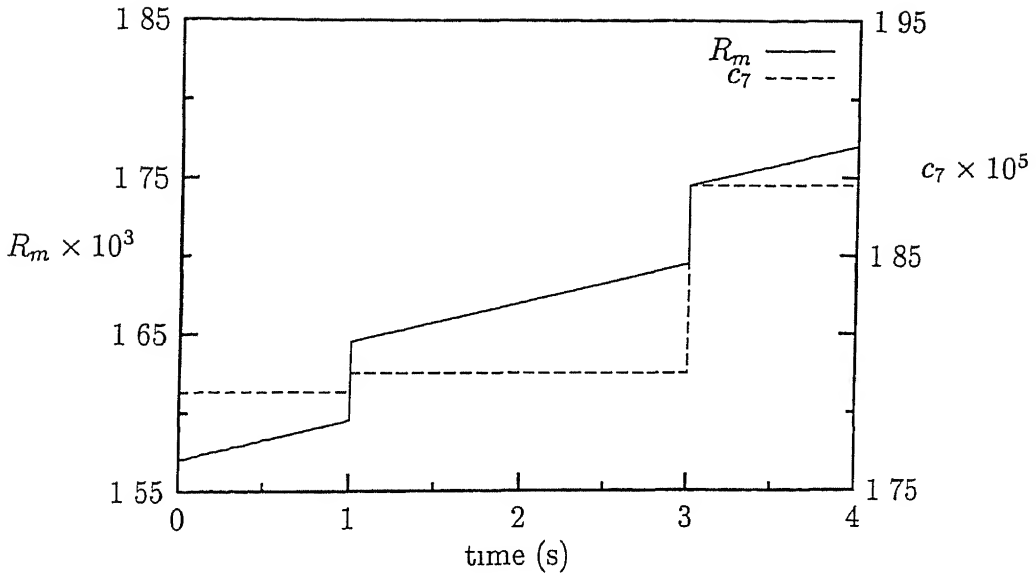


Fig D 1 Variation in the  $R_m$  and the  $c_7$  parameters of the aircraft

- **External Disturbances in the governing differential equation** For simulation purposes the external disturbances were assumed to be

$$\begin{aligned}
 d_U &= 0.05 + 0.25 \cos(3\pi t), \\
 d_W &= -0.05 + 0.25 \cos(7\pi t), \text{ and} \\
 d_Q &= 0.05 + 0.15 \cos(5\pi t) \\
 d_\theta &= 0.04 + 0.25 \cos(3\pi t), \\
 d_x &= -0.74d_0 + 0.25 \cos(7\pi t), \text{ and} \\
 d_z &= 0.05d_0 + 0.85 \cos(5\pi t)
 \end{aligned} \tag{D 11}$$

with  $D_U = 0.3$ ,  $D_W = 0.3$ , and  $D_Q = 0.3$ . Note that the other disturbance terms are unmatched. Their bounds are taken as  $D_\theta = 0.3$ ,  $D_x = 1.0$ , and  $D_z = 1.0$ .

The boundary layer thicknesses have been selected as  $\phi = [0.5, 0.5, 0.005]$  for the tracking mode and  $\phi = [0.5, 0.01, 0.01]$  for the trimming mode.

# Appendix E

## Time Derivatives of Functions

The definitions and notations of time derivatives of smooth scalar, vector and matrix functions of a vector of variables used in this work is given here. The vector of variables is taken as  $\mathbf{x} = [x_1, x_2, \dots, x_n]^T \in \mathcal{R}^n$  and  $\mathbf{x}$  is assumed to be available. Also arguments of the functions are omitted where they are not likely to create confusion.

### Derivative of a Scalar Function

Let  $f(\mathbf{x})$  be a scalar function. Then its time derivative is given using Lie derivatives [21, 22] as

$$\frac{df}{dt} = \frac{\partial f}{\partial x_1} \dot{x}_1 + \dots + \frac{\partial f}{\partial x_n} \dot{x}_n = L_{\mathbf{x}} f \quad (\text{E.1})$$

In this work, the above Lie derivative will be expressed as

$$\frac{df}{dt} = L_{\mathbf{x}} f = R_f \mathbf{x} \quad (\text{E.2})$$

$R_f$  represents a  $1 \times n$  element row vector formed from  $f$  as defined above.

## Derivative of a Vector Function

Let  $\mathbf{f}(\mathbf{x}) = [f_1, f_2, \dots, f_m]^T$  be a  $m \times 1$  vector function. Then using the above notation, its derivative is given as

$$\frac{d\mathbf{f}}{dt} = \begin{pmatrix} L_{\mathbf{x}}f_1 \\ L_{\mathbf{x}}f_2 \\ \vdots \\ L_{\mathbf{x}}f_m \end{pmatrix} = \begin{pmatrix} R_{f_1}\mathbf{x} \\ R_{f_2}\mathbf{x} \\ \vdots \\ R_{f_m}\mathbf{x} \end{pmatrix} = M_f\mathbf{x}, \quad (\text{E } 3)$$

where  $M_f$  may be rewritten using (E 2) and the above equation as

$$M_f = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} & \frac{\partial f_1}{\partial x_n} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} & \frac{\partial f_2}{\partial x_n} \\ \vdots & \vdots & \vdots \\ \frac{\partial f_m}{\partial x_1} & \frac{\partial f_m}{\partial x_2} & \frac{\partial f_m}{\partial x_n} \end{bmatrix} \quad (\text{E } 4)$$

$M_f$  represents a  $m \times n$  matrix formed from the components of the vector function  $\mathbf{f}$  as defined above

## Derivative of a Matrix Function

Let  $A(\mathbf{x})$  represent a  $m \times p$  matrix function. By definition,

$$\frac{d[A(\mathbf{x})]}{dt} = \left[ \frac{da_{ij}(\mathbf{x})}{dt} \right], \quad (\text{E } 5)$$

where,  $a_{ij}(\mathbf{x})$  represents the element in the  $i^{\text{th}}$  row and  $j^{\text{th}}$  column of  $A$ . Since  $a_{ij}$  is a scalar function, its time derivative may be written using (E 2) as

$$\frac{da_{ij}}{dt} = R_{a_{ij}}\mathbf{x} \quad (\text{E } 6)$$



The derivative of  $A$  (E 5), using the above equation can be expressed in a matrix product form as

$$\frac{d[A]}{dt} = \begin{bmatrix} R_{a_{11}} & R_{a_{1p}} \\ R_{a_{21}} & R_{a_{2p}} \\ \vdots & \vdots \\ R_{a_{m1}} & R_{a_{mp}} \end{bmatrix} \begin{bmatrix} \mathbf{x} & 0 & 0 \\ 0 & \mathbf{x} & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \mathbf{x} \end{bmatrix}, \quad (\text{E } 7)$$

where 0 in the above equation represent a  $n$  column zero vector. Using the definition of a Kronecker product, and defining the first matrix in the above product as  $J_A$ , the above equation may be rewritten as

$$\frac{d[A]}{dt} = J_A [I_p \otimes \mathbf{x}] \quad (\text{E } 8)$$

where,  $I_p$  denotes a  $p \times p$  identity matrix,  $\otimes$  represents the Kronecker product. In the  $J_A$  as defined in (E 7) it is clear that, since  $R_{a_{ij}}$  represents a  $1 \times n$  row vector, the matrix will be a  $m \times np$  matrix. Also, the  $[I_p \otimes \mathbf{x}]$  matrix will be a  $np \times p$  matrix by definition. Thus the time derivative of  $A$  results in a  $m \times p$  matrix. The  $J_A$  matrix as defined above is seen from (E 7) to contain the partial derivatives of  $a_{ij}$  with respect to  $\mathbf{x}$  as

$$J_A = \begin{bmatrix} \frac{\partial a_{11}}{\partial x_1} & \frac{\partial a_{11}}{\partial x_2} & \frac{\partial a_{11}}{\partial x_n} & \frac{\partial a_{12}}{\partial x_1} & \frac{\partial a_{12}}{\partial x_2} & \frac{\partial a_{1p}}{\partial x_n} \\ \frac{\partial a_{21}}{\partial x_1} & \frac{\partial a_{21}}{\partial x_2} & \frac{\partial a_{21}}{\partial x_n} & \frac{\partial a_{22}}{\partial x_1} & & \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ \frac{\partial a_{m1}}{\partial x_1} & \frac{\partial a_{m1}}{\partial x_2} & \frac{\partial a_{m1}}{\partial x_n} & \frac{\partial a_{m2}}{\partial x_1} & \frac{\partial a_{m2}}{\partial x_2} & \frac{\partial a_{mp}}{\partial x_n} \end{bmatrix} \quad (\text{E } 9)$$

# Appendix F

## The Uniform Ultimate Boundedness of Systems

**Definition 1** (Global uniform ultimate boundedness) [52]

*An uncertain feedback system with state  $\mathbf{x}(t)$  is said to be globally uniformly ultimately bounded with respect to a set  $S \subset \mathcal{R}^n$ , if*

- 1 for each uncertainty realization and for each  $(t_0, \mathbf{x}(t_0)) \in \mathcal{R} \times \mathcal{R}^n$  there exists at least one solution  $\mathbf{x}(\cdot) : [t_0, t_1) \rightarrow \mathcal{R}^n$ ,  $t_1 > t_0$ ,*
- 2 given any real number  $\delta > 0$ , there exists a real number  $d(\delta) > 0$  such that, for any solution  $\mathbf{x}(\cdot)$  with  $\|\mathbf{x}(t_0)\| \leq \delta$ ,  $\|\mathbf{x}(t)\| < d(\delta)$  for all  $t \in [t_0, t_1)$  all solutions can thus be continued over  $[t_0, \infty]$ ,*
- 3 for every  $\mathbf{x}(t_0) \in \mathcal{R}^n$ , there exists a non-negative constant  $T(\mathbf{x}(t_0), S) \in \mathcal{R}^+$  such that, for every solution  $\mathbf{x}(\cdot)$  with  $t_0$  arbitrary,  $\mathbf{x}(t) \in S$  for all  $t \geq t_0 + T(\mathbf{x}(t_0), S)$*

Using the above definition, the global uniform ultimate boundedness of the following system is established. The  $S_{x_i}$  dynamics in (4.12) may be written in general form as

$$\dot{x} = -kx + d, \tag{F.1}$$

where  $x \in \mathcal{R}$ ,  $k > 0$ , and  $d$  represents the unknown uncertainty term which is given to be bounded with  $|d| < D$ . The subsequent developments follow the steps as outlined in [52, 70]. Select the candidate Lyapunov function as

$$V(x) = \frac{1}{2}x^2 \quad (\text{F.2})$$

Its time derivative may be calculated as  $\dot{V} = -kx^2 + xd$ . With the bound on  $d$  as specified above, it is seen that

$$\dot{V} \leq -kx^2 + D|x| \quad (\text{F.3})$$

Note that  $|x| = \sqrt{2V}$  from (F.2). Thus,  $\dot{V} \leq -2kV + D\sqrt{2V}$ . It is evident from this equation that  $\dot{V} < 0$  if  $V > r_1 - \epsilon$ , where  $\epsilon > 0$  is a small constant, and  $r_1 = D^2/(2k^2)$ . Define the set  $S = \{x \mid \frac{1}{2}x^2 \leq r_1\}$ . From the fact that  $\dot{V} < 0$  if  $V > r_1 - \epsilon$ , it is seen that if  $x(t_0) \in S$  then  $x(t) \in S$  for all  $t \geq t_0$ . The (F.3) may be rewritten as

$$\dot{V} \leq -2kV + D\sqrt{2V} \quad (\text{F.4})$$

The time taken for  $V$  to change from  $V_0$  at  $t = t_0$  to  $V_1$  at  $t = t_1$  may be evaluated as

$$t_1 - t_0 \leq \frac{1}{k} \ln \left[ \frac{k\sqrt{2V_0} - D}{k\sqrt{2V_1} - D} \right] \quad (\text{F.5})$$

Thus, if  $x(t_0) \notin S$ , then the trajectory will reach  $S$  in a finite time given by

$$t_1 - t_0 \leq \frac{1}{k} \ln \left[ \frac{k\sqrt{2V_0} - D}{k\sqrt{2r_1} - D} \right] \quad (\text{F.6})$$

All conditions for uniform ultimate boundedness are thus satisfied

# Appendix G

## The Error Bounds

The  $S_v$  is shown to satisfy the bounds as in (5.51). Putting  $\alpha_i = [|\mathbf{B}_1|\phi_u + \mathbf{D}_1 + D_t(|\mathbf{f}_1 - \mathbf{T}_a|)]_i$ , it may be rewritten in a simpler form component-wise as

$$\begin{aligned} |S_U| &\leq \frac{\alpha_U + D'_{2U}}{K_U[1 - D_t(1, 1)]} \\ |S_W| &\leq \frac{\alpha_W + D'_{2W}}{K_W[1 - D_t(2, 2)]} \\ |S_Q| &\leq \frac{\alpha_Q + D'_{2Q}}{K_Q[1 - D_t(3, 3)]} \end{aligned} \quad (\text{G.1})$$

Similarly, the  $|S_{x_i}|$  are given to be bounded as in (5.52) and using the bounds on the  $B_2$  matrix in (4.29), these may be expressed as

$$\begin{aligned} K_x |S_x| &\leq S_U + S_W + D_{2x}, \\ K_z |S_z| &\leq S_U + S_W + D_{2z}, \text{ and} \\ K_\theta |S_\theta| &\leq S_Q + D_{2\theta} \end{aligned} \quad (\text{G.2})$$

The bounds  $D'_2$  as required in (G.1) are given in (4.43) and are seen to involve the bounds on the position errors, i.e.  $|S_x|$ . Using the bounds on the position errors as

above in (4 43) gives

$$\begin{pmatrix} D'_{2U} \\ D'_{2W} \\ D'_{2Q} \end{pmatrix} = \begin{pmatrix} K_x D_{2x} |\cos(\theta)| + K_z D_{2z} |\sin(\theta)| \\ + D_{2\theta} [|U_d \sin(S_\theta)| + |W_d \cos(S_\theta)| + D_{2x} + D_{2z}] \\ + 2D_{2\theta} [|S_U| + |S_W|] \\ K_x D_{2x} |\sin(\theta)| + K_z D_{2z} |\cos(\theta)| \\ + D_{2\theta} [|U_d \cos(S_\theta)| + |W_d \sin(S_\theta)| + D_{2x} + D_{2z}] \\ + 2D_{2\theta} [|S_U| + |S_W|] \\ K_\theta D_{2\theta} \end{pmatrix}, \text{ or,} \\ = \begin{pmatrix} \beta_U + 2D_{2\theta} [|S_U| + |S_W|] \\ \beta_W + 2D_{2\theta} [|S_U| + |S_W|] \\ K_\theta D_{2\theta} \end{pmatrix}, \quad (\text{G } 3)$$

where,  $\beta_U, \beta_W$  are positive quantities and are obviously defined. It is seen from the above equation that  $D'_{2Q}$  does not depend on any of the velocity error bounds. Thus the bounds  $|S_Q|$  and the  $|S_\theta|$  may be directly evaluated as defined in (G 1) and (G 2) respectively. However, the  $|S_U|$  and the  $|S_W|$  bounds are implicitly defined and may be evaluated as follows.

Using the above developed bounds for  $D'_2$  (G 3), and putting  $\alpha'_i = \alpha_i + \beta_i$ ,  $i = U, W$ ,  $q_1 = K_U[1 - D_t(1, 1)]$ , and  $q_2 = K_W[1 - D_t(2, 2)]$ , the  $|S_U|$  and  $|S_W|$  in (G 1) may be rewritten as

$$\begin{aligned} |S_U| &\leq \frac{\alpha'_U + 2D_{2\theta} [|S_U| + |S_W|]}{q_1}, \text{ and} \\ |S_W| &\leq \frac{\alpha'_W + 2D_{2\theta} [|S_U| + |S_W|]}{q_2} \end{aligned} \quad (\text{G } 4)$$

The above inequalities may be expressed as set of simultaneous linear inequalities in matrix form as

$$\begin{bmatrix} 1 - 2D_{2\theta}/q_1 & -2D_{2\theta}/q_1 \\ -2D_{2\theta}/q_2 & 1 - 2D_{2\theta}/q_2 \end{bmatrix} \begin{pmatrix} |S_U| \\ |S_W| \end{pmatrix} \leq \begin{pmatrix} \alpha'_U/q_1 \\ \alpha'_W/q_2 \end{pmatrix} \quad (\text{G } 5)$$

Note that  $\alpha'_i$ ,  $i = U, W$  and  $q_1, q_2$  are always positive. The solution  $|S_U|$  and  $|S_W|$  of the above equation should be positive to be practically meaningful. This may be easily established using the following theorem.

**Theorem 1 (Forbenius-Perron)** [21] *Consider a square matrix  $A$  with nonnegative elements. Then the largest eigenvalue  $\rho_1$  of  $A$  is nonnegative. Furthermore, consider the equation*

$$(I - \rho^{-1}A)y = z, \quad (\text{G } 6)$$

*where,  $y, z$  are vectors,  $I$  is the identity matrix of appropriate dimensions and all components of the vector  $z$  are nonnegative.*

*If  $\rho > \rho_1$ , then the above equation admits a unique solution  $y$ , whose components  $y_i$  are all nonnegative.*

From (G 5), it is seen that the  $z = [\alpha'_U/q_1 \ \alpha'_W/q_2]^T$  has all its components positive, and the  $A$  matrix, as in the above theorem, is seen from (G 5) to be

$$A = \begin{bmatrix} 2D_{2\theta}/q_1 & 2D_{2\theta}/q_1 \\ 2D_{2\theta}/q_2 & 2D_{2\theta}/q_2 \end{bmatrix} \quad (\text{G } 7)$$

The eigenvalues of the  $A$  matrix are easily obtained as 0 and  $2D_{2\theta}/(q_1 + q_2)$ . According to the above theorem, if the largest eigenvalue is less than 1.0, then the (G 5) is guaranteed to have a positive solution for the norm of the error bounds. Now, by definition  $q_1 + q_2 = K_U[1 - D_t(1, 1)] + K_W[1 - D_t(2, 2)]$ , and since  $D_{2\theta}$  is a known bounded quantity, sufficiently large positive values for  $K_U$  and  $K_W$  can be selected to make the non-zero eigenvalue less than 1.0. Thus, the error bounds may be obtained by solving the simultaneous linear equation set in (G 5). Further, once the  $|S_v|$  are guaranteed to be positive, the positiveness of  $|S_x|$  is obvious from its definition in (4.45). Similar results are presented in [70] using a different approach.

## APPENDIX 1

### ERRATA

The following corrections are to be included in the thesis

**1) Ref: Pg-6: 5th Line-**

*"Using this result, is proposed"* should be corrected to  
This result has been used to propose a new method of selection of controller parameters, which gives a lower time to OTE

**2) Ref: Pg-9: 15th Line-**

*"Application of the unmatched uncertainty"* should be corrected to  
The ML approach is then applied to a third order nonlinear system with unmatched uncertainties and disturbances. A new method of selecting the gain of the switching term is proposed. Further it is shown that the conventional SMC may be extended to tackle the unmatched uncertainty case with the proposed gain selection.

**3) Ref: Pg-72: 18th Line-**

*"The  $\Delta_{ae}$  in the simulation"* The ' $\Delta_{ae}$ ' in this line should be corrected to ' $\Delta_{ac}$ '

**4) Ref: Pg-94: 14th Line-**

*"As seen earlier in this chapter"* should be corrected to  
As discussed in Section 4.2, the effect of disturbances in the outer loops is easily passed on to the inner loop. This simple propagation of disturbances results in a simplified robustness analysis, as will be shown in this chapter.

**5) Ref: Pg-94: 21st Line-**

*"Following the developments in the innermost loop"* should be corrected to  
Following the developments in Chapter 4, the tracking of position variables is done in the outer loop by generating augmented velocity command signals. These augmented velocity signals are tracked in the inner loop by synthesizing augmented input command signals. A SMC law is then designed to track the commanded input signals in the innermost loop.

**6) Ref: Pg-116: 10th Line-**

*"In this chapter, is developed"* should be corrected to  
In this chapter, the ML strategy has been used to develop a robust control law design method for a nonlinear system with specified input dynamics under unmatched uncertainties and disturbances.

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